

Reference Correlation for the Viscosity of Xenon from the Triple Point to 750 K and up to 86 MPa

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A new wide-ranging correlation for the viscosity of xenon, based on the most recent theoretical calculations and critically evaluated experimental data, is presented. The correlation is designed to be used with an existing equation of state, and it is valid from the triple point to 750 K, at pressures up to 86 MPa. The estimated expanded uncertainty (at a coverage factor of $k = 2$) varies depending on the temperature and pressure, from 0.2 % to 3.6 %. A term accounting for the critical enhancement is also included. The correlation behaves in a physically reasonable manner when extrapolated to 200 MPa, however care should be taken when using the correlations outside of the validated range.

Key words: transport properties; viscosity; xenon.

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1 Introduction

In a series of recent papers, reference correlations for the viscosity of selected common fluids [1-8] have been developed that cover a wide range of temperature and pressure conditions, including the gas, liquid, and supercritical phases. In this paper, the methodology adopted in the aforementioned papers is extended to developing a new reference correlation for the viscosity of xenon.

The currently employed reference correlation for the viscosity of xenon was developed by Hanley et al. [9] in 1974; it is based on the corresponding-states principle and covers a temperature range (165 – 500) K and pressures up to 20 MPa. The only other available correlation is the corresponding-states model developed by Huber [10] and implemented in REFPROP v10.0 [11]; with 1 % uncertainty for the gas-phase viscosity and 5 % for the liquid-phase viscosity up to 60 MPa and temperatures from (170 – 750) K.

The analysis that will be described is based on the most recent theoretical advances as well as the best available experimental data for the viscosity. Thus, a prerequisite to the analysis is a critical assessment of the experimental data. For this purpose, two categories of experimental data are defined: primary data, employed in the development of the correlation, and secondary data, used simply for comparison purposes. According to the recommendation adopted by the Subcommittee on Transport Properties (now known as The International Association for Transport Properties) of the International Union of Pure and Applied Chemistry, the primary data are identified by a well-established set of criteria [12]. These criteria have been successfully employed to establish standard reference values for the viscosity and thermal conductivity of fluids over wide ranges of conditions, with uncertainties in the range of 1 %. However, in many cases, such a narrow definition unacceptably limits the range of the data representation. Consequently, within the primary data set, it is also necessary to include results that extend over a wide range of conditions, albeit with a higher uncertainty, provided they are consistent with other lower uncertainty data or with theory. In all cases, the uncertainty claimed for the final recommended data must reflect the estimated uncertainty in the primary information.

2 The Correlation

The viscosity η can be expressed [1, 4-7] as the sum of four independent contributions, as

$$\eta(\rho, T) = (\eta_0(T) + \eta_1(T)\rho + \Delta\eta(\rho, T)) \times \Delta\eta_c(\rho, T), \quad (1)$$

where ρ is the density, T is the absolute temperature, and the first term, $\eta_0(T) = \eta(0, T)$, is the contribution to the viscosity in the dilute-gas limit, where only two-body molecular interactions occur. The linear-in-density term, $\eta_1(T)\rho$, known as the initial density dependence term, can be separately established with the development of the Rainwater-Friend theory [13-15] for the transport properties of moderately dense gases. The critical enhancement term, $\Delta\eta_c(\rho, T)$, arises from the long-range density fluctuations that

occur in a fluid near its critical point, which contribute to divergence of the viscosity at the critical point. This term for viscosity is significant only in the region very near the critical point, as shown in Vesovic et al. [16] and Hendl et al. [17]. To calculate this enhancement term, the crossover theory of Bhattacharjee and coworkers [18] may be used, provided there are adequate data to determine the parameters. Finally, the term $\Delta\eta(\rho,T)$, the residual term, represents the contribution of all other effects to the viscosity of the fluid at elevated densities including many-body collisions, molecular-velocity correlations, and collisional transfer.

The identification of these four separate contributions to the viscosity and to transport properties in general is useful because it is possible, to some extent, to treat $\eta_0(T)$, $\eta_1(T)$, and $\Delta\eta_c(\rho,T)$ theoretically. In addition, it is possible to derive information about both $\eta_0(T)$ and $\eta_1(T)$ from experiment. In contrast, there is little theoretical guidance concerning the residual contribution, $\Delta\eta(\rho,T)$, and therefore its evaluation is based entirely on an empirical equation obtained by fitting experimental data.

Table 1 summarizes, to the best of our knowledge, the theoretical prediction/estimations as well as the experimental measurements of the viscosity of xenon reported in the literature. Uncertainties given in Table 1 are those provided by the original authors. As early as 1962, based on kinetic-theory calculations, Svehla [19] proposed dilute-gas viscosity values covering the temperature range (100 – 5000) K. However, the first empirical correlation for the viscosity and thermal conductivity of xenon based on the corresponding-states principle was proposed in 1974 by Hanley et al. [9]. The viscosity correlation covered a temperature range from the triple point to 500 K and pressures up to 20 MPa with an uncertainty of 5 %.

In 1983, Najafi et al. [20] employed an improved two-parameter corresponding-states scheme to correlate the dilute-gas viscosity from (100 – 2000) K with an uncertainty of better than 2 %, while Vargaftik and Vasilevskaya [21] proposed dilute-gas viscosity values based on kinetic-theory calculations, covering a temperature range (800 – 5000) K with an uncertainty of up to 5 %.

In 1990, Bich et al. [22] proposed reference values for the viscosity of xenon from the triple point to 5000 K at zero density and also at 0.101325 MPa, with an uncertainty ranging from 0.3 % to 2 % at the highest temperatures.

In 1999, Berg et al. [23] reported viscosity data near the critical point of xenon from the Critical Viscosity of Xenon (CVX) experiment. Data were measured with a low-frequency torsional viscometer at frequencies from 1/32 Hz to 12.5 Hz on the ground and aboard the Space Shuttle in microgravity. These exceptional data have an estimated uncertainty of 1.6 % and approach to within 0.1 mK of the critical temperature along the critical isochore.

In 2007, May et al. [24] reported new very accurate measurements of the viscosity of xenon in relation to that of helium, performed in a single-capillary viscometer at 298.15 K, and the reference value for the viscosity of xenon, $(23.026 \pm 0.016) \mu\text{Pa}\cdot\text{s}$, at that temperature, was proposed. Furthermore, a two-capillary viscometer was employed for the measurement of the viscosity of xenon over (202 – 298) K.

A critical assessment of 18 viscometers, carried out by Berg and Moldover [25] in 2012, resulted in the proposition of the viscosity value of (23.0183 ± 0.0072) $\mu\text{Pa}\cdot\text{s}$ for xenon at 298.15 K and zero density.

In 2016, Vogel [26] published low-uncertainty values of the viscosity of xenon at zero density over the temperature range (295 – 650) K. These were based on a reevaluation of their oscillating-disk measurements [27], employing a more recent value of the viscosity of argon for the calibration of the instrument. Their work was expanded by Hellmann et al. [28], who produced reference values for the dilute gas over a temperature range (100 – 5000) K with an uncertainty of 0.07 to 0.28 %, based on an *ab initio* intermolecular potential energy and related spectroscopic and thermophysical properties data for xenon.

In 2020, the combined use of experimental viscosity ratios together with *ab initio* calculations for helium has driven significant improvements in the description of dilute gas transport properties [29]. Hence, Xiao et al. [29, 30] first used improvements to *ab initio* helium calculations [31] to update previously measured viscosity ratios [24]. Subsequently, they used these improved values to get better reference correlations for the dilute-gas viscosity of xenon and 9 other gases. The new reference dilute-gas viscosity correlation for xenon covers the temperature range from (100 – 5000) K with a relative uncertainty 0.2 %, and it will form the dilute-gas viscosity contribution of xenon in this work. We note that the uncertainties in Xiao et al. [29, 30] are expressed as standard uncertainties corresponding to a coverage factor of $k = 1$; in this work all uncertainties discussed are combined expanded uncertainties with a coverage factor of $k = 2$.

The dilute-gas extrapolated viscosity measurements of Lin et al. [32], performed with an uncertainty of 0.1 % with a double capillary calibrated with argon over the temperature range (298–393) K, were included in the primary data set. The following seven atmospheric-pressure viscosity investigators were also considered part of the primary data set:

- The 1972 and 1978 measurements of Kestin et al. [33, 34], with a 0.1-0.3 % uncertainty, over the temperature ranges (298 – 973) K, and (298 – 778) K respectively, performed in an oscillating-disk viscometer calibrated with noble gases,
- the measurements of Rigby and Smith [35] over (293– 972) K with an uncertainty of 0.3 %, Dawe and Smith [36] over (300– 1600) K, and Clarke and Smith [37] over (176– 375) K with an uncertainty of 0.5 % to 1 %, all performed with a capillary instrument calibrated with nitrogen,
- the measurement of Thornton [38] performed in a Rankine viscometer with a 1 % uncertainty, and
- the high-temperature, (1100 – 2000) K, measurements of Goldblatt and Wageman [39] performed with a capillary viscometer, calibrated with xenon at 298 K, with an uncertainty of 0.5 %.

Table 1 Viscosity theoretical predictions and measurements of xenon

Investigators / Reference	Technique employed ^a	Purity ^b (%)	Uncertainty (%)	No. of data	Temperature range (K)	Pressure range (MPa)
Reference Correlations/Values						
Xiao et al. [29]	Dil.Gas Reference Cor.	-	0.2	-	100-5000	0
Hellmann et al. [28]	Ab initio Calculations	-	0.07-0.28	109	100-5000	0
Berg and Moldover [25]	Recommended Value	-	0.03	1	298.15	0
May et al. [24]	Recommended Value	-	0.07	1	298.15	0
Bich et al. [22]	Recommended values	-	0.3-2.0	92	165-5000	0
			0.3-2.0	92	165-5000	0.1
Vargaftik and Vasilevskay [21]	Kinetic Theory Calc.	-	3-5	33	800-5000	0.1
Najafi et al. [20]	CS Correlation	-	2	-	100-2000	0
Hanley et al. [9]	CS Correlation	-	5	-	165-500	0.1-20
Svehla [19]	Kinetic Theory Calc	-	na	50	100-5000	0.1
Primary Data						
Lin et al. [32]	Cap (cal Ar)	99.999	0.11	10	298-393	0
Vogel [26]	OD (reeval Ar)	99.99	0.2-0.4	20	295-650	0
May et al. [24]	Single Cap	99.995	0.07	1	298.15	0
	Double Cap	99.999	0.07	7	202-298	0
Berg et al. [23]	(CVX) Torsion Oscill.	99.995	1.6	43	292-306	5.8-7.8
Kestin et al. [34]	OD (cal NG 298 K)	99.995	0.1-0.3	9	298-778	0.1
Kestin et al. [33]	OD (cal NG 298 K)	99.998	0.1-0.3	8	298-973	0.1
Ulybin and Makarushkin [40]	Cap (abs)	99.894	1.4	68	170-293	0.1-54
Goldblatt and Wageman [39]	Cap (cal Xe 283 K)	99.99	0.5	11	1100-2000	0.1
Dawe and Smith [36]	Cap (cal N ₂ 293 K)	99.998	0.5-1	15	300-1600	0.1
Clarke and Smith [37]	Cap (cal N ₂ 293 K)	99.998	0.5-1	9	176-375	0.1
Rigby and Smith [35]	Cap (cal N ₂ av.val)	99.0	0.3	14	293-972	0.1
Trappeniers et al. [41]	Cap (abs)	na	0.5	23	273-348	1-86
Reynes and Thodos [42]	Cap	99.99	na	48	323-473	7-83
Thornton [38]	Rank (cal N ₂ 291 K)	99.0	1	1	291	0.09
Secondary Data						
Grisnik [43]	Cap (abs)	na	3	31	210-298	0.09-0.1
Malbrunot et al. [44]	QuartzAtt	na	25	7	161-180	0.08-0.2
Baharudin et al. [45]	BB	na	12	7	168-271	0.1-3.9
Strumpf et al. [46]	OQ	<40 ppm	3	182	287-303	5.5-8.6
Zollweg et al [47]	LS	na	3	EQ	285-289	5.3-5.9
Legros and Thomaes [48]	Cap (cal Ar)	99.94	1	9	163-169	0.09-0.13
Kestin and Leidenfrost [49]	OD (abs)	99.929	0.05	8	298	0.1-2.9

^a abs, absolute; Ar, argon; av. val, average values; BB, Brillouin Bandwidth ; cal, calibrated; calc, calculated; Cap, Capillary; CVX, Torsion Oscill., critical viscosity of xenon by Torsional Oscillator; LS, Light scattering; NG, noble gases; N₂, nitrogen; OD, Oscillating Disc; OQ, Oscillating Quartz; Quartz Att, Quartz-attenuating technique; Rank, Rankine viscometer; reeval, reevaluated.

^b na. not available.

In relation to high-pressure measurements, Ulybin and Makarushkin [40] performed capillary measurements with an uncertainty of 1.4 % in the temperature range (170 – 293) K and up to 54 MPa. These were included in the primary data set, regardless of their relatively high uncertainty, as they extend to high pressures. Trappeniers et al. [41] published capillary measurements with a 0.5 % uncertainty over the temperature range (273 – 348) K and up to 86 MPa. This set was also part of the primary data sets. We also included with some caution in the primary data set the measurements of Reynes and Thodos [42], of unquoted uncertainty, as they extended to pressures of 83 MPa.

The remaining sets were not considered as primary sets as their quoted uncertainty was 3 % or higher, with the exception of a) the earlier measurements by Kestin and Leidenfrost [49] that were replaced by the more recent ones [33, 34], and b) the 1966 capillary measurements of Legros and Thomaes [48] performed with a 1 % uncertainty in the limited temperature range of (163 – 169) K, which were however about 3 % to 4 % higher than the other two primary sets that extend over a much wider range of temperatures (170 – 293) K, Ulybin and Makarushkin [40], and (176 – 375) K, Clarke and Smith [37].

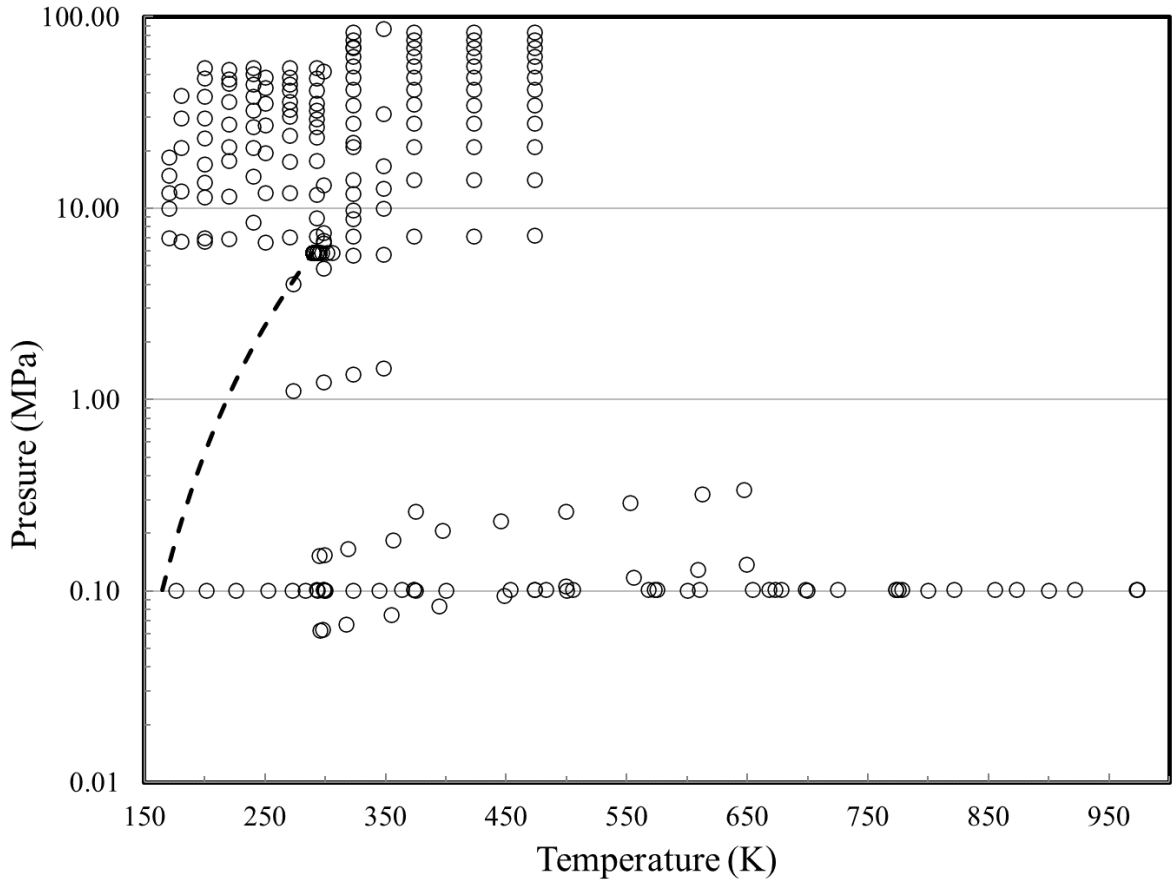


FIG. 1 Temperature-pressure ranges of the theoretical calculations and the primary experimental viscosity data for xenon (temperature restricted to 1000 K as in the region up to 5000 K only dilute-gas values exist). (–) saturation curve.

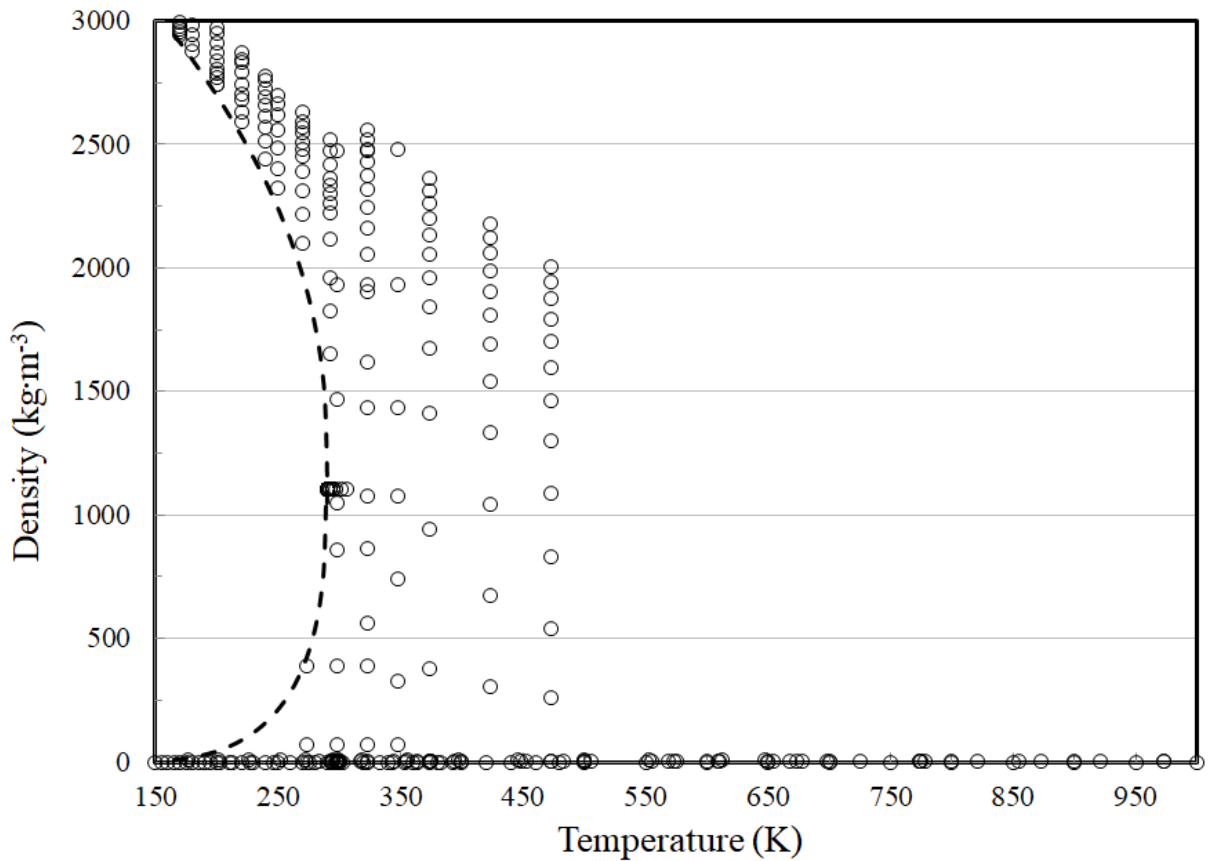


FIG. 2 Temperature-density ranges of the theoretical calculations and the primary experimental viscosity data for xenon (temperature restricted to 1000 K as in the region up to 5000 K only dilute-gas values exist). (–) saturation curve.

Figures 1 and 2 show the ranges of the theoretical calculations and primary measurements outlined in Table 1, and the phase boundary may be seen as well. The development of the correlation requires densities; Lemmon and Span [50] in 2006 developed an accurate, wide-ranging equation of state that is valid from the triple point up to 750 K and 700 MPa. The equation of state has an uncertainty in density of 0.2 % up to 100 MPa, rising to 1 % at higher pressures. We also adopt the values for the critical point from their equation of state; the critical temperature, T_c , and the critical density, ρ_c , are 289.733 K and 1102.8612 kg m⁻³, respectively [50]. The triple-point temperature given by Lemmon and Span [50] is 161.405 K. We here adopt the value of 161.406 K given in 2005 by Hill and Steele [51] and recently confirmed by Steur et al.[52]

2.1 The dilute-gas limit viscosity term

The dilute-gas limit viscosity, $\eta_0(T)$ in $\mu\text{Pa s}$, can be analyzed independently of all other contributions in Eq. 1. As already discussed in the previous section, Xiao et al. [29, 30] first used improvements to *ab initio* helium calculations [31] to update previously measured viscosity ratios [24]. Following this, they used these improved values to get better reference correlations for the dilute-gas viscosity of xenon and 9 other gases. The new reference dilute-gas viscosity correlation for xenon covers the temperature range from (100 – 5000) K with an expanded combined ($k = 2$) uncertainty of 0.2 %, and it will form the dilute-gas viscosity contribution of xenon in this work. The dilute-gas limit viscosity, η_0 ($\mu\text{Pa}\cdot\text{s}$) given by Xiao et al. [29, 30] is,

$$\eta_0(T) = \eta_0(298.15 \text{ K}) \exp \left\{ \sum_{i=1}^{11} a_i \left(\ln \left[\frac{T}{298.15 \text{ K}} \right] \right)^i \right\}. \quad (2)$$

For the viscosity at 298.15 K, $\eta_0(298.15 \text{ K})$, the value of $(23.0183 \pm 0.0072) \mu\text{Pa}\cdot\text{s}$, proposed by Berg and Moldover [25] was adopted [29]. The coefficients a_i (-), are shown in Table 2.

Table 2 Coefficients a_i of Eq. 2 [29].

i	a_i
1	$9.652\ 514 \times 10^{-1}$
2	$-5.237\ 199 \times 10^{-2}$
3	$-6.758\ 414 \times 10^{-2}$
4	$2.855\ 787 \times 10^{-2}$
5	$1.002\ 789 \times 10^{-2}$
6	$-9.639\ 621 \times 10^{-3}$
7	$1.329\ 770 \times 10^{-3}$
8	$1.114\ 305 \times 10^{-3}$
9	$-5.992\ 234 \times 10^{-4}$
10	$1.224\ 218 \times 10^{-4}$
11	$-9.584\ 978 \times 10^{-6}$

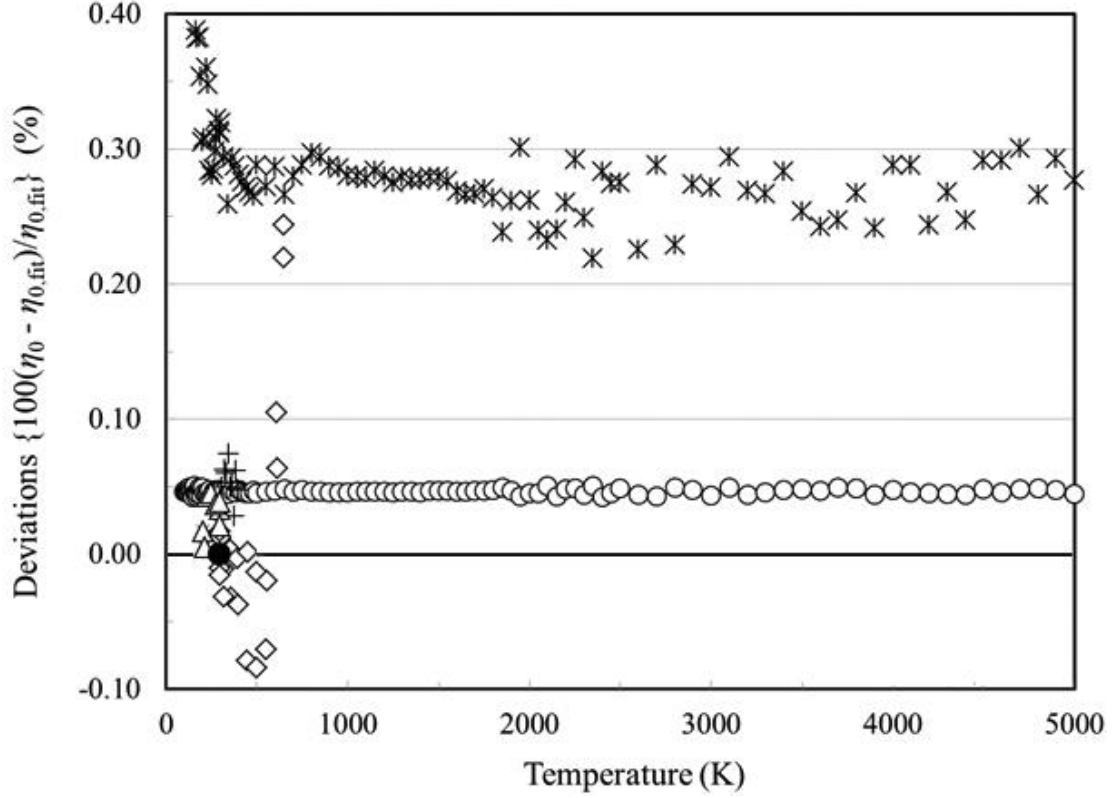


FIG. 3 Percentage deviations of the dilute-gas theoretical values and experimental values of the viscosity of xenon from the values calculated by Eq. 2. Hellmann et al. [28] (\circ), Berg and Moldover [25] (\bullet), Bich et al. [22] (\ast), Lin et al. [32] ($+$), Vogel [26] (\diamond), and May et al. [24] (\triangle).

Figure 3 shows the percentage deviations from the dilute-gas viscosity correlation of Equation 2, as a function of temperature. The *ab initio* 2017 calculated values of Hellmann et al. [28] agree with the proposed correlation within 0.05 %, while the 2012 recommended value of Berg and Moldover [25] is fully reproduced. Furthermore, the 1990 recommended dilute-gas values of Bich et al. [22], quoted with an uncertainty of 0.3 % to 2 %, are well within the mutual uncertainties. In the same figure, we included the dilute-gas viscosity extrapolated from measurements from Lin et al. [32], Vogel [26], and May et al. [24] with corresponding uncertainties of 0.1 %, 0.2 % to 0.4 %, and 0.07 %. These three sets also agree well with the proposed correlation of Eq. 2.

Hence Equation 2, proposed by Xiao et al. [29, 30], represents the dilute-gas limit viscosity of xenon with an uncertainty of 0.2 % over the temperature range (100 – 5000) K. Note that the 1990 values of Bich et al. [22], calculated with an uncertainty of 0.3 % to 2 %, are still represented within the mutual uncertainties.

2.2 The initial-density dependence viscosity term

The temperature dependence of the linear-in-density coefficient of the viscosity $\eta_1(T)$ in Eq. 1 is large at subcritical temperatures and must be taken into account to obtain an accurate representation of the behavior of the viscosity in the vapor phase. It changes sign from positive to negative as the temperature decreases. Therefore, the viscosity along an isotherm should first decrease in the vapor phase and subsequently increase with increasing density [53]. Vogel et al. [54] have shown that fluids exhibit the same general behavior of the initial density dependence of viscosity, which can also be expressed by means of the second viscosity virial coefficient $B_\eta(T)$ in $\text{m}^3 \cdot \text{kg}^{-1}$, as

$$B_\eta(T) = \frac{\eta_1(T)}{\eta_0(T)}. \quad (3)$$

Note that in the above equation, if the dilute-gas limit viscosity, $\eta_0(T)$, is expressed in $\mu\text{Pa s}$, then the initial-density viscosity, $\eta_1(T)$, will be expressed in $\mu\text{Pa} \cdot \text{s} \cdot \text{m}^3 \cdot \text{kg}^{-1}$. The second viscosity virial coefficient can be obtained according to the theory of Rainwater and Friend [13, 14] as a function of a reduced second viscosity virial coefficient, $B_\eta^*(T^*)$, as

$$B_\eta^*(T^*) = \frac{B_\eta(T) M}{N_A \sigma^3}, \quad (4)$$

where [14]

$$B_\eta^*(T^*) = \sum_{i=0}^6 b_i (T^*)^{-0.25i} + b_7 (T^*)^{-2.5} + b_8 (T^*)^{-5.5}. \quad (5)$$

In Eq. 4, M is the molar mass in g mol^{-1} given in Table 3, T^* is the scaled temperature $T/(\varepsilon/k_B)$, and N_A is the Avogadro constant. The coefficients b_i from Ref. [53] are given in Table 3, together with the scaling parameters σ and ε/k_B proposed by Bich et al. [22].

Table 3 Coefficients and parameters for Eqs. 4 and 5.

Molar mass		
131.293 $\text{g} \cdot \text{mol}^{-1}$		
Scaling parameters		
$\varepsilon/k_B = 250.0 \text{ K}$	$\sigma = 0.396 \text{ nm}$	
Coefficients b_i for Eq. 5 [53]		
$b_0 = -19.572 \ 881$	$b_1 = 219.739 \ 99$	$b_2 = -1015.322 \ 6$
$b_3 = 2471.012 \ 5$	$b_4 = -3375.171 \ 7$	$b_5 = 2491.659 \ 7$
$b_6 = -787.260 \ 86$	$b_7 = 14.085 \ 455$	$b_8 = -0.346 \ 641 \ 58$

Figure 4 shows the experimental and calculated values of the initial-density viscosity. In the same figure, the initial-density viscosity values calculated from the dilute-gas and 0.1 MPa values given by Bich et al. [22] are also shown. The agreement is excellent.

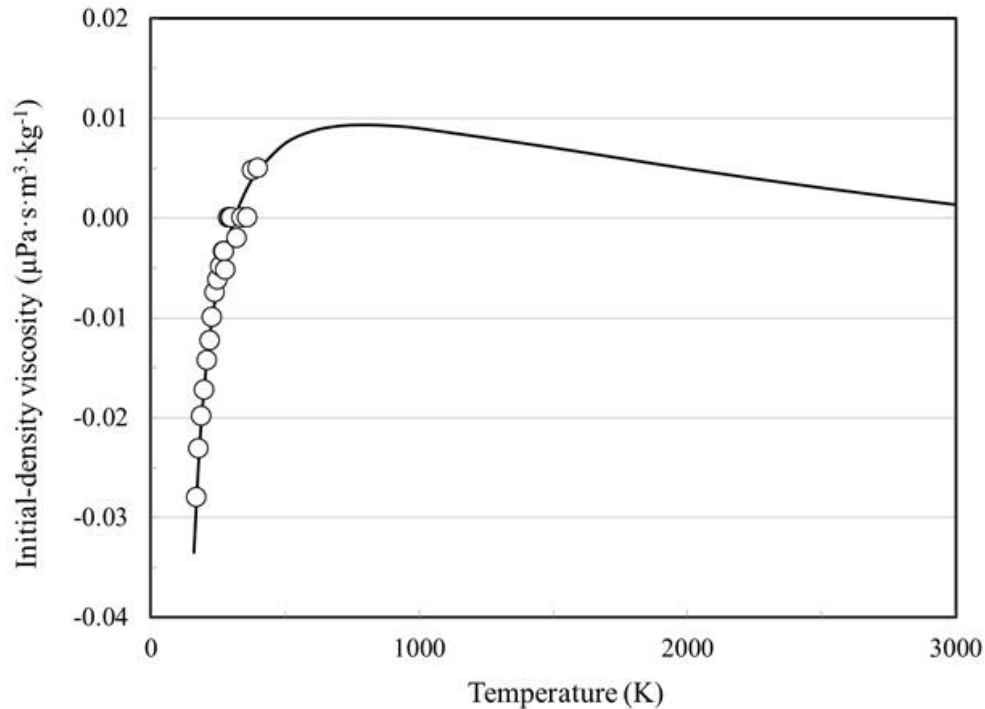


FIG. 4 Experimental and calculated values of the initial-density viscosity. Theoretical, Eqs. 2-5 (—), Bich et al. [22] (○).

2.3 The residual term

As stated in Section 2, the residual viscosity term, $\Delta\eta(\rho, T)$, represents the contribution of all other effects to the viscosity of the fluid at elevated densities including many-body collisions, molecular-velocity correlations, and collisional transfer. An attempt to employ the hard-sphere model proposed by Assael et al. [55] was not very successful, as the present data cover the gas, liquid, and supercritical regions. Hence, it was preferred to evaluate this term almost entirely on experimentally obtained data, as discussed in the next paragraph.

The procedure adopted during this analysis used symbolic regression software [56] to fit all the primary data (excluding the critical region) to the residual viscosity. Symbolic regression is a type of genetic programming that allows the exploration of arbitrary functional forms to regress data. The functional form is obtained by use of a set of operators, parameters, and variables as building blocks. Most recently this method has been used to obtain correlations for the viscosity of R161 [1], *n*-undecane [3], R1234yf and R1234ze(E) [2], and ammonia [8]. In the present work, we restricted the operators to the set (+, -, *, /) and the operands (constant, T_r , ρ_r), with $T_r = T/T_c$ and $\rho_r = \rho/\rho_c$. As mentioned earlier,

the critical temperature $T_c = 289.733$ K and critical density $\rho_c = 1102.8612$ kg·m⁻³ are from the equation of state of Lemmon and Span [50]. In addition, we adopted a form suggested by the hard-sphere model employed by Assael *et al.* [55], $\Delta\eta(\rho_r, T_r) = (\rho_r^{2/3} T_r^{1/2}) F(\rho_r, T_r)$, where the symbolic regression method was used to determine the functional form for $F(\rho_r, T_r)$. For this task, the dilute-gas limit and the initial density dependence term were calculated for each experimental point, employing Eqs. 2-5, and subtracted from the experimental viscosity to obtain the residual term, $\Delta\eta(\rho_r, T_r)$. The density values employed were obtained by the equation of state of Lemmon and Span [50]. The final equation obtained was

$$\Delta\eta(\rho, T) = (\rho_r^{2/3} T_r^{1/2}) \left\{ T_r + c_0 T_r \rho_r^4 + \frac{c_1 \rho_r^7}{T_r} + \frac{(c_2 + c_3 \rho_r)}{T_r^2} \right\}. \quad (6)$$

Coefficients c_i are given in Table 4, and $\Delta\eta$ is in $\mu\text{Pa}\cdot\text{s}$.

Table 4 Coefficients c_i for Eq. 6.

i	c_i
0	1.396 328 251
1	5.418 871 011 $\times 10^{-4}$
2	4.478 809 952
3	2.491 698 858 $\times 10^{+1}$

2.4 Critical Enhancement

The viscosity of xenon in the critical region has been definitively studied by Berg and Moldover [57] and Berg *et al.* [23] on earth and in microgravity. Measurements in microgravity allowed the critical temperature to be approached much more closely along the critical isochore. It was found that xenon exhibited viscoelasticity for reduced temperatures of $t = (T - T_c)/T_c \leq 10^{-5}$. The viscosity measurements were made at frequencies from 1/32 to 12.5 Hz and the results reported from measurements at 2 Hz are considered here. The relative repeatability of the viscosity measurements was about ± 0.2 % and the relative uncertainty of the viscometer calibration was ± 1.6 % at a 2σ confidence level.

These results for xenon in the critical region agreed well with the theory of Bhattacharjee and coworkers [18, 58]. This critical enhancement theory has also been shown to work well for both water [59, 60], and heavy water [61]. The critical enhancement is given by

$$\Delta\eta_c = \exp(x_\mu Y), \quad (7)$$

where x_μ is the critical exponent for viscosity and the function Y is defined for two ranges of correlation length ξ . For $0 \leq \xi \leq 0.06$ nm

$$Y = \frac{1}{5} q_C \xi (q_D \xi)^5 \left(1 - q_C \xi + (q_C \xi)^2 - \frac{765}{504} (q_D \xi)^2 \right), \quad (8)$$

while for $\xi > 0.06$ nm

$$Y = \frac{1}{12} \sin(3\psi_D) - \frac{1}{4q_C \xi} \sin(2\psi_D) + \frac{1}{(q_C \xi)^2} \left[1 - \frac{5}{4} (q_C \xi)^2 \right] \sin(\psi_D) - \frac{1}{(q_C \xi)^3} \left\{ \left[1 - \frac{3}{2} (q_C \xi)^2 \right] \psi_D - \left| (q_C \xi)^2 - 1 \right|^{3/2} L(w) \right\} \quad (9)$$

with

$$\psi_D = \arccos(1 + q_D^2 \xi^2)^{-1/2} \quad (10)$$

and with the function $L(w)$ given by

$$L(w) = \begin{cases} \ln \frac{1+w}{1-w}, & \text{for } q_C \xi > 1 \\ 2 \arctan |w|, & \text{for } q_C \xi \leq 1 \end{cases}. \quad (11)$$

The variable w is defined by

$$w = \left| \frac{q_C \xi - 1}{q_C \xi + 1} \right|^{1/2} \tan\left(\frac{\psi_D}{2}\right). \quad (12)$$

The critical enhancement of viscosity given by Eqs. (7) – (12) is a function of the correlation length ξ calculated from the equation of state:

$$\xi = \xi_0 \left(\frac{\Delta\chi}{\Gamma_0^+} \right)^{1/\gamma} \quad (13)$$

in terms of $\overline{\Delta\chi}$ (≥ 0) which is defined by

$$\overline{\Delta\chi} = \overline{\rho} \left[\left(\frac{\partial \overline{\rho}(\overline{T}, \overline{\rho})}{\partial \overline{p}} \right)_{\overline{T}} - \left(\frac{\partial \overline{\rho}(\overline{T}_R, \overline{\rho})}{\partial \overline{p}} \right)_{\overline{T}} \frac{\overline{T}_R}{\overline{T}} \right]. \quad (14)$$

When $\overline{\Delta\chi}$ calculated by Eq. (14) is less than zero, it must be set to zero for calculations to proceed.

The constants needed to compute the critical enhancement, $\Delta\eta_c$, in Eqs. (7) – (14) are those found by Berg and coworkers, and are provided in Table 5.

Table 5 Critical-Region Constants for viscosity critical enhancement.

x_μ	0.068
q_C^{-1}	3.6 nm
q_D^{-1}	1.15 nm
ν	0.630
γ	1.239
ξ_0	0.184 nm
Γ_0^+	0.058
\overline{T}_R	1.5

The correlation length calculated from the classical equation of state may not have the theoretical scaling behavior very close to the critical point [62]. Near the critical point, the correlation length is expected to follow

$$\xi \approx \xi_0 \left(\frac{T - T_c}{T_c} \right)^{-\nu}. \quad (15)$$

Figure 5 shows the correlation length calculated from the equation of state with Eqs. (13) and (14) along with the curve calculated from eq. (15). Systematic differences are apparent very near to the critical point.

The viscosity data of Berg et al.[23] are shown in Figure 6 along with curves based on critical enhancement calculated with correlation length from the equation of state as a solid line and from the power law expression of Eq. (15) as a dotted line.

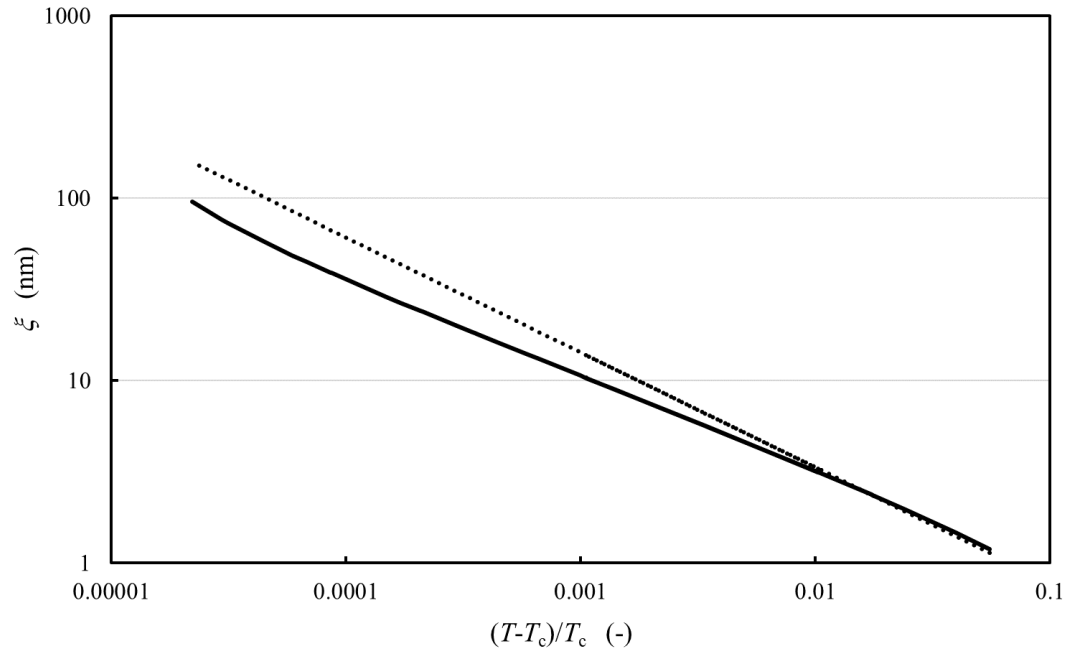


FIG. 5 Correlation length calculated with Eqs. (13) and (14) and the equation of state shown as a solid line and with power-law expression of Eq. (15) as a dotted line.

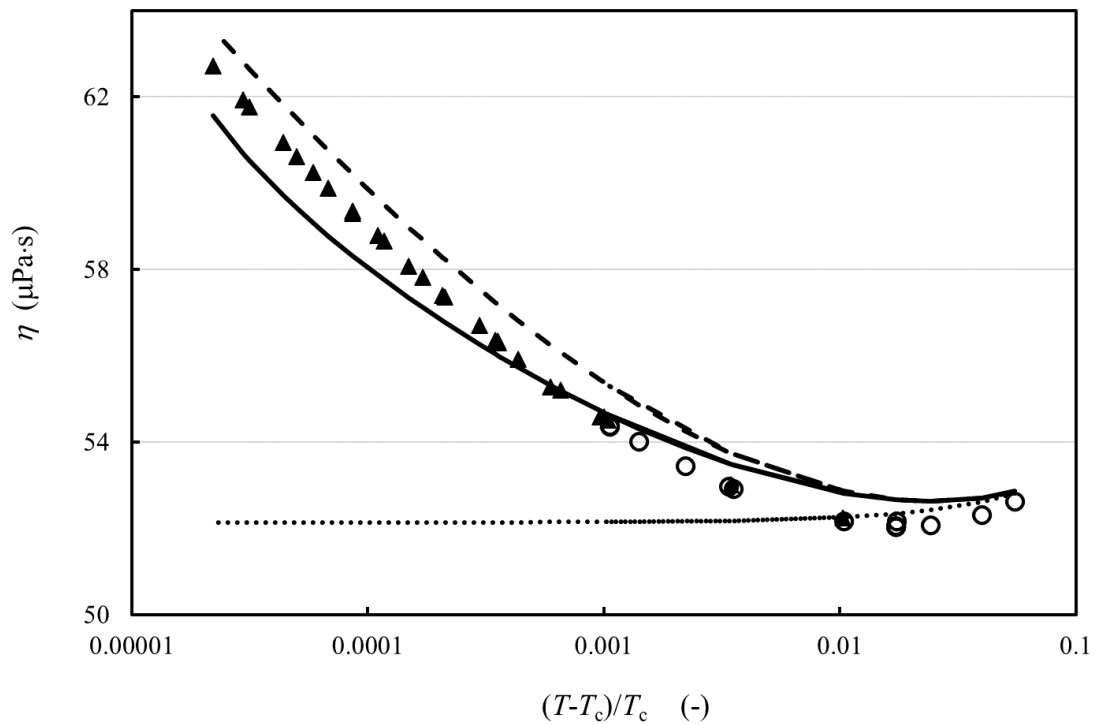


FIG. 6 Experimental viscosity data of Berg et al.[23] in the critical region: microgravity, ▲ and earth gravity, ○. Background viscosity shown as dotted line with solid line for critical enhancement based on Eqs. 7-14 with equation of state for the correlation length. Dashed line shows critical enhancement with power-law correlation length from Eq. (15).

It can be seen in Figure 6 that the critical enhancement calculated with Eqs. (7) to (14) based on the correlation length from the equation of state is a good representation of the critical enhancement of xenon. The deviations between the data of Berg et al.[23] relative to this model are shown in Figure 7. The data of Berg et al.[23] in the critical region are generally represented by the present model to within the uncertainty claimed by these authors of $\pm 1.6\%$. Deviations of up to 2% are found very close to the critical point where the correlation length calculated from the classical equation of state does not follow the expected power-law behavior.

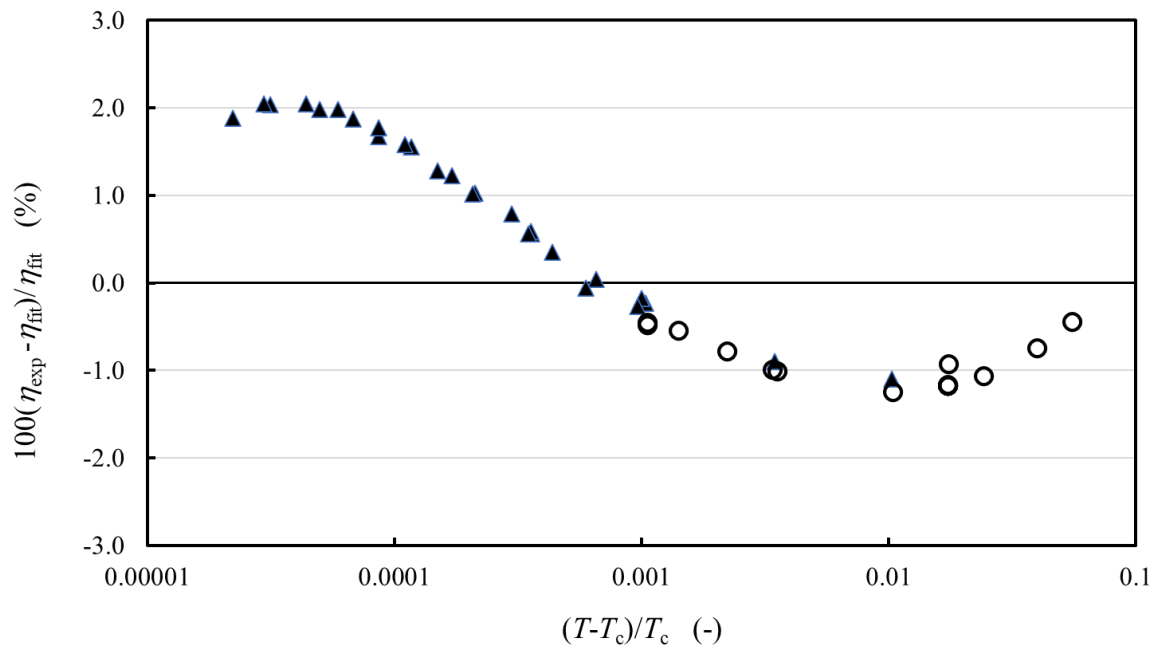


FIG. 7 Deviations between the viscosity data of Berg et al.[23] and the correlation including the critical enhancement from Eqs. (7) to (14) based on the equation of state.

3 Comparison with data

Table 6 summarizes comparisons of the primary data with the correlation. We have defined the percent deviation as $\text{PCTDEV} = 100(\eta_{\text{exp}} - \eta_{\text{fit}})/\eta_{\text{fit}}$, where η_{exp} is the experimental value of the viscosity and η_{fit} is the value calculated from the correlation. Thus, the average absolute percent deviation (AAD) is found with the expression $\text{AAD} = (\sum |\text{PCTDEV}|)/n$, where the summation is over all n points, the bias percent is found with the expression $\text{BIAS} = (\sum \text{PCTDEV})/n$. The average absolute percentage deviation of the fit for all primary data is 1.13%, with a bias of 0.03%. The percentage standard deviation of the correlation from the triple point up to 750 K and 86 MPa is 3.6% (at the 95% confidence level). The correlation behaves in a physically realistic manner at pressures up to 200 MPa and we feel the correlation may be extrapolated to this limit, although the uncertainty will be larger. Additional

experimental data at high pressures are necessary to validate the correlation or make improved correlations possible in the future.

Table 6. Evaluation of the xenon viscosity correlation for the primary data.

Investigators / Reference	AAD (%)	BIAS (%)
Lin et al. [32]	0.05	0.05
Vogel [26]	0.38	-0.38
May et al. [24]	0.03	0.03
Berg et al. [23]	1.19	0.24
Kestin et al. [34]	0.99	0.91
Kestin et al. [33]	0.74	0.65
Ulybin and Makarushkin [40]	0.79	-0.40
Goldblatt and Wageman [39]	1.23	1.23
Dawe and Smith [36]	0.52	-0.18
Clarke and Smith [37]	0.58	-0.55
Rigby and Smith [35]	1.35	-1.35
Trappeniers et al. [41]	3.44	3.24
Reynes and Thodos [42]	1.63	-0.90
Thornton [38]	0.67	-0.67
Entire data set	1.13	0.03

Fig. 8 shows the percentage deviations of all primary viscosity data of xenon, excluding the critical region data of Berg et al.[23], from the values calculated by Eqs. 1 - 6, as a function of temperature, while Figs. 9 and 10 show the same deviations but as a function of the pressure and the density. The deviations of the experimental data from the present correlation are within the uncertainty of the correlation with only a few exceptions. One point from the data set of Trappeniers et al. [41] at 298.135 K and 6.799 MPa is off scale and is not shown.

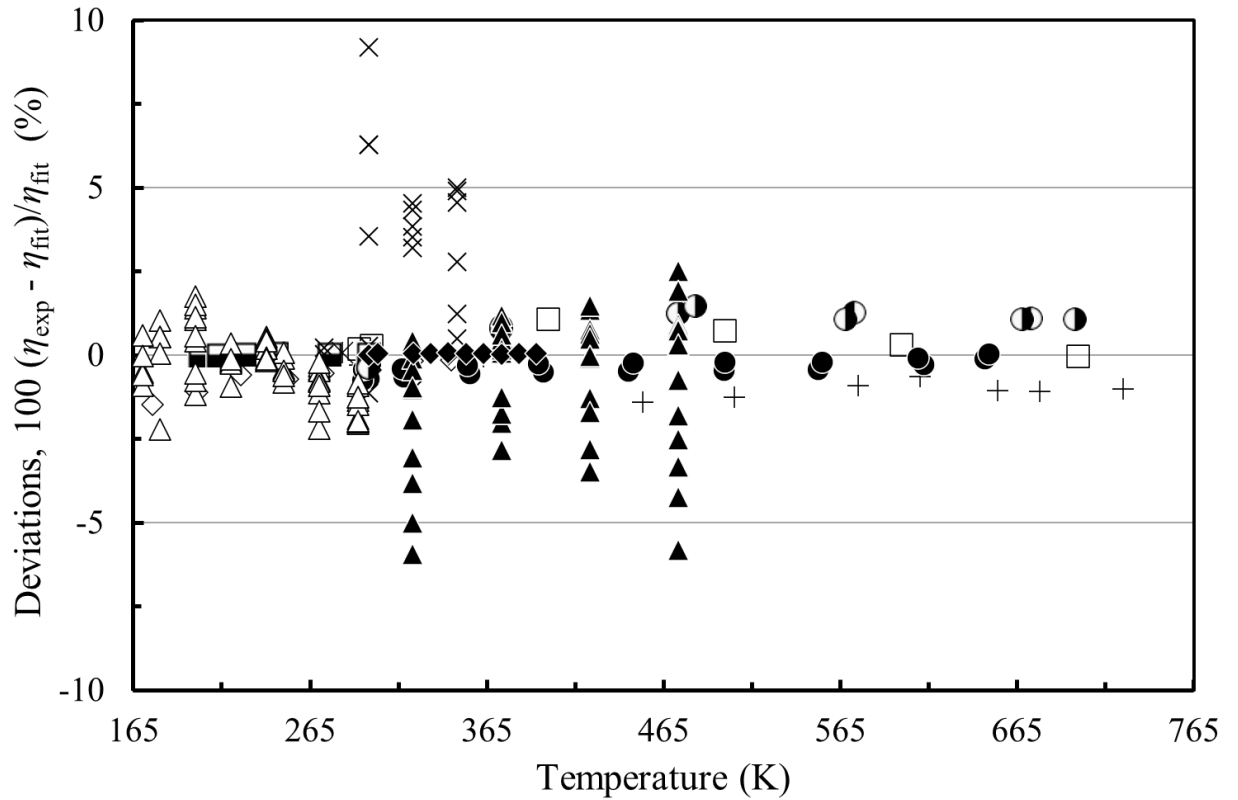


FIG. 8 Percentage deviations of primary experimental data of xenon from the values calculated by the present model as a function of temperature. Lin et al. [32] (\blacklozenge), Vogel [26] (\bullet), May et al. [24] (\blacksquare), Kestin et al. [33] (\bullet), Kestin et al. [34] (\bullet), Rigby and Smith [35] (+), Ulybin and Makarushkin [40] (Δ), Goldblatt and Wageman [39] ($*$), Dawe and Smith [36] (\square), Clarke and Smith [37] (\diamond), Trappeniers et al. [41] (\times), Reynes and Thodos [42] (\blacktriangle), and Thornton [38] (\circ).

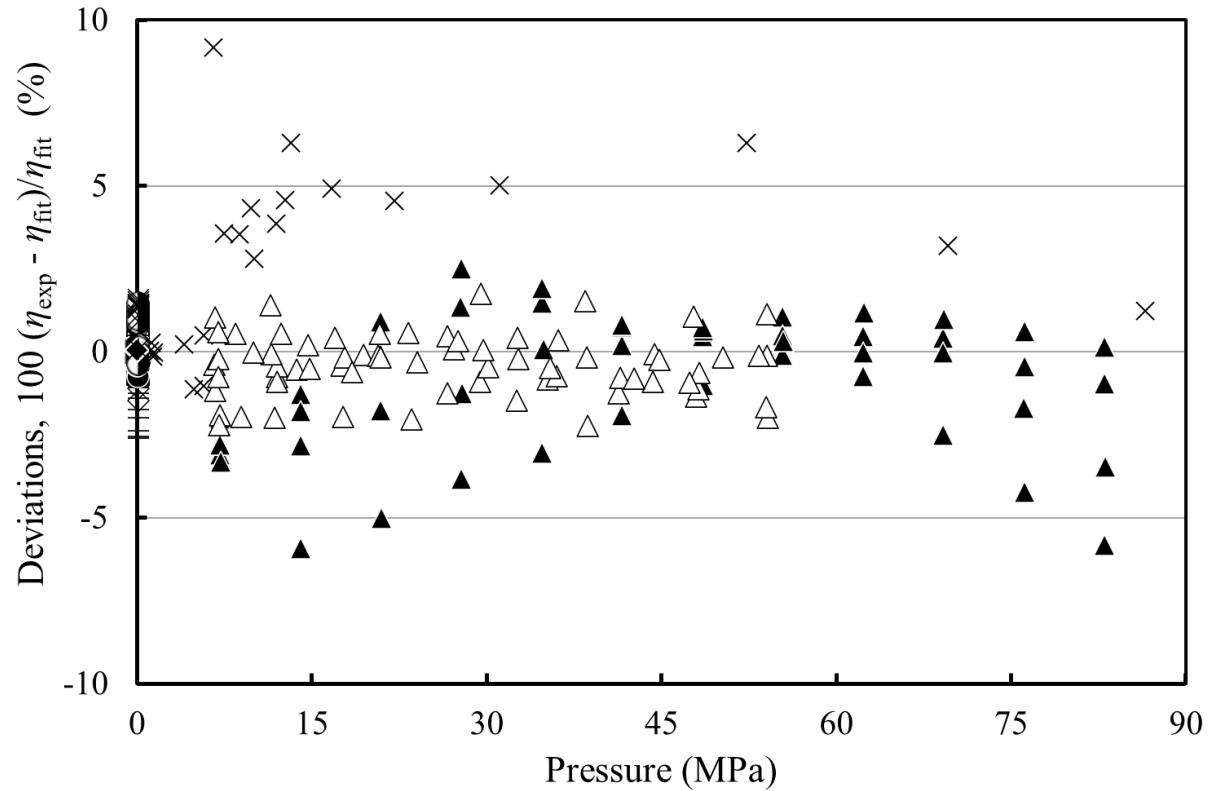


FIG. 9 Percentage deviations of primary experimental data of xenon from the values calculated by the present model as a function of pressure. Lin et al. [32] (\blacklozenge), Vogel [26] (\bullet), May et al. [24] (\blacksquare), Kestin et al. [33] (\ominus), Kestin et al. [34] (\bullet), Rigby and Smith [35] (+), Ulybin and Makarushkin [40] (Δ), Goldblatt and Wageman [39] (\ast), Dawe and Smith [36] (\square), Clarke and Smith [37] (\diamond), Trappeniers et al. [41] (X), Reynes and Thodos [42] (\blacktriangle), and Thornton [38] (o).

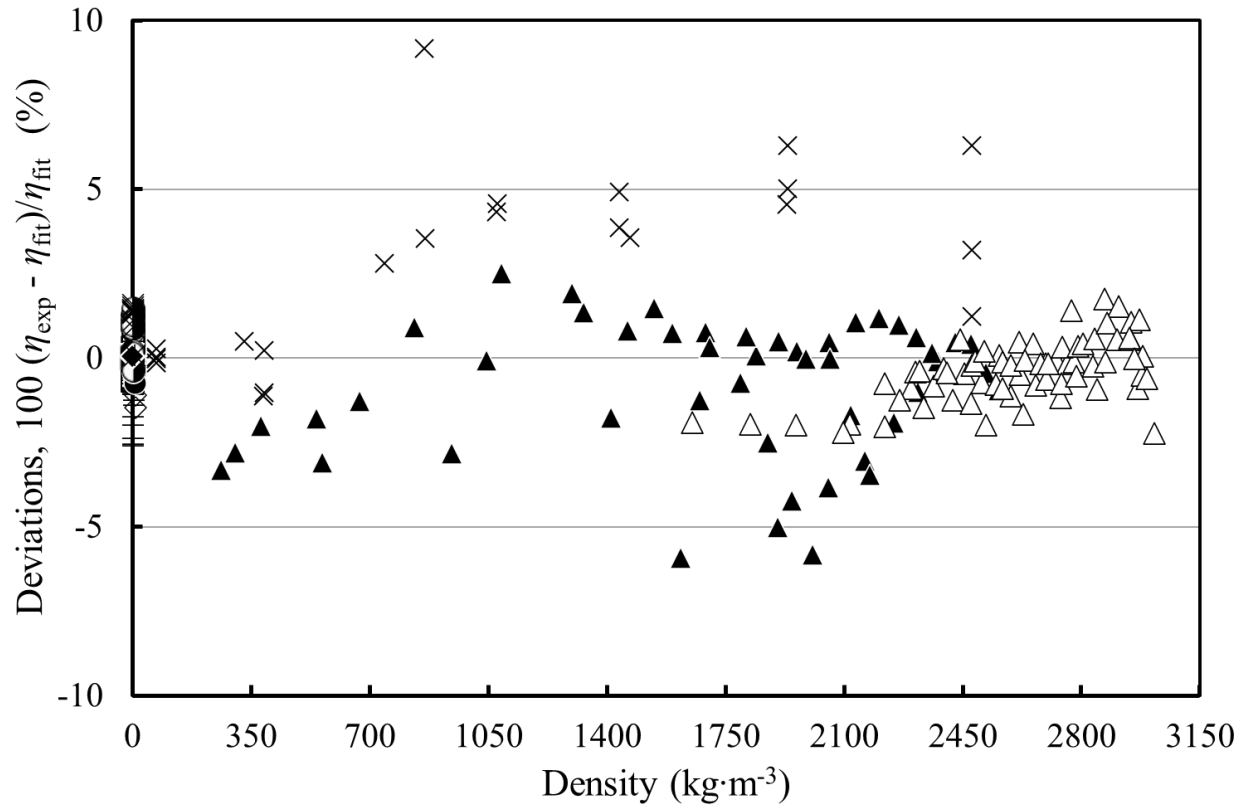
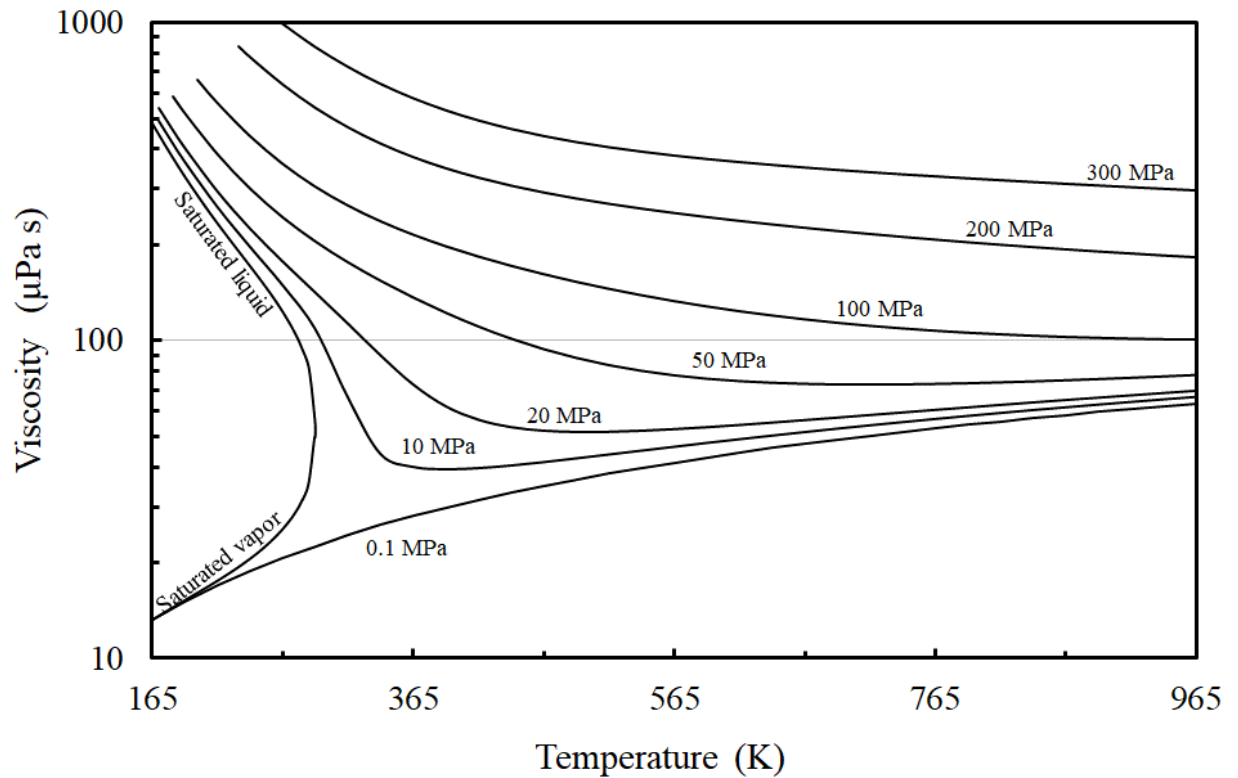


FIG. 10 Percentage deviations of primary experimental data of xenon from the values calculated by the present model as a function of density. Lin et al. [32] (\blacklozenge), Vogel [26] (\bullet), May et al. [24] (\blacksquare), Kestin et al. [33] (\bullet), Kestin et al. [34] (\bullet), Rigby and Smith [35] (+), Ulybin and Makarushkin [40] (Δ), Goldblatt and Wageman [39] (\ast), Dawe and Smith [36] (\square), Clarke and Smith [37] (\diamond), Trappeniers et al. [41] (X), Reynes and Thodos [42] (\blacktriangle), and Thornton [38] (o).

Table 7 shows the average absolute percent deviation (AAD) and the bias for the secondary data. Finally, Fig. 11 shows a plot of the viscosity of xenon as a function of the temperature for different pressures. The plot demonstrates the extrapolation behavior at pressures higher than 86 MPa, and at temperatures that exceed the 750 K limit of the equation of state.

Table 7 Evaluation of the xenon viscosity correlation for the secondary data.

Investigators / Reference	AAD (%)	BIAS (%)
Grisnik [43]	1.62	1.19
Malbrunot et al. [44]	11.28	11.28
Baharudin et al. [45]	5.28	5.28
Strumpf et al. [46]	7.71	7.70
Zollweg et al [47]	2.73	-2.67
Legros and Thomaes [48]	5.53	5.53
Kestin and Leidenfrost [49]	1.96	-1.96

**FIG. 11** Viscosity of xenon as a function of the temperature for different pressures.

4 Recommended Values

In Table 8, viscosity values are given along the saturated liquid and vapor lines, calculated from the present proposed correlations between (170 – 285) K, while in Table 9 viscosity values are given for temperatures between (200 – 750) K at selected pressures. Saturation pressure and saturation density values for selected temperatures, as well as the density values for the selected temperature and pressure, are obtained from the equation of state of Lemmon and Span [50]. The calculations are performed at the given temperatures and densities. For computer verification of values, the following points may be used for the given T, ρ conditions: $T = 300$ K, $\rho = 0$ kg m⁻³, $\eta = 23.1561$ μ Pa·s; $T = 300$ K, $\rho = 6.0$ kg·m⁻³, $\eta = 23.3186$ μ Pa·s; $T = 300$ K, $\rho = 2500.0$ kg·m⁻³, $\eta = 206.449$ μ Pa·s. For checking the critical enhancement, $T = 292.711322$ K, $\rho = 0$ kg m⁻³, $\eta = 22.6125$ μ Pa·s; $T = 292.711322$ K, $\rho = 1102.9$ kg m⁻³, $\eta = 52.82074$ μ Pa·s.

Table 8 Viscosity values of xenon along the saturation line, calculated by the present scheme.

T (K)	p (MPa)	ρ_{liq} (kg·m ⁻³)	ρ_{vap} (kg·m ⁻³)	η_{liq} (μ Pa·s)	η_{vap} (μ Pa·s)
170	0.13343	2908.8	12.88	442.32	13.56
190	0.34774	2768.4	31.19	326.28	15.19
210	0.75025	2614.9	64.37	248.25	17.00
230	1.4155	2441.5	120.1	193.12	19.19
250	2.4229	2235.4	212.1	150.75	22.14
270	3.8623	1962.2	376.6	113.51	26.93
285	5.3025	1607.3	655.3	81.276	35.30

Table 9 Viscosity values of xenon at selected temperatures and pressures, calculated by the present scheme.

p (MPa)	T (K)	ρ (kg·m ⁻³)	η (μPa·s)	p (MPa)	T (K)	ρ (kg·m ⁻³)	η (μPa·s)
0.1	200	8.032	15.80	50	200	2956.6	460.85
	250	6.372	19.57		250	2706.5	276.72
	300	5.291	23.31		300	2449.8	193.41
	350	4.526	26.96		350	2190.7	147.31
	400	3.956	30.51		400	1940.7	117.85
	450	3.514	33.93		450	1713.6	98.60
	500	3.161	37.23		500	1518.5	86.59
	550	2.873	40.42		550	1356.5	79.49
	600	2.633	43.49		600	1223.6	75.56
	650	2.430	46.46		650	1114.6	73.64
700	2.256	49.33	700	1024.1	72.97		
750	2.106	52.12	750	948.3	73.13		
10	200	2762.2	317.4	80	200	3056.9	577.06
	250	2375.5	176.2		250	2843.6	351.34
	300	1744.0	92.16		300	2634.4	249.56
	350	724.4	41.81		350	2431.1	196.21
	400	501.1	39.59		400	2237.8	163.37
	450	403.8	41.02		450	2058.5	140.81
	500	344.5	43.25		500	1896.0	124.61
	550	303.1	45.75		550	1751.2	112.93
	600	271.9	48.34		600	1623.5	104.61
	650	247.3	50.94		650	1511.4	98.79
700	227.2	53.54	700	1412.9	94.81		
750	210.4	56.10	750	1326.3	92.21		

5 Conclusions

A new wide-ranging correlation for the viscosity of xenon was developed based on critically evaluated experimental data and theoretical results. In the dilute-gas range, the correlation incorporates the very recent correlation of Xiao et al. [29, 30] with a quoted uncertainty of 0.2 %, while the initial-density dependence viscosity is based on the scheme proposed by Vogel et al. [53]. The residual term is based on a critically evaluated set of measurements. In the dilute-gas region the uncertainty is 0.2 %, while in all other cases it is 3.6 % (in the 95% confidence level). The correlation is valid for temperatures from

the triple-point temperature to 750 K, a limit imposed by the validity of the equation of state, while its pressure range extends to 86 MPa. The correlation behaves in a physically realistic manner at pressures up to 200 MPa and we feel the correlation may be extrapolated to this limit, although the uncertainty will be larger, and caution is advised. A critical enhancement term based on the data of Berg et al.[23] has also been included for the near-critical region but is not necessary for industrial applications.

Finally, it is worth saying that the new correlation is characterized by a lower uncertainty than previous correlations while at the same time covers the wide range of temperature and pressure of the available measurements.

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