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Thank you for your assistance.

# Accessing ratios of quantized resistances in graphene $p$ - $n$ junction devices using multiple terminals

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## ABSTRACT

The utilization of multiple current terminals on millimeter-scale graphene  $p$ - $n$  junction devices has enabled the measurement of many atypical, fractional multiples of the quantized Hall resistance at the  $\nu = 2$  plateau ( $R_H \approx 12\,906\ \Omega$ ). These fractions take the form  $\frac{a}{b}R_H$  and can be determined both analytically and by simulations. These experiments validate the use of either the LTspice circuit simulator or the analytical framework recently presented in similar work. Furthermore, the production of several devices with large-scale junctions substantiates the approach of using simple ultraviolet lithography to obtain junctions of sufficient sharpness.

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Graphene, composed of carbon atoms arranged in a two-dimensional honeycomb lattice, has been extensively studied for more than a decade, in part because of its excellent optical, mechanical, and electrical transport properties.<sup>1–4</sup> The quantum Hall effect (QHE) in graphene gives resistance values at  $\frac{1}{(4n+2)}\frac{h}{e^2}$ , where  $n$  is an integer,  $h$  is the Planck constant, and  $e$  is the elementary charge. Graphene  $p$ - $n$  junctions ( $pn$ Js), which are suitable for one to explore transport in the QHE,<sup>5–18</sup> enable one to access various multiples and fractions of the von Klitzing constant. These types of graphene devices also have additional applications in electron optics,<sup>19–22</sup> photodetection,<sup>23–27</sup> and quantum Hall resistance standards.<sup>28–38</sup>

For clarity, a  $pn$ J device contains some form of interface at which a positively doped and a negatively doped region meet. For graphene, whose Fermi level can be electrically or chemically

modulated, such an interface can be effectively one-dimensional, allowing edge state electrons to tunnel from one region to the other. This behavior results in the observation of quantized longitudinal resistances due to the presence of the junction. Typically, these devices are of sub-millimeter sizes due to constraints on top-gating. One motivation for pursuing large-scale  $pn$ J devices is to determine the feasibility of using quantum transport across the junctions to access different quantized values of resistance, as shown in previous studies.<sup>39–41</sup> One first major hurdle is to fabricate large-scale devices without the need for top-gating, since such techniques become more complicated as the device incorporates more elements. Although extensive analyses exist on Landauer–Büttiker edge state equilibration,<sup>5–8,42–46</sup> creating a  $pn$ J device capable of accessing different plateaus with top gates is a difficult task. Instead, one approach to accessing different quantized values is to incorporate multiple

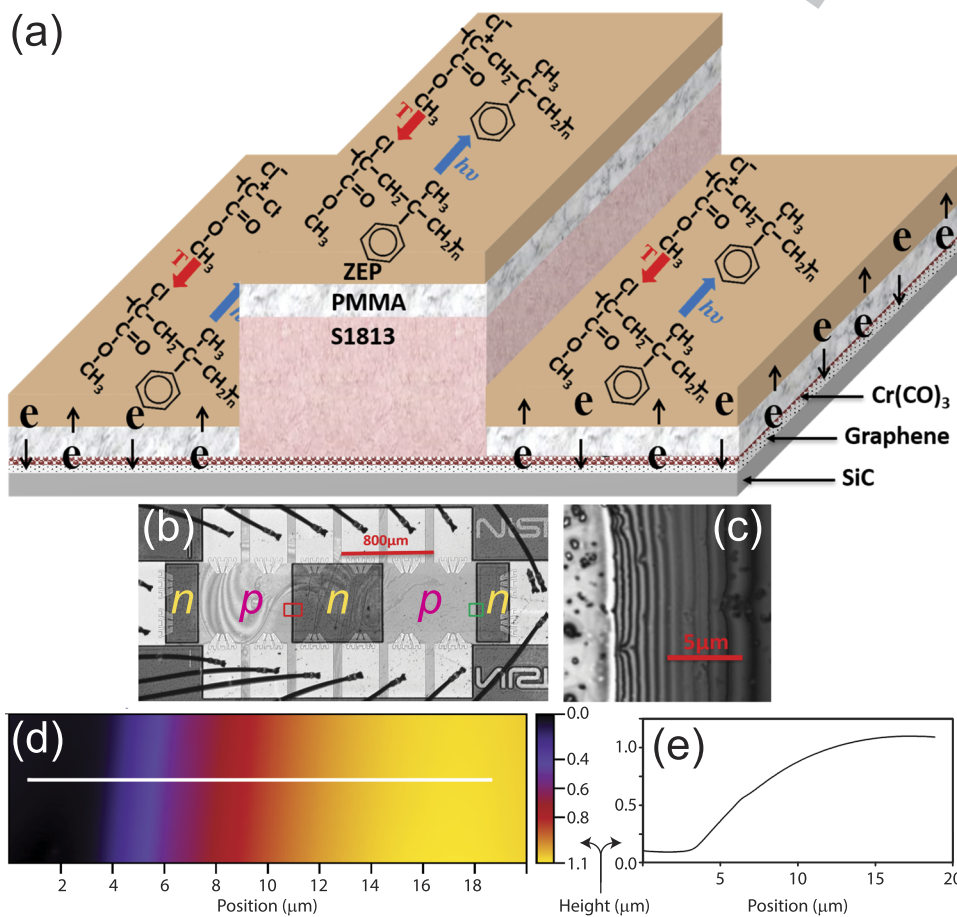
current terminals, which opens the parameter space within which  $pnj$  devices are able to be operated.

For millimeter-scale device fabrication, epitaxial graphene (EG) is grown to accommodate device size, but the issue of processing the correspondingly large  $pnj$ s was not trivial, as shown in previous work.<sup>47</sup> This work elaborates on further efforts involving the use of standard ultraviolet photolithography (UVP) and ZEP520A to build  $pnj$ s having widths smaller than 200 nm. Devices were verified via quantum Hall transport measurements and LTspice current simulations,<sup>48</sup> and multiple current terminals and configurations were used to test the viability of the simulations as well as the quality of the devices. Furthermore, recently reported analytical methods were also used to predict atypical fractions of the quantized Hall resistance,  $R_H$ , that would become experimentally accessible depending on the configuration of the current terminals.<sup>49</sup> These experiments also serve as supporting evidence on the validity of those analytical methods, which provide easily implementable algorithms for determining effective quantized resistances in complicated  $pnj$  circuits.

Simulations for the  $pnj$  devices were performed with the analog electronic circuit simulator LTspice in an identical manner as demonstrated for similar devices in other works.<sup>47,49–51</sup> The circuit

uses both  $p$ -type and  $n$ -type  $k$ -terminal quantum Hall elements, designated as either having ideal counterclockwise (CCW) or clockwise (CW) edge state current flow. EG on SiC was fabricated into  $pnj$  devices after the growth at a temperature of 1900 °C. First, chips were diced from 4H-SiC(0001) wafers (CREE)<sup>48</sup> and chemically cleaned with a 5:1 diluted solution of hydrofluoric acid and deionized water. Just prior to growth, chips were processed with AZ5214E to utilize polymer-assisted sublimation.<sup>52</sup> Finally, after placing the chips on a polished graphite substrate (SPI Glas 22)<sup>50</sup> silicon-face down, the growth occurred under an ambient argon environment at 1900 °C with a graphite-lined resistive-element furnace (Materials Research Furnaces, Inc.).<sup>48</sup> The corresponding heating and cooling rates of the furnace were about 1.5 °C/s.

Once grown, EG was assessed with confocal laser scanning, optical, and atomic force microscopy (AFM).<sup>53</sup> Images acquired from these techniques are provided in Fig. 1, which confirmed that homogeneous monolayer EG had successfully covered millimeter-scale areas (see the supplementary material for additional AFM images). Next, using Pd and Au as protective layers against organic contamination, photolithographic processes were performed, details of which may be found in other works.<sup>31,47</sup> Once each Hall bar device was completed, it underwent  $\text{Cr}(\text{CO})_3$  functionalization to reduce



**FIG. 1.** (a) An illustration of the surface of an EG  $pnj$  device. The photoresist S1813 was deposited and lithographically processed on specific regions where  $n$ -type doping was preferred. The molecule in ZEP520A is shown to clarify the electron acceptor as the photoresist is exposed to ultraviolet light.  $\text{Cr}(\text{CO})_3$  was used to stabilize the electron density. (b) A confocal microscope image acquired for the full device after wire bonding, with the darker region indicating the desired  $n$ -type regions. (c) A magnification of the small green box in (b) for a scale of the order of 5 μm. Oxidized residue from the  $\text{Cr}(\text{CO})_3$  deposition takes the form of visible black specs. (d) and (e) show both the two-dimensional and one-dimensional height profiles, respectively, with the one-dimensional profile represented as a white line in (d) and the two-dimensional profile acquired within the red box in (b).

123 the electron density to approximately  $10^{10} \text{ cm}^{-2}$ .<sup>54–58</sup> The major final  
 124 steps included the deposition of S1813 photoresist as a spacer layer  
 125 for intended *n*-type regions, PMMA/MMA photoresist as an addi-  
 126 tional spacer, and ZEP520A as a photoactive layer, as described in  
 127 the literature.<sup>47,59</sup> Uniformity is also verified with Raman spectra (see  
 128 the supplementary material).

129 Although AFM images suggest a sloped S1813 spacer layer,  
 130 preservation of the *n*-type regions can still be accomplished with  
 131 thicknesses of the order of 100 nm.<sup>49</sup> Furthermore, the upper bound  
 132 of the junction width resulting from these photolithographic pro-  
 133 cesses was measured to be approximately 200 nm in another work,  
 134 rendering them of sufficient sharpness to accommodate edge-state  
 135 propagation.<sup>49</sup> Ultraviolet (UV) light, with a wavelength of 254 nm,  
 136 was used to realize *p*-type doping in regions without S1813. The lon-  
 137 gitudinal resistivity was monitored during periods of UV exposure,  
 138 and additional information and data on this process are found in the  
 139 supplementary material.

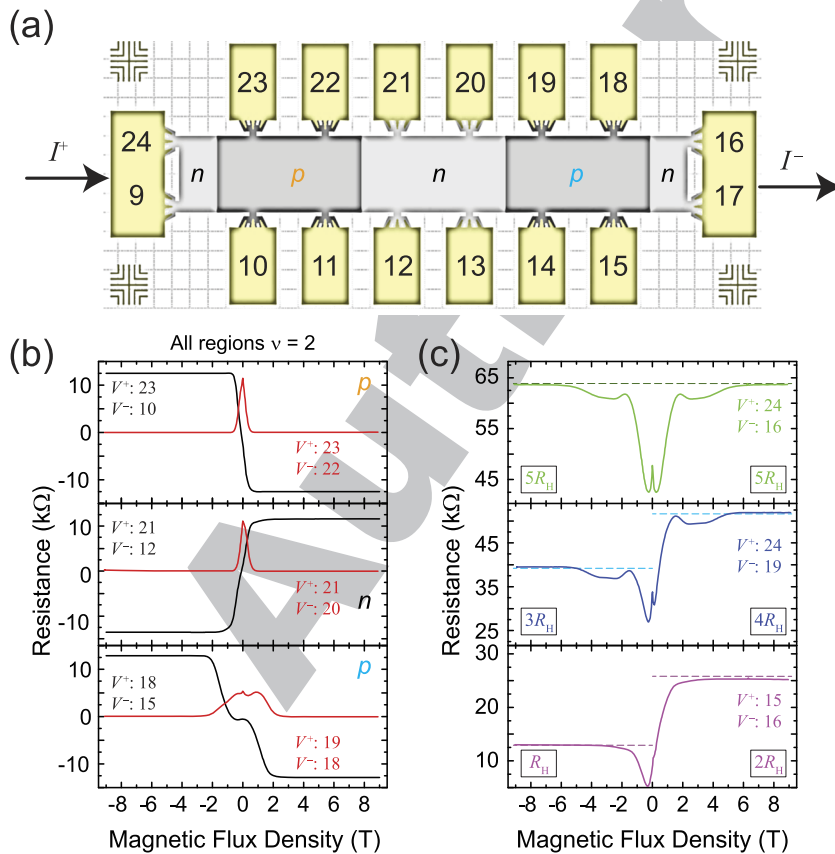
140 Completed four-junction devices, like the one shown in  
 141 Fig. 1(c), were measured with the traditional methods to verify  
 142 that regions exhibited resistance quantization. This type of device  
 143 is shown in Fig. 2(a). Electrical contact pads are numbered based on  
 144 the measurement system used to provide the corresponding mea-  
 145 surements in (b) and (c). Traditional longitudinal and Hall  
 146 measurements were acquired at 1.6 K and  $\pm 9$  T, with the results shown  
 147 in Fig. 2(b) as black and red curves, respectively. With proper UV

148 exposure, regions without the S1813 spacer layer are subject to *p*  
 149 doping, and after sufficient exposure time, they become set as *p*-type  
 150 regions.

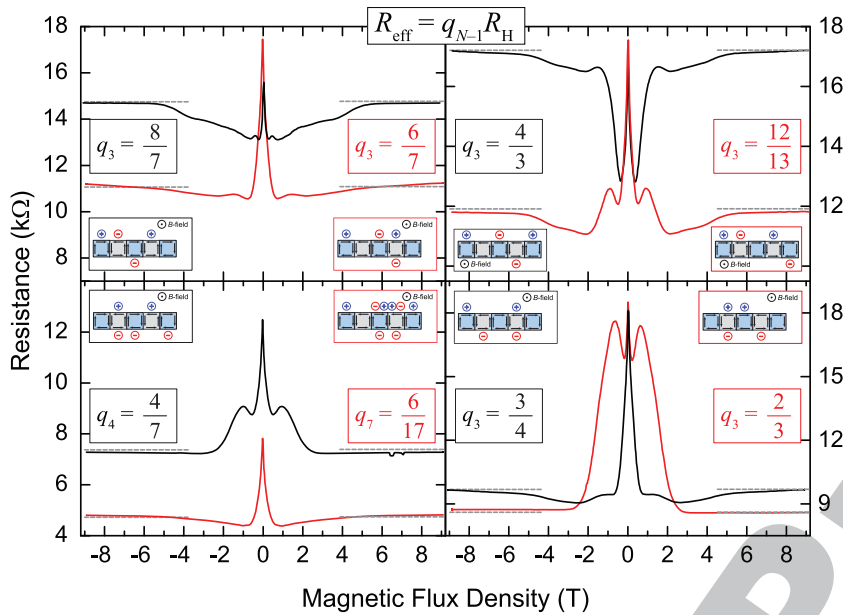
151 The resulting *pn*Js were found to be of sufficient narrowness  
 152 to accommodate dissipationless edge-state propagation.<sup>47</sup> However,  
 153 to further verify that the entire device was functional, voltage mea-  
 154 surements were performed along the length of the device, bearing  
 155 in mind the formation of the device’s so-called hot spots, as shown  
 156 pictorially in Ref. 40. In Fig. 2(c), the plotted resistances further sup-  
 157 port the idea that millimeter-scale *pn*Js can be successfully fabricated  
 158 with standard UV lithography.

159 A recent formulation for using multiple terminals on a *pn*J  
 160 device as the only resistive elements of a circuit has established a  
 161 mathematical way of predicting the effective quantized resistance of  
 162 that circuit.<sup>49</sup> Essentially, a single current source can inject current  
 163 into an arbitrary number of terminals—likewise for the drain port of  
 164 the current source. The voltage difference of the whole circuit, and  
 165 by extension the effective quantized resistance  $R_{\text{eff}} = q_{N-1}R_H$ , can  
 166 then be measured between just after the current source starts and just  
 167 before the drain of the current source terminates. The coefficient of  
 168 effective resistance (CER) is labeled *q* and represents a device config-  
 169 uration containing *N* total terminals that are used (either as a source  
 170 or as a drain).

171 Eight different configurations were measured, and their effec-  
 172 tive circuit resistances are plotted in Fig. 3. Furthermore, two meth-

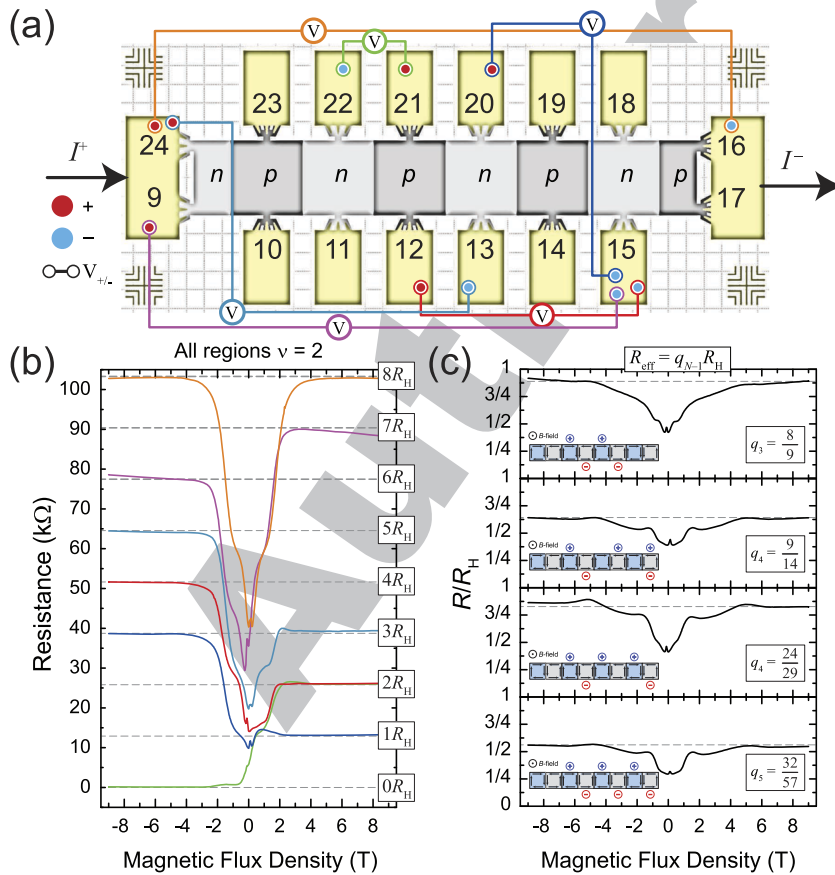


173 FIG. 2. (a) A four-junction device illustration with numbers corresponding to  
 174 wired connections on a 32-pin leadless chip carrier, with the electron flow enter-  
 175 ing from the right-side contact (drain) and with the source on the left side. A cur-  
 176 rent of 1  $\mu\text{A}$  was applied for all mea-  
 177 surements. Darker and lighter gray col-  
 178 ors indicate *p*-type and *n*-type regions,  
 179 respectively. The three middle regions  
 180 are tested to check traditional Hall re-  
 181 sistance curves, with orange and cyan *p*  
 182 labels matching those seen in (b). (b)  
 183 The longitudinal and Hall resistances  
 184 were measured from 9 T to  $-9$  T at  
 185 1.6 K and are represented by red and  
 186 black curves, respectively. Pin labels  
 187 are also provided. (c) Integer multiples  
 188 of  $R_H$  (from 1 to 5) were measured  
 189 across varying lengths of the device  
 190 to ensure device functionality. Dotted  
 191 lines are provided as a visual guide to  
 192 compare exact quantized values. All  
 193 regions were on the  $\nu = 2$  plateau.  
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**FIG. 3.** Multiple-terminal configurations have been measured and their effective circuit resistances are plotted in the four panels. Three of the four panels contain four-terminal configurations (two sources and two drains), whereas the panel on the lower left corner uses a five-terminal and an eight-terminal configuration. The latter panel, when compared with the calculated and simulated value in dotted gray lines, provides some evidence that the CER formulation is valid for larger numbers of used terminals. All panels contain the calculated and simulated value in dotted gray lines (valid for sufficiently high magnetic flux density), and for all cases, the calculated and simulated results agree with each other. The insets of each panel have colored perimeters corresponding to the curve of the same color and illustrate the four-junction device and its edge-state current flow abstractly. The blue plus and red minus signs indicate source and drain terminals, respectively.

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**FIG. 4.** (a) A seven-junction device illustration with numbers corresponding to the same measurement system is shown using a measurement current of  $1 \mu\text{A}$ . Darker and lighter gray colors indicate  $p$ -type and  $n$ -type regions, respectively. Each measurement pair is color-coded for easy comparison to its corresponding data. (b) The resistance is plotted for each of the voltage measurement pairs in (a) with the same color-coding used to match the illustration. The dotted gray lines represent the exact values of the multiples of  $R_H$ . All regions were on the  $\nu = 2$  plateau. (c) Several new configurations were measured and compared with both simulations and the CER formulation, with the latter two in exact agreement. Thus, both theoretical values are represented by the same gray dotted line in each of the four panels. On the bottom left of each graph panel, the illustrated device is shown with the corresponding locations of sources (blue plus symbol) and drains (red minus symbol) along the device. Voltages were measured from the point before the sources split to the point after the drains rejoin, yielding the CERs of each configuration.

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ods were used to predict the expected CERs of the circuit—the LTspice simulator and the CER formulation. Both methods agreed exactly and are plotted as gray dotted lines for each of the eight configurations. The crucial formula used to mathematically predict the expected CERs<sup>49</sup> is as follows:

$$q_{N-1}(n_{N-1}) = \frac{q_{N-2}(n_{N-1} + 1)}{n_{N-1} + \frac{q_{N-2}}{q_{N-1}}}. \quad (1)$$

The CERs calculated in Fig. 3 include the following:  $\{\frac{6}{7}, \frac{8}{7}, \frac{12}{13}, \frac{4}{3}, \frac{6}{17}, \frac{4}{7}, \frac{3}{4}, \frac{2}{3}\}$ . Details on how to proceed with the calculation are well-documented in Ref. 49, and additional examples for some of the configurations in this manuscript are found in the [supplementary material](#).

To demonstrate how increasingly complex calculations can yield atypical CERs, devices containing seven  $pn$ s were fabricated as shown in Fig. 4(a). Although even more  $pn$ s can be placed along the 2 mm length of the device, their number was limited by the preference of accessing each region with an electrical contact for proof of concept. Figure 4(a) shows voltage leads of varying color that were used for determining the resistance curves and by extension the CERs [Fig. 4(b)].

Sufficient quantization was seen for the more traditional cases of measuring the resistance across parts of the device while the source and drain are at the farthest terminals. All integer multiples of  $R_H$  between 1 and 8 were accessible in this characterization, warranting further measurements with multiple terminals. In Fig. 4(c), four configurations were measured using different numbers of total terminals. The top panel, using four terminals as illustrated in the inset, yielded data that were then compared to the predicted CER of  $q_3 = \frac{8}{9}$ . The two middle panels used five terminals and were compared with their corresponding predicted values of  $q_4 = \frac{9}{14}$  and  $q_4 = \frac{24}{29}$ . In the bottom panel, the six-terminal configuration was measured and compared with its corresponding prediction of  $q_5 = \frac{32}{57}$ . For the sake of clarity and as an additional tutorial, this fourth case is calculated in more detail in the [supplementary material](#). Overall, such devices and their CERs can be measured for many configurations of similar or greater complexity. Moreover, desired, user-specific CERs can be reversed engineered into a corresponding configuration.

In conclusion, this work pursued further efforts involving  $pn$  devices fabricated from EG on SiC with junction widths sufficiently narrow to observe usual edge-state propagation. By configuring an experimental setup to include multiple sources and drains, various atypical quantized resistances became accessible and matched predicted values based on LTspice simulations. Additionally, recently reported analytical methods were also used to support the predicted values of the same atypical fractions of  $R_H$ . The results demonstrate that  $pn$ s have the potential to bring scalable resistance values as well as reinforce the validity of the aforementioned CER formulation, which provides a simple algorithm for determining the effective quantized resistances in  $pn$  circuits.

See the [supplementary material](#) for the details on UV exposure and for additional calculations.

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# Supplementary Material: Accessing ratios of quantized resistances in graphene $p$ - $n$ junction devices using multiple terminals

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## Contents

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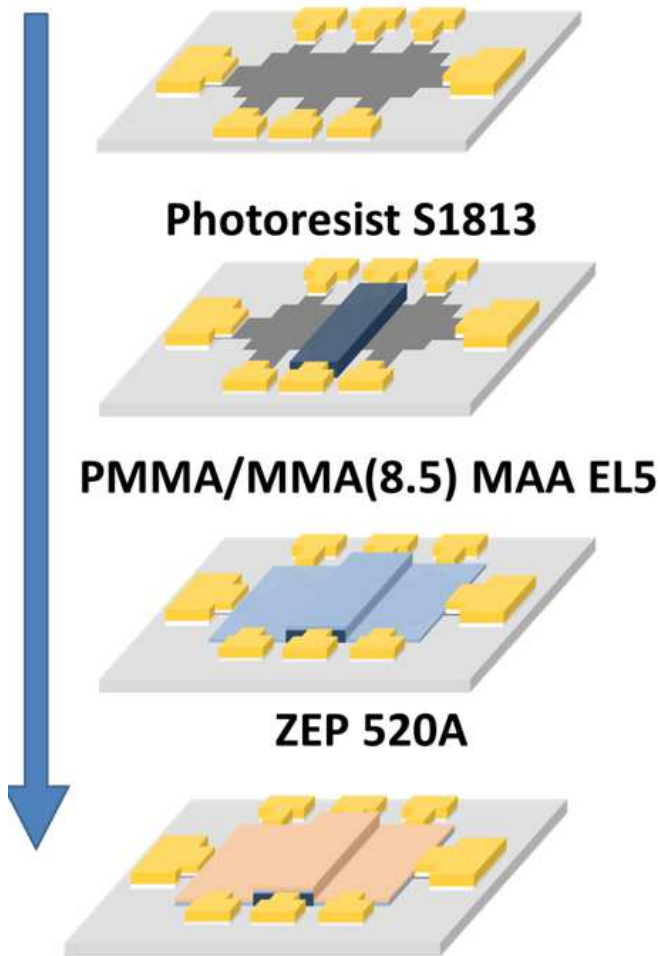
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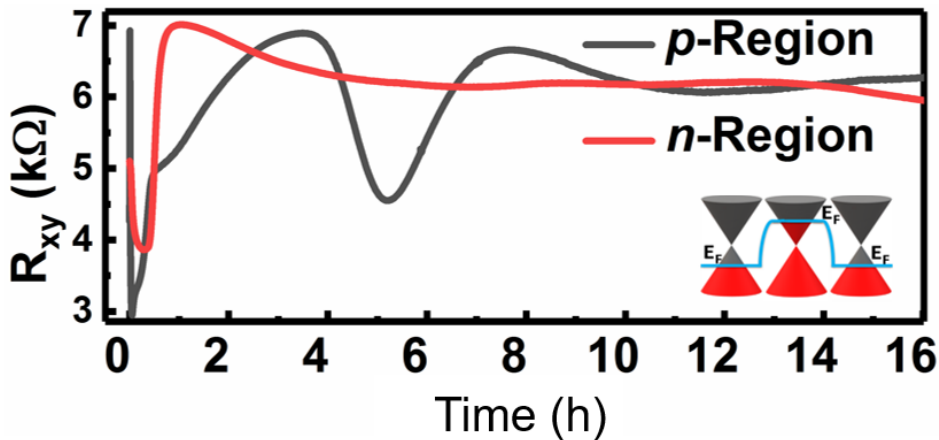
## 1. Device fabrication and UV exposure information

Devices underwent additional fabrication steps after unmodified Hall bar devices were functionalized with  $\text{Cr}(\text{CO})_3$ . The steps are listed below, with the full process illustrated in Fig. 1-SM:<sup>6</sup>

1. Spin photoresist at 5000 rpm for 1 min (acceleration: 5000 rpm/s). Photoresist composed of 75 % electronic-grade propylene glycol monomethyl ether acetate, 15 % mixed cresol novolak resin, and 10 % diazo photoactive compound (sold commercially as S1813 from The Dow Chemical Company).
2. Bake chips at 115 °C for 1 min.
3. Expose to ultraviolet light (365 nm) for 5 seconds, using a photomask designed to expose only the central region of the device, as in Figure 4 (other designs shown later). Parameters were measured on a high-precision mask and bond aligner (sold commercially as the Suss MA6 from Suss Microtec). {1130 W; WEC = cont.; Vacuum mode: 10 s / 30 s / 15 s; Al-gap = 15  $\mu\text{m}$ ; Dosage = 100 mJ}.
4. Use solution of 97 % water, 2.3 % tetramethylammonium hydroxide, and 0.7 % polyglycol (commercially sold as MF-26A Developer from The Dow Chemical Company), for 1 min to remove exposed region.
5. Bake chips at 200 °C for 5 min.
6. Spin solution of 95 % ethyl lactate and 5 % Poly(methyl methacrylate/methacrylic acid) as a spacer layer (sold commercially as EL6 from The Dow Chemical Company). Thickness of this photoresist should be between 50 nm to 100 nm (or less). Spin rate is 5000 rpm (acceleration of 5000 rpm/s).
7. Bake chips at 170 °C for 1 min.
8. Spin photoresist at 4000 rpm for 1 min to get a desired thickness between 300 nm and 400 nm. Photoresist composed of 89 % anisole and 11 % methyl styrene / chloromethyl acrylate copolymer (sold commercially as ZEP 520A from Zeon Chemicals L. P.).
9. Bake chips at 170 °C for 1 min.
10. Expose chips to 254 nm ultraviolet light for approximately 15 hours to activate the *p*-type regions. This time can be altered based on distance from the sample.
11. Other device regions should be inherently *n*-type. Level of doping can be adjusted by annealing.
12. UV data shown in Figure 2-SM.



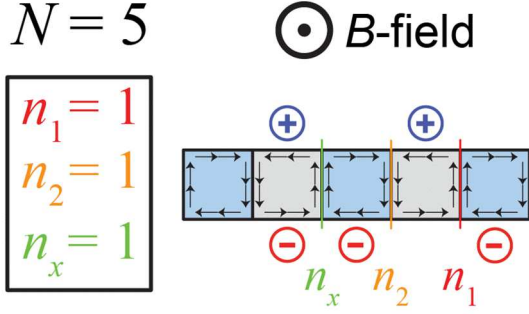
**Figure 1-SM.** A typical Hall bar device, after functionalization, is prepared with various polymers to enable the eventual adjustment of *p*-type and *n*-type regions.



**Figure 2-SM.** Data of an example UV exposure session. As expected, the *n*-region, protected by a spacer layer of S1813, does not change much with time (initial transient effects aside). The *p*-region does shift after crossing the Dirac point around 7 h to 8 h. The dip at 5.5 h is the result of competing effects from the UV treatment and the device heating due to the UV bulb.

## 2. Example calculations

Calculations are provided below for three cases presented in the main text (Figs. 3-SM, 4-SM, 5-SM).



**Figure 3-SM.** The calculation for an example configuration from the main text is provided below. This  $N = 5$  non-alternating configuration has its  $n_j$  terms assigned according to the guidelines in Ref. [1].

Once the  $n_j$  terms have been assigned, the calculation may begin. Since this is a non-alternating system, the condition of edge state cancellation along the junction marked in green in Fig. 3-SM allows us to treat the whole system as two smaller circuits in parallel. The “unit” terminal on the left gives a coefficient of effective resistance (CER) of 1. For the right branch, as described in Ref. [1], the use of the following equation is warranted:

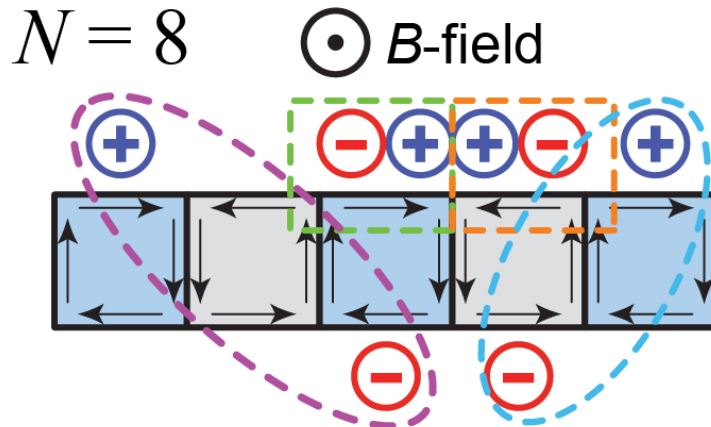
$$q_{N-1}(n_{N-1}) = \frac{q_{N-2}(n_{N-1} + 1)}{n_{N-1} + \frac{q_{N-2}^{(0)}}{q_{N-1}}}$$

(A1)

With  $n_1 = 1$ , we use the linear form of Eq. (A1), which is  $q_2 = (n_1 + 1)$ .  $q_1 = 2$ , and that brings us to  $n_2 = 1$ . If we apply the iteration in Eq. (A1) again:

$$q_2(n_2) = \frac{q_1(n_2 + 1)}{n_2 + \frac{q_1^{(0)}}{q_2}} = \frac{2(1 + 1)}{1 + \frac{2}{1}} = \frac{4}{3}$$

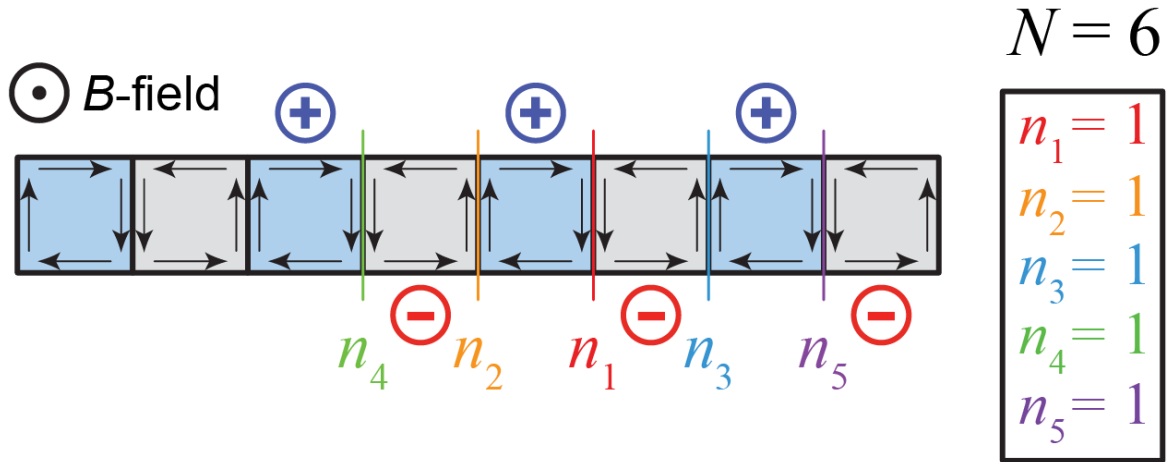
In the main text, the term  $q_2^{(0)}$  was not directly addressed since its explanation is provided in Ref. [1]. With our two branches assigned, we can get our final CER as  $(\frac{1}{1} + \frac{3}{4})^{-1} = \frac{4}{7}$ .



**FIG. 4-SM.** The calculation for this  $N = 8$ , non-alternating, example configuration from the main text is provided below. Dotted colored lines indicate the terminals in the various parallel circuits.

Since the next example is also a non-alternating system, the condition of edge state cancellation along various junctions allows us to demarcate four distinct parallel circuits. In Fig. 4-SM, two “unit” terminals in green and orange dotted lines give CERs of 1. The dotted blue and purple configurations are also effectively  $N = 2$  systems with the purple dotted-lined system having  $n_1 = 2$  and the blue dotted-lined system having  $n_1 = 1$ . If one sums all these branches in parallel, then the CER is:

$$\left(\frac{1}{1} + \frac{1}{1} + \frac{1}{3} + \frac{1}{2}\right)^{-1} = \frac{6}{17}.$$

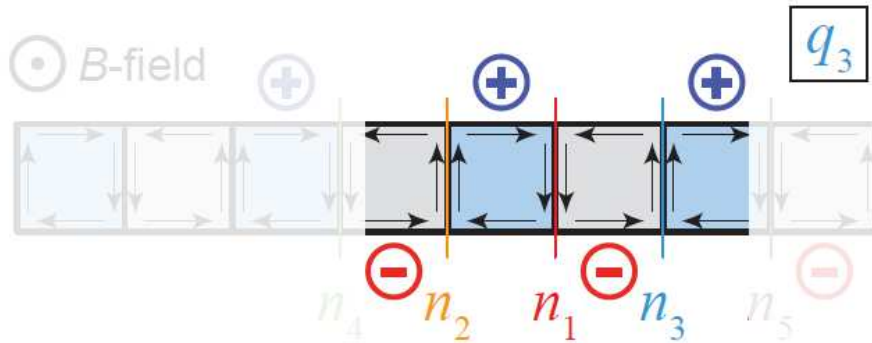


**FIG. 5-SM.** The calculation for this  $N = 6$  alternating configuration from the main text is provided below. The  $n_j$  terms have been assigned according to the guidelines in Ref. [1].

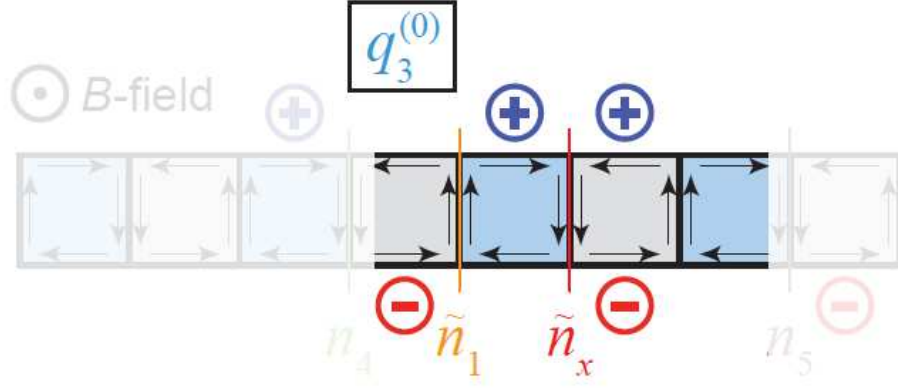
This calculation will be the most involved of the examples. After the  $n_j$  terms have been assigned according to the guidelines in Ref. [1], one can begin using Eq. (A1) to begin the iterative algorithm. Since  $n_1 = 1$ , one obtains  $q_2 = (n_1 + 1) = 2$ . Next, with  $n_2 = 1$ :

$$q_2(n_2) = \frac{q_1(n_2 + 1)}{n_2 + \frac{q_1}{q_2^{(0)}}} = \frac{2(1 + 1)}{1 + \frac{2}{1}} = \frac{4}{3}$$

Then, with  $n_3 = 1$ , approaching the next iteration to get  $q_3$  (see Fig. 6-SM) becomes slightly more difficult since the term  $q_3^{(0)}$  needs evaluation.



**FIG. 6-SM.** For subsequent iterations of the calculation for the configuration in Fig. 5-SM, one must focus on smaller subset configurations to determine  $q_5$  mathematically. Here,  $q_3$  is dependent on the term  $q_3^{(0)}$ , which is the CER for the limiting case where  $n_3 = 0$  (see Fig. 7-SM).

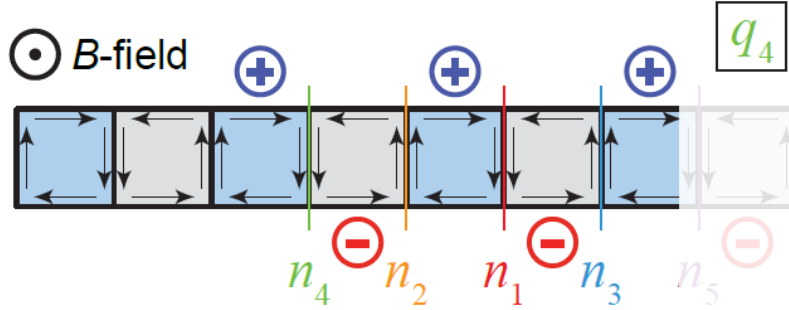


**FIG. 7-SM.** Evaluation for  $q_3^{(0)}$  is easier to accomplish with this visual guide. For the limiting case where  $n_3 = 0$  (where  $n_3$  is defined in Fig. 6-SM), a “new” configuration must be evaluated. New parameters have been labeled in orange and red. This configuration contains a unit terminal on the right that is isolated from the left branch defined by the parameter  $\tilde{n}_1$ . Therefore,  $q_3^{(0)} = \left(\frac{1}{1} + \frac{1}{2}\right)^{-1} = \frac{2}{3}$ .

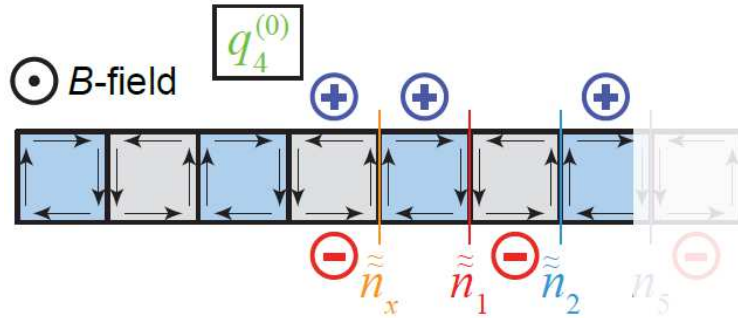
From Fig. 7-SM, we get  $q_3^{(0)} = \frac{2}{3}$  since the first parallel branch (unit terminal on right) gives a CER of 1 and the left parallel branch gives a CER of 2. This allows us to get  $q_3$ :

$$q_3(n_3) = \frac{q_2(n_3 + 1)}{n_3 + \frac{q_2^{(0)}}{q_3}} = \frac{\frac{4}{3}(1 + 1)}{1 + \frac{4/3}{2/3}} = \frac{8}{9}$$

The next iteration continues with  $q_4$ , where we evaluate the CER of the entire circuit shown in Fig. 8-SM.



**FIG. 8-SM.** Evaluation continues with  $q_4$ , where this five-terminal configuration must be solved before continuing. The formula contains the term  $q_4^{(0)}$ , which must first be evaluated before  $q_4$  can be solved.

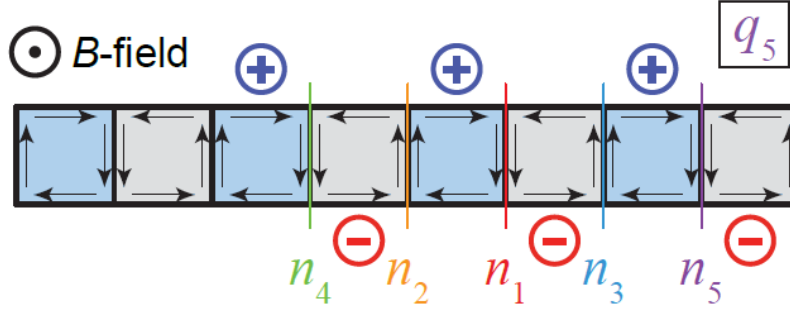


**FIG. 9-SM.** Evaluation for  $q_4^{(0)}$  requires  $n_4 = 0$  (where  $n_4$  is defined in Fig. 8-SM), giving us a “new” configuration to solve here. This configuration contains a unit terminal on the left that is isolated from the right branch defined by the parameters (double-tilde)  $\tilde{n}_1$  and  $\tilde{n}_2$ .

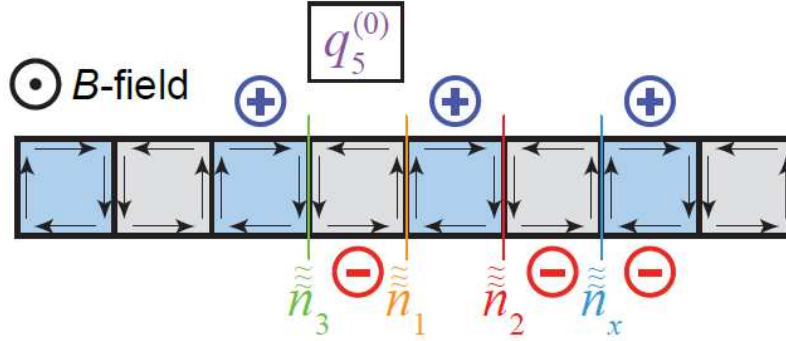
In Fig. 9-SM,  $q_4^{(0)} = \frac{4}{7}$  since it is numerically identical to Fig. 3-SM. This allows us to get  $q_4$ :

$$q_4(n_4) = \frac{q_3(n_4 + 1)}{n_4 + \frac{q_3}{q_4^{(0)}}} = \frac{\frac{8}{9}(1 + 1)}{1 + \frac{8/9}{4/7}} = \frac{16}{23}$$

The final iteration ends with  $q_5$ , where we evaluate the CER of the entire circuit shown in Fig. 10-SM.



**FIG. 10-SM.** Evaluation ends with  $q_5$ , where this six-terminal configuration must be solved for the final answer. The formula contains the term  $q_5^{(0)}$ , which must first be evaluated before  $q_5$  can be solved.



**FIG. 11-SM.** Evaluation for  $q_5^{(0)}$  requires  $n_5 = 0$  (where  $n_5$  is defined in Fig. 10-SM), giving us a “new” configuration to solve here. This configuration contains a unit terminal on the far right that is isolated from the right branch defined by the parameters ( $\tilde{\tilde{\tilde{}}$ )  $n_1$ ,  $n_2$ , and  $n_3$ .

In Fig. 11-SM,  $q_5^{(0)}$  is relatively straightforward since there are only two parallel branches: a unit terminal giving a CER of 1 and an alternating four-terminal configuration that is mathematically identical to  $q_3$ , whose CER is  $\frac{8}{9}$ . This allows us to

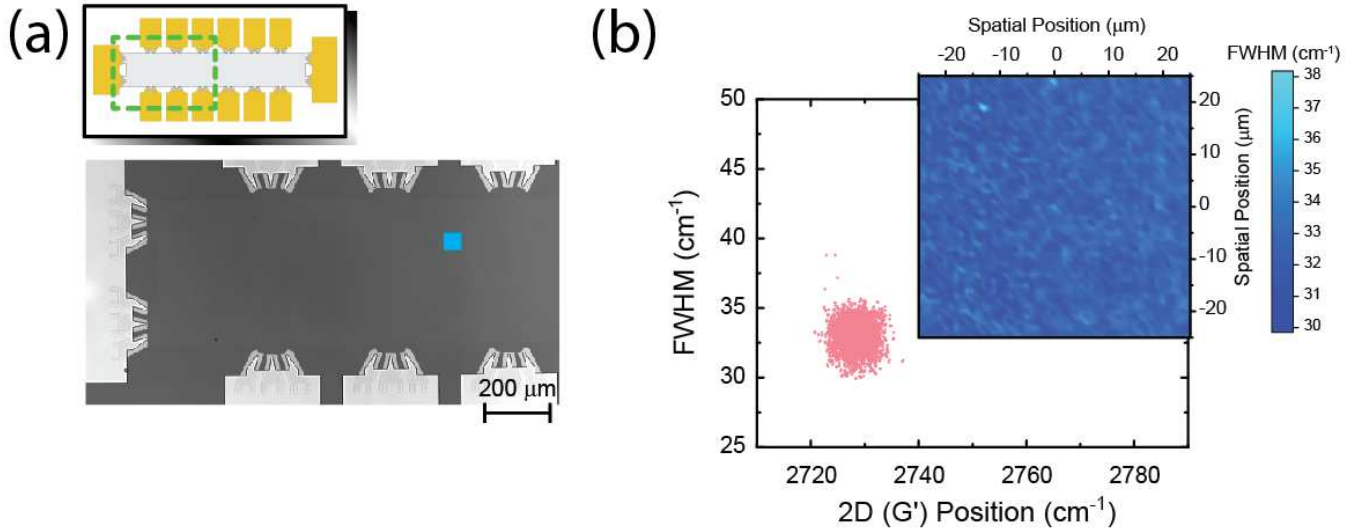
get  $q_5^{(0)}$ :  $q_5^{(0)} = \left(\frac{1}{1} + \frac{9}{8}\right)^{-1} = \frac{8}{17}$

$$q_5(n_5) = \frac{q_4(n_5 + 1)}{n_5 + \frac{q_4}{q_5^{(0)}}} = \frac{\frac{16}{23}(1 + 1)}{1 + \frac{16/23}{8/17}} = \frac{32}{57}$$

The final result is  $q_5 = \frac{32}{57}$ , and is closely matched by the experimental data in the main text.

### 3. Raman spectra for large scale homogeneity

In Fig. 12-SM, a Raman map was acquired with a Renishaw InVia micro-Raman spectrometer<sup>[see notes]</sup> using a 633 nm wavelength excitation laser source and a backscattering configuration. The spot size was about 1  $\mu\text{m}$ , the acquisition times were 300 s, the laser power was 1.7 mW power, and the optical path included a 50  $\times$  objective and 1200  $\text{mm}^{-1}$  grating. The spread is indicative of a relatively homogeneous sample.

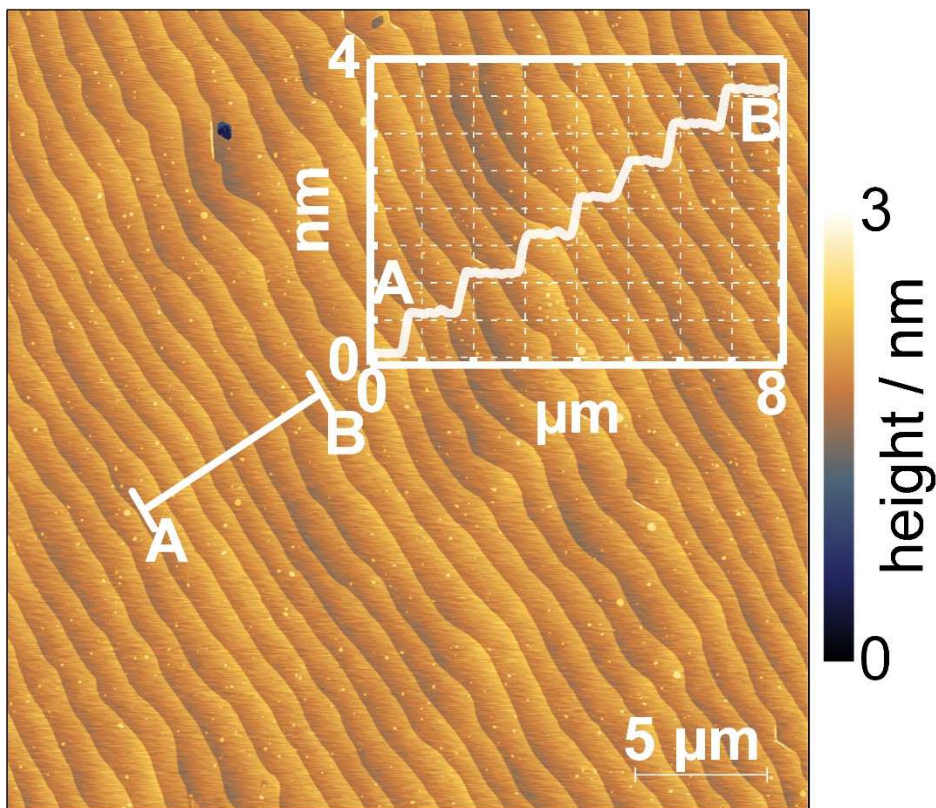


**FIG. 12-SM.** (a) Optical image of example device after growth. (b) A Raman map was acquired to ensure sample homogeneity. The map was taken over the area shaded in light blue in (a).

### 4. Supporting AFM images

Prior to deposition of  $\text{Cr}(\text{CO})_3$  and the various polymers required for large-scale electron density modulation, AFM images were acquired on post-growth graphene areas to verify homogeneity. The polymer-assisted growth suppressed the formation of nanoscopic steps typically seen in SiC sublimation.





**FIG. 13-SM.** Example AFM image for approximate region of the device similar to Raman map and taken prior to functionalization. This image verifies the suppression of overactive step bunching typically seen with SiC sublimation. Aside from several spot contaminants, the graphene can grow unimpeded along the ordered steps.

## NOTES

<sup>a</sup> Commercial equipment, instruments, and materials are identified in this paper in order to specify the experimental procedure adequately. Such identification is not intended to imply recommendation or endorsement by the National Institute of Standards and Technology or the United States government, nor is it intended to imply that the materials or equipment identified are necessarily the best available for the purpose.

## REFERENCES

<sup>1</sup>A.F. Rigosi, D.K. Patel, M. Marzano, M. Kruskopf, H.M. Hill, H. Jin, J. Hu, A.R. Hight Walker, and D.B. Newell, *Physica B*, DOI: 10.1016/j.physb.2019.411971 (2019).