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# Spectrum and energy levels of five-times ionized zirconium (Zr VI)

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## Abstract

We carried out a new analysis of the spectrum of five-times-ionized zirconium Zr VI. For this we used sliding-spark discharges together with normal- and grazing-incidence spectrographs to observe the spectrum from 160 to 2000 Å. These observations showed that the analysis of this spectrum by Khan *et al* (1985 *Phys. Scr.* **31** 837) contained a significant number of incorrect energy levels. We have now classified ~420 lines as transitions between 23 even-parity levels 73 odd-parity levels. The  $4s^2 4p^5$ ,  $4s 4p^6$ ,  $4s^2 4p^4 4d$ ,  $5s$ ,  $5d$ ,  $6s$  configurations are now complete, although a few levels of  $4s^2 4p^4 5d$  are tentative. We determined Ritz-type wavelengths for ~135 lines from the optimized energy levels. The uncertainties range from 0.0003 to 0.0020 Å. Hartree–Fock calculations and least-squares fits of the energy parameters to the observed levels were used to interpret the observed configurations. Oscillator strengths for all classified lines were calculated with the fitted parameters. The results are compared with values for the level energies, percentage compositions, and transition probabilities from recent *ab initio* theoretical calculations. The ionization energy was revised to  $777\,380 \pm 300 \text{ cm}^{-1}$  ( $96.38 \pm 0.04 \text{ eV}$ ).

Keywords: zirconium, spectrum, energy levels, wavelengths, ionization energy, transition probabilities, ultraviolet

(Some figures may appear in colour only in the online journal)

## 1. Introduction

The zirconium atom has atomic number  $Z = 40$ . Five-times-ionized zirconium, Zr VI, is isoelectronic with neutral Br. The ground state is  $4s^2 4p^5 \ ^2P$ , and excited states are mainly of the type  $4s^2 4p^4 nl$ . The first work on this spectrum was done by Paul and Rense [1]. From their observation of transitions to the ground term, they determined the  $4p^5 \ ^2P$  interval as well as the first excited state  $4s 4p^6 \ ^2S_{1/2}$  and several levels of the  $4p^4 4d$  and  $4p^4 5s$  configurations. Subsequently, Chaghtai [2, 3] re-observed the resonance transitions and found that nearly all of Paul and Rense's excited levels were in error. Chaghtai gave values for 16 new levels in these configurations. Subsequently, Ekberg *et al* [4] re-investigated the spectrum and gave improved values for nearly all levels of the  $4p^4 4d$  and  $5s$  configurations. Seven of Chaghtai's levels were found to be spurious. Chaghtai *et al* [5] later extended the resonance lines to the  $4p^4 5d$ ,  $6s$ ,  $6d$ , and  $7s$  configurations. Khan *et al* [6] determined the levels of the  $4p^4 5p$

configuration by using longer wavelength transitions from the above configurations to levels of  $4p^4 5p$ .

In the present work we re-observed the spectrum of Zr VI in the vacuum ultraviolet and revised the analysis considerably. In particular, 13 of the 21 levels of  $4p^4 5p$  reported by Khan *et al* [6] were found to be spurious. Several new levels of  $4p^4 4d$ ,  $5s$ ,  $5d$ , and  $6s$  reported in [6] were also found to be spurious.

## 2. Experiment

The observations used for this work were the same as used for earlier work in our laboratory on zirconium [7]. The main light source was a low-voltage sliding-spark with metallic Zr electrodes. The source was operated as described by Reader *et al* [8]. From 500 to 2000 Å the spectra were recorded on our 10.7 m normal-incidence vacuum spectrograph. From 160 to 500 Å the spectra were recorded on our 10.7 m grazing

incidence spectrograph. Both instruments had gratings with 1200 lines/mm. The plate factor for the normal-incidence spectrograph was about  $0.78 \text{ \AA mm}^{-1}$ . The plate factor for the grazing-incidence spectrograph at  $350 \text{ \AA}$  was  $0.25 \text{ \AA mm}^{-1}$ . From 600 to  $2000 \text{ \AA}$  the spectra were calibrated by spectra of Cu II excited in a hollow cathode discharge. Below  $600 \text{ \AA}$  calibration was obtained from lines of Y in various stages of ionization. Shifts between the positions of the reference spectra and those of the unknown spectra due to differing illumination of the spectrograph were removed by use of impurity lines of oxygen, nitrogen, carbon, and silicon. Complete references for the calibration spectra are given in [7].

Ionization stages were distinguished by comparing the intensities of the lines at various peak currents in the spark. The spectra of Zr VI were relatively enhanced at a peak current of about  $2000 \text{ A}$ .

The wavelengths, intensities, and classifications of the observed lines of Zr VI are given in table 1. The intensities are estimates of photographic plate blackening. No effort was made to harmonize the intensities through the complete region of observation. The general uncertainty of the wavelengths is  $\pm 0.005 \text{ \AA}$ . Hazy lines (h) were given an uncertainty of  $\pm 0.010 \text{ \AA}$ ; perturbed (p), or asymmetric lines (s, l) an uncertainty of  $\pm 0.020$ ; unresolved (u) or doubly classified (dc) lines an uncertainty of  $\pm 0.030 \text{ \AA}$ . By *perturbed* we mean that the measured position may possibly be affected by the presence of a close line. The line at  $1749.353 \text{ \AA}$  could not be measured in the original observations because of a local defect in the emulsion of one of the photographic plates. It was later recorded with an image plate [9, 10] on the normal-incidence spectrograph. Its wavelength uncertainty was also taken as  $\pm 0.005 \text{ \AA}$ . All uncertainties are reported at the level of one standard deviation.

### 3. Spectrum analysis and level value determination

The analysis was carried out in a manner similar to that used for the recent analysis of Mo V [11]. As described there 'Interpretation of the spectrum was guided by calculations of the level structures and transition probabilities with the Hartree-Fock code of Cowan [12]. Further guidance was provided by construction of two-dimensional transition arrays with the computer spreadsheet method described by Reader [13]'.

The odd parity energy levels are given in table 2, the even levels in table 3. In addition to the usual spectroscopic designations in either LS or  $jl$  (pair) coupling, the levels are given shorthand designations that are used in the classification of the spectral lines. The shorthand designations are explained in the footnotes to tables 2 and 3. As described in [11] 'the values of the energy levels were optimized with the computer program ELCALC [14], an iterative procedure in which the observed wave numbers are weighted according to the inverse square of their uncertainties. The uncertainties of the level values given by this procedure are also listed'. For the level optimization only the most reliably classified lines were used.

That is, lines that were very weak or that appeared with suspiciously high intensities were excluded.

Figure 1 shows a schematic overview of the positions of the  $4s^24p^5$ ,  $4s4p^6$ ,  $4s^24p^44d$ ,  $5s$ ,  $5p$ ,  $5d$ , and  $6s$ , configurations. It also shows the calculated positions of the  $4s^24p^44f$  and  $4s4p^54d$  configurations, although no levels have as yet been established for them.

#### 3.1. $4s^24p^44d$ levels

Nearly all levels of this configuration that could combine with the ground state were present in [4]. Remaining as unknown were  $(^3P)^4D_{1/2,7/2}$ ,  $(^1S)^2D_{5/2}$ ,  $(^3P)^4F_{7/2,9/2}$ ,  $(^3P)^2F_{7/2}$ ,  $(^1D)^2G_{7/2,9/2}$ , and  $(^1D)^2F_{7/2}$ . Values for these 9 levels were given in [6]. Our present work shows that 6 of the 9 were spurious. Details of these 9 levels are:

- (1)  $(^3P)^4D_{1/2}$ —new level; two new resonance lines ( $397.112$  and  $423.344 \text{ \AA}$ ) and three transitions to levels of  $4p^45p$
- (2)  $(^3P)^4D_{7/2}$ —new level; four strong transitions to levels of  $4p^45p$
- (3)  $(^1S)^2D_{5/2}$ —new level; one new resonance line ( $307.148 \text{ \AA}$ ) and three transitions to levels of  $4p^45p$
- (4)  $(^3P)^4F_{7/2}$ —present in [6]; five transitions to levels of  $4p^45p$
- (5)  $(^3P)^4F_{9/2}$ —new level; single line at  $602.387 \text{ \AA}$ , places  $(^3P)^4F_{9/2}$  close to prediction
- (6)  $(^3P)^2F_{7/2}$ —new level; six transitions to levels of  $4p^45p$
- (7)  $(^1D)^2G_{7/2}$ —new level; four transitions to levels of  $4p^45p$
- (8)  $(^1D)^2G_{9/2}$ —present in [6]; single line at  $600.282 \text{ \AA}$ ; places  $(^1D)^2G_{9/2}$  close to prediction
- (9)  $(^1D)^2F_{7/2}$ —present in [6]; six transitions to levels of  $4p^45p$ .

We note that the two  $J = 9/2$  levels of  $4p^44d$  are established by single transitions that are close in wavelength,  $600.282 \text{ \AA}$  and  $602.387 \text{ \AA}$ . Thus, one could consider interchanging their classifications without changing the level values very much. Our present classifications were chosen to provide the best match with the level values given by the least-squares fit (LSF) with the Cowan code, described in section 4 below.

The structure of the  $4p^44d$  configuration is shown in figure 2. This is similar to figure 1 of [4], except that we show here the observed positions of levels that were previously unknown.

#### 3.2. $4s^24p^45s$ levels

The  $4s^24p^45s$  levels [1, 2, 4] have improved values due to their combinations with  $4s^24p^45p$ . For completeness, in figure 3 we give the structure of the  $4p^45s$  configuration. This is the same as figure 2 of [4], except that here we designate the levels in  $jl$  coupling, rather than  $Jj$ . This coupling scheme is more now more commonly used for  $np^4ns$  configurations.

**Table 1.** Observed spectral lines of Zr VI. Wavelengths and wave numbers are in vacuum. Wavelength values in parentheses are Ritz values. General uncertainty of the observed wavelengths is  $\pm 0.005$  Å. Uncertainties for less certain wavelengths are given in section 2 of text. Acc. is the accuracy estimate.

$\lambda_{\text{obs}}(\text{Å})$	Intensity	$\sigma_{\text{obs}}(\text{cm}^{-1})$	Even level <sup>a</sup>	Odd level <sup>a</sup>	$\lambda_{\text{Ritz}}(\text{Å})$	Unc( $\lambda_{\text{Ritz}}$ , Å)	$g_U A(\text{s}^{-1})$	$\log(g_L f)$	ICFI	Acc.
165.930	5	602 664	6s31	p5 3	165.9308	0.0011	2.28E + 09	-2.03	0.15	D+
170.342	6	587 054	6s31	p5 1	170.3408	0.0012	6.37E + 09	-1.56	0.60	D+
174.066	6	574 495	5d85	p5 3	174.0660	0.0003	2.46E + 09	1.95	0.30	D+
174.489	70	573 102	6s25	p5 3	174.4891	0.0003	2.27E + 10	0.99	0.65	D+
178.236	50	561 054	6s21	p5 3	178.2371	0.0003	9.00E + 09	1.37	0.54	D+
178.776	60	559 359	6s23	p5 3	178.7769	0.0003	8.48E + 09	1.39	0.55	D+
178.794	30	559 303	5d83	p5 1	178.7993	0.0004	6.19E + 09	1.53	0.26	D+
179.144	10	558 210	6s11	p5 3	179.1445	0.0003	1.17E + 09	2.25	0.51	E
179.308	70	557 700	6s33	p5 1	179.3084	0.0003	2.14E + 10	0.99	0.70	D+
182.213	30	548 808	5d73	p5 3	182.2139	0.0003	3.07E + 09	1.82	0.16	D+
182.550	20	547 795	5d51	p5 3			4.24E + 09	1.67	0.14	D+
182.657	90	547 474	6s13	p5 3	182.6578	0.0003	1.86E + 10	1.03	0.25	D+
182.744	80	547 214	5d75	p5 3	182.7439	0.0003	1.34E + 10	1.18	0.45	D+
183.262	70	545 667	5d65	p5 3	183.2623	0.0003	9.69E + 09	1.31	0.35	D+
183.336	60	dc	545 447	6s15	183.3357	0.0004	2.33E + 09	1.93	0.67	D+
183.336	60	dc	545 447	6s21	183.3471	0.0003	1.07E + 10	1.27	0.40	D+
183.680	90		544 425	5d63			3.65E + 10	0.73	0.50	D+
183.908	5		543 750	6s23	183.9068	0.0004	1.19E + 09	2.22	0.35	E
184.063	60		543 292	5d41	184.0618	0.0003	6.50E + 09	1.48	0.17	D+
187.075	20		534 545	5d53	187.0723	0.0003	2.64E + 09	1.86	0.06	D+
187.361	100		533 729	5d55	187.3582	0.0003	2.74E + 10	0.84	0.41	D+
187.549	80		533 194	5d73	187.5459	0.0004	2.50E + 10	0.88	0.42	D+
187.830	5	ℓ	532 396	5d45	187.8277	0.0003	1.04E + 09	2.26	0.25	E
187.905	60		532 184	5d51			1.67E + 10	1.05	0.44	D+
188.490	20		530 532	5d43	188.4876	0.0003	2.23E + 09	1.93	0.20	D+
188.912	2	x	529 347	5d35	188.9103	0.0003	1.89E + 08	3.00	0.05	E
189.046	3		528 972	5d33	189.0444	0.0003	7.85E + 08	2.38	0.31	E
189.101	30		528 818	5d63			6.39E + 09	1.47	0.29	D+
189.267	2		528 354	5d31	189.2658	0.0003	3.84E + 08	2.69	0.11	E
189.506	5		527 688	5d41	189.5041	0.0004	4.92E + 08	2.58	0.02	E
191.557	90		522 038	5d25	191.5577	0.0003	2.73E + 10	0.82	0.43	D+
191.666	80		521 741	5d23	191.6663	0.0004	1.43E + 10	1.10	0.42	D+
192.182	20	u, J	520 340	5d21	192.1679	0.0004	2.51E + 09	1.86	0.20	D+
192.696	60		518 952	5d53	192.6968	0.0004	7.84E + 09	1.36	0.23	D+
194.108	1		515 177	5d13	194.1104	0.0003	5.39E + 07	3.52	0.01	E
194.197	20	p, x	514 941	5d43	194.1988	0.0004	2.32E + 09	1.88	0.12	D+
195.024	2	x	512 757	5d31	195.0250	0.0004	4.35E + 08	2.61	0.08	E
197.575	80		506 137	5d23	197.5749	0.0005	1.90E + 09	1.95	0.05	D+
236.281	100		423 225	5s31	236.2818	0.0005	3.14E + 09	1.58	0.06	D+
245.327	90	u	407 619	5s31	245.3261	0.0006	1.62E + 10	0.84	0.47	D+
253.678	80		394 201	5s33	253.6812	0.0005	2.26E + 09	1.66	0.04	D+
254.092	400		393 558	5s25	254.0939	0.0005	6.20E + 10	0.22	0.65	C
259.888	200		384 781	5s21	259.8878	0.0006	2.91E + 10	0.53	0.67	D+
263.310	500		379 780	5s23	263.3127	0.0006	4.96E + 10	0.29	0.83	C
264.142	90	p	378 584	5s33	264.1361	0.0007	4.67E + 10	0.31	0.61	C
264.940	100		377 444	5s11	264.9343	0.0006	6.57E + 08	2.16	0.15	D+
270.480	200		369 713	5s13	270.4811	0.0006	6.60E + 10	0.14	0.74	C
270.872	200		369 178	5s21	270.8716	0.0007	3.75E + 10	0.39	0.61	C
274.105	200		364 824	5s15	274.1024	0.0006	2.76E + 09	1.51	0.33	D+
274.598	100		364 169	5s23	274.5941	0.0007	4.14E + 09	1.33	0.24	D+
276.364	80		361 842	5s11	276.3582	0.0007	2.53E + 07	3.54	0.01	E
279.198	90	p	358 169	4d83	279.1985	0.0007	1.78E + 10	0.68	0.05	D+
282.400	90		354 108	5s13	282.3990	0.0008	3.56E + 09	1.37	0.10	D+
288.730	200		346 344	4d51	288.7290	0.0008	2.75E + 10	0.46	0.11	D+
290.949	500		343 703	4d85	290.9433	0.0007	1.05E + 12	1.12	0.85	C
291.920	500	p	342 560	4d83	291.9151	0.0009	6.60E + 11	0.93	0.85	C

Table 1. (Continued.)

$\lambda_{\text{obs}}(\text{\AA})$	Intensity	$\sigma_{\text{obs}}(\text{cm}^{-1})$	Even level <sup>a</sup>	Odd level <sup>a</sup>	$\lambda_{\text{Ritz}}(\text{\AA})$	Unc( $\lambda_{\text{Ritz}}-\text{\AA}$ )	$g_U A(\text{s}^{-1})$	$\log(g_L f)$	ICFI	Acc.	
294.395	500	339 680	4d73	p5 3	294.3923	0.0007	5.84E + 11	0.88	0.90	C	
298.779	300	334 696	4d41	p5 3	298.7796	0.0008	2.81E + 11	0.58	0.71	C	
302.351	300	330 741.4	4d51	p5 1	302.3498	0.0010	2.56E + 11	0.55	0.87	C	
307.148	30	325 575.9	4d75	p5 3	307.1472	0.0010	3.16E + 06	4.35	0.00	E	
308.569	100	324 076.6	4d73	p5 1	308.5658	0.0009	4.65E + 09	1.18	0.02	D+	
313.150	300	319 335.8	4d63	p5 3	313.1496	0.0010	1.27E + 10	0.73	0.11	D+	
313.389	300	319 092.2	4d41	p5 1	313.3891	0.0010	2.55E + 10	0.43	0.11	C	
329.242	300	303 728.0	4d63	p5 1	329.2361	0.0012	1.31E + 10	0.67	0.06	D+	
333.768	400	299 609.3	4d65	p5 3	333.7687	0.0010	2.97E + 09	1.31	0.10	D+	
340.915	30	293 328.2	4p61	5p83	340.9169	0.0011	1.38E + 09	1.62	0.02	E	
343.493	10	291 126.7	4p61	5p61	343.4908	0.0011	2.34E + 07	3.38	0.02	E	
348.262	200	p	287 140.1	4d55	p5 3	348.2592	0.0012	9.38E + 08	1.77	0.01	D+
353.221	250	283 108.9	4d45	p5 3	353.2171	0.0011	2.40E + 09	1.35	0.01	D+	
357.837	30	279 456.8	4d53	p5 3	357.8365	0.0012	2.21E + 08	2.37	0.00	D+	
358.755	300	278 741.8	4d35	p5 3	358.7544	0.0012	1.71E + 09	1.48	0.02	D+	
364.080	300	274 664.9	4d43	p5 3	364.0791	0.0013	1.52E + 09	1.52	0.01	D+	
366.095	60	p	273 153.1	4p61	5p51	366.0947	0.0012	9.72E + 08	1.71	0.18	D+
366.522	200	272 834.9	4d33	p5 3	366.5226	0.0014	2.11E + 09	1.37	0.02	D+	
367.523	300	272 091.8	4d31	p5 3	367.5238	0.0015	1.72E + 09	1.46	0.15	D+	
368.494	300	271 374.8	4d25	p5 3	368.4947	0.0015	1.28E + 09	1.58	0.61	D+	
368.600	250	271 296.8	4d23	p5 3	368.6010	0.0013	8.52E + 08	1.76	0.01	D+	
375.546	30	266 279.0	4d21	p5 3	375.5467	0.0015	2.99E + 07	3.20	0.00	E	
378.342	60	264 311.1	4p61	5p63	378.3472	0.0013	1.61E + 09	1.46	0.27	D+	
378.992	80	263 857.8	4d53	p5 1	378.9969	0.0015	6.03E + 07	2.89	0.00	E	
386.007	250	259 062.7	4d43	p5 1	386.0068	0.0016	1.55E + 09	1.46	0.01	D+	
388.754	20	257 232.1	4d33	p5 1	388.7546	0.0018	3.39E + 07	3.12	0.00	E	
389.881	100	p	256 488.5	4d31	p5 1	389.8811	0.0019	1.43E + 08	2.49	0.01	E
391.094	100	p	255 693.0	4d23	p5 1	391.0936	0.0017	3.67E + 07	3.07	0.00	E
397.112	30	251 818.1	4d11	p5 3			2.79E + 07	3.18	0.01	E	
398.588	2	250 885.6	4p61	5p43	398.5922	0.0014	2.20E + 08	2.28	0.15	D+	
398.919	80	250 677.5	4d21	p5 1	398.9218	0.0019	1.53E + 08	2.44	0.00	E	
399.967	80	250 020.6	4d13	p5 3	399.9718	0.0018	4.90E + 07	2.93	0.00	E	
401.701	80	248 941.4	4d15	p5 3	401.7031	0.0019	5.69E + 07	2.86	0.00	E	
411.136	4	243 228.5	4p61	5p21	411.1384	0.0016	7.96E + 07	2.70	0.08	E	
423.344	5	236 214.5	4d11	p5 1			1.93E + 07	3.29	0.00	E	
514.611	1	x	194 321.5	4d13	5p41		2.32E + 08	2.04	0.07	D+	
516.763	10	193 512.3	4d15	5p43			7.64E + 08	1.52	0.06	D+	
516.970	10	x	193 434.8	4d27	5p55	516.9686	0.0014	3.09E + 08	1.91	0.06	E
522.000	2000	191 570.9	4p61	p5 3			2.62E + 09	0.97	0.04	D+	
522.929	20	191 230.5	4d17	5p35			1.95E + 09	1.10	0.08	D+	
524.835	5	190 536.1	4d13	5p35			2.97E + 08	1.91	0.06	D+	
530.404	5	x	188 535.5	4d15	5p33		1.43E + 08	2.22	0.01	D+	
532.528	10	s	187 783.6	4d23	5p73	532.5335	0.0017	6.94E + 08	1.53	0.11	D+
533.450	30	187 459.0	4d13	5p33			7.08E + 08	1.52	0.10	D+	
535.216	80	186 840.5	4d13	5p31			1.16E + 09	1.30	0.12	D+	
538.618	5	185 660.3	4d11	5p33			3.24E + 08	1.85	0.12	D+	
539.350	70	$\ell, x$	185 408.4	4d13	5p23		3.38E + 07	2.83	0.00	E	
539.765	10	$\ell, x$	185 265.8	4d53	5p51	539.7620	0.0014	1.46E + 08	2.20	0.02	D+
540.791	40	184 914.3	4d43	5p55	540.7885	0.0015	1.06E + 09	1.33	0.24	E	
541.756	10	x	184 584.9	4d23	5p63	541.7643	0.0017	1.56E + 08	2.16	0.02	D+
542.264	60	184 412.0	4d43	5p73	542.2639	0.0015	1.15E + 09	1.30	0.08	D+	
544.117	10	183 784.0	4d31	5p63			2.25E + 08	2.00	0.09	D+	
546.182	80	183 089.2	4d37	5p55			1.27E + 09	1.24	0.10	D+	
546.508	50	p, x	182 979.9	4d11	5p21		1.59E + 09	1.15	0.19	D+	
556.729	80	179 620.6	4d53	5p73	556.7295	0.0013	5.98E + 08	1.55	0.07	D+	
559.569	200	178 709.0	4d15	5p17			1.54E + 09	1.14	0.55	D+	
560.428	2	x	178 435.1	4d23	5p45	560.4292	0.0018	2.26E + 08	1.97	0.14	D+
560.769	300	178 326.5	4d17	5p17			9.64E + 09	0.34	0.71	C	

Table 1. (Continued.)

$\lambda_{\text{obs}}(\text{\AA})$	Intensity		$\sigma_{\text{obs}}(\text{cm}^{-1})$	Even level <sup>a</sup>	Odd level <sup>a</sup>	$\lambda_{\text{Ritz}}(\text{\AA})$	Unc( $\lambda_{\text{Ritz}}-\text{\AA}$ )	$g_U A(\text{s}^{-1})$	$\log(g_L f)$	ICFI	Acc.
561.601	10	x	178 062.4	4d21	5p41			1.88E + 08	2.05	0.03	D+
562.444	300		177 795.5	4d17	5p25			4.34E + 09	0.69	0.33	C
564.537	200		177 136.3	4d35	5p63	564.5382	0.0015	1.19E + 09	1.25	0.16	D+
565.300	5	x	176 897.2	4d33	5p45			6.70E + 07	2.49	0.10	D+
566.546	20	ℓ	176 508.2	4d37	5p27			1.65E + 08	2.10	0.03	D+
566.670	300	p	176 469.6	4d45	5p55	566.6725	0.0013	5.13E + 09	0.61	0.34	C
566.819	300		176 423.2	4d53	5p63	566.8261	0.0014	2.37E + 09	0.94	0.18	D+
567.620	80	h	176 174.2	4d21	5p43			4.59E + 08	1.65	0.14	D+
568.284	2000		175 968.4	4p61	p5 1			1.19E + 09	1.24	0.05	D+
569.281	300		175 660.2	4d13	5p11			2.08E + 09	1.00	0.27	D+
573.360	300		174 410.5	4d27	5p35			5.60E + 09	0.56	0.17	C
575.179	500		173 858.9	4d11	5p11			3.29E + 09	0.79	0.58	D+
576.090	10		173 584.0	4d23	5p53	576.0923	0.0019	5.03E + 07	2.60	0.01	E
577.233	20		173 240.3	4d37	5p45			2.04E + 09	0.99	0.09	D+
577.863	500		173 051.4	4d15	5p15			1.10E + 10	0.26	0.69	C
578.737	100		172 790.1	4d31	5p53			9.14E + 08	1.34	0.18	D+
578.811	80		172 768.0	4d45	5p63	578.8171	0.0014	8.03E + 08	1.40	0.05	D+
579.142	400	ℓ	172 669.2	4d17	5p15			1.47E + 10	0.13	0.43	C
579.913	200		172 439.7	4d55	5p55	579.9174	0.0018	1.38E + 09	1.15	0.22	D+
580.321	300	ℓ	172 318.4	4d15	5p13			7.13E + 09	0.45	0.36	C
581.236	200		172 047.2	4d33	5p53			1.44E + 09	1.14	0.26	D+
581.480	300		171 975.0	4d13	5p15			2.49E + 09	0.90	0.66	D+
581.610	200		171 936.5	4d55	5p73	581.6144	0.0018	1.34E + 09	1.16	0.18	D+
583.063	200		171 508.1	4d33	5p41			1.59E + 09	1.09	0.33	D+
583.970	400		171 241.7	4d13	5p13			7.86E + 09	0.40	0.68	C
584.111	150		171 200.3	4d21	5p33			9.04E + 08	1.33	0.34	D+
584.251	250		171 159.3	4d23	5p43	584.2568	0.0020	1.67E + 09	1.07	0.25	D+
584.517	200	x	171 081.4	4d25	5p43			9.33E + 08	1.32	0.27	D+
586.229	100		170 581.8	4d21	5p31			8.86E + 08	1.34	0.26	D+
588.625	200		169 887.4	4d45	5p27	588.6235	0.0015	1.42E + 09	1.13	0.36	D+
589.367	5	x	169 673.6	4d43	5p41	589.3639	0.0019	1.98E + 08	1.99	0.03	D+
(590.182)		A	(169 439.3)	4d11	5p13			2.20E + 09	0.94	0.71	D+
591.079	100		169 182.1	4d25	5p35			2.29E + 09	0.92	0.35	D+
593.405	200		168 519.0	4d21	5p21			3.21E + 09	0.77	0.66	D+
595.987	5	x	167 788.9	4d43	5p43	595.9900	0.0019	4.71E + 08	1.60	0.07	D+
596.236	5		167 718.8	4d33	5p35			3.91E + 08	1.68	0.12	D+
598.686	400		167 032.5	4d47	5p27			3.31E + 09	0.75	0.65	D+
600.282	1000		166 588.4	4d29	5p27			3.30E + 10	0.25	0.73	C
601.759	2		166 179.5	4d23	5p33			1.23E + 09	1.18	0.15	D+
601.914	50		166 136.7	4d35	5p53	601.9125	0.0017	3.33E + 09	0.74	0.21	C
602.040	100		166 101.9	4d25	5p33			7.35E + 09	0.40	0.59	C
602.387	2000		166 006.2	4d19	5p17			3.36E + 10	0.26	0.80	C
602.932	5		165 856.2	4d55	5p27			5.55E + 08	1.52	0.46	D+
604.002	100		165 562.4	4d23	5p31			4.62E + 09	0.60	0.44	C
604.515	50		165 421.9	4d53	5p53	604.5140	0.0016	1.93E + 09	0.97	0.29	D+
606.493	50		164 882.4	4d53	5p41	606.4912	0.0016	4.18E + 09	0.64	0.71	C
607.378	100		164 642.1	4d33	5p33			2.27E + 09	0.90	0.28	D+
609.525	100	p	164 062.2	4d37	5p35			1.82E + 10	0.01	0.78	C
609.552	90	u	164 054.9	4d25	5p23			7.55E + 09	0.38	0.76	C
610.639	500		163 762.9	4d47	5p45			2.09E + 10	0.07	0.65	C
610.834	1000		163 710.6	4d35	5p43	610.8309	0.0018	6.00E + 09	0.48	0.36	C
611.614	10		163 501.8	4d23	5p21			2.05E + 09	0.94	0.22	D+
612.145	200		163 360.0	4d63	5p61			5.37E + 09	0.52	0.48	C
612.234	50		163 336.2	4d31	5p23			1.49E + 09	1.07	0.40	D+
614.207	5		162 811.6	4d43	5p33	614.2076	0.0020	1.51E + 09	1.07	0.18	D+
615.047	200		162 589.2	4d55	5p45	615.0504	0.0020	2.12E + 09	0.92	0.40	D+
616.547	100		162 193.6	4d43	5p31	616.5475	0.0020	2.95E + 09	0.77	0.41	D+
617.422	200		161 963.8	4d33	5p21			2.16E + 09	0.91	0.29	D+

Table 1. (Continued.)

$\lambda_{\text{obs}}(\text{\AA})$	Intensity	$\sigma_{\text{obs}}(\text{cm}^{-1})$	Even level <sup>a</sup>	Odd level <sup>a</sup>	$\lambda_{\text{Ritz}}(\text{\AA})$	Unc( $\lambda_{\text{Ritz}}-\text{\AA}$ )	$g_U A(\text{s}^{-1})$	$\log(g_L f)$	ICFI	Acc.
617.999	5	161 812.6	4d35	5p35	617.9987	0.0019	2.77E + 08	1.80	0.06	D+
618.172	200	161 767.3	4d45	5p53	618.1718	0.0016	2.80E + 09	0.80	0.25	D+
619.181	50	161 503.7	4d27	5p17			1.22E + 09	1.15	0.23	D+
620.741	2	161 097.8	4d53	5p35	620.7415	0.0017	1.53E + 08	2.05	0.05	D+
621.223	800	160 972.8	4d27	5p25			1.55E + 10	0.05	0.80	C
622.037	100	160 762.1	4d43	5p23	622.0372	0.0020	3.26E + 09	0.72	0.42	C
627.081	200	159 469.0	4d65	5p73	627.0812	0.0019	6.98E + 09	0.38	0.57	C
627.358	10	159 398.6	4d21	5p11			4.46E + 08	1.58	0.09	D+
627.583	50	159 341.5	4d45	5p43	627.5823	0.0017	2.84E + 09	0.78	0.18	D+
627.667	100	159 320.1	4d75	5p83			1.54E + 10	0.04	0.68	C
629.982	20	158 734.7	4d35	5p33	629.9817	0.0019	1.61E + 09	1.02	0.33	D+
632.835	5	158 019.1	4d53	5p33	632.8321	0.0017	8.15E + 08	1.31	0.11	D+
633.968	200	157 736.7	4d55	5p53			7.53E + 09	0.34	0.68	C
635.151	50	157 442.9	4d45	5p35	635.1510	0.0017	1.27E + 09	1.12	0.24	D+
635.318	5	157 401.5	4d53	5p31	635.3164	0.0018	4.21E + 08	1.59	0.10	D+
638.222	5	156 685.3	4d35	5p23	638.2213	0.0020	1.29E + 09	1.10	0.14	D+
639.920	200	156 269.5	4d65	5p63	639.9202	0.0019	4.09E + 09	0.60	0.63	C
640.764	500	156 063.7	4d57	5p55			1.65E + 10	0.01	0.85	D
641.147	5	155 970.5	4d53	5p23	641.1470	0.0018	4.45E + 08	1.56	0.07	D+
641.661	500	155 845.5	4d27	5p15			3.05E + 09	0.73	0.26	C
642.080	40	155 743.8	4d25	5p25			8.32E + 08	1.29	0.48	D+
643.746	50	155 340.8	4d53	5p21	643.7469	0.0019	1.13E + 09	1.15	0.20	D+
643.869	400	155 311.1	4d55	5p43			4.62E + 09	0.54	0.50	C
645.249	2	154 978.9	4d21	5p13			3.77E + 08	1.62	0.17	D+
646.881	2	154 587.9	4d47	5p35			6.90E + 08	1.37	0.13	D+
647.745	100	154 381.7	4d23	5p11			1.52E + 09	1.02	0.38	D+
647.816	100	154 364.8	4d45	5p33	647.8152	0.0017	2.33E + 09	0.84	0.26	D+
651.100	30	153 586.2	4d31	5p11			9.61E + 08	1.22	0.78	D+
654.264	2	152 843.5	4d33	5p11			1.02E + 09	1.19	0.31	D+
655.940	10	152 453.0	4d43	5p25			2.88E + 08	1.73	0.17	D+
656.533	20	152 315.3	4d45	5p23	656.5312	0.0018	1.52E + 09	1.01	0.15	D+
661.560	4	151 157.9	4d37	5p17			2.67E + 08	1.75	0.08	D+
662.196	100	151 012.7	4d43	5p11			9.46E + 08	1.21	0.15	D+
663.593	5	150 694.8	4d23	5p15			3.43E + 08	1.65	0.23	D+
663.892	100	150 626.9	4d37	5p25			3.94E + 09	0.58	0.18	C
663.935	5	150 617.2	4d25	5p15			3.00E + 08	1.70	0.12	D+
665.185	1	150 334.1	4d55	5p33			2.80E + 07	2.73	0.01	E
666.124	100	150 122.2	4d65	5p45			3.19E + 09	0.67	0.40	C
666.835	50	149 962.1	4d23	5p13			3.73E + 08	1.61	0.10	D+
667.185	10	149 883.5	4d25	5p13			2.76E + 08	1.74	0.10	D+
668.970	500	149 483.5	4d57	5p27			4.62E + 09	0.51	0.55	C
670.392	700	149 166.5	4d31	5p13			2.13E + 09	0.84	0.47	D+
673.754	50	148 422.1	4d33	5p13			5.75E + 08	1.41	0.11	D+
673.961	100	148 376.5	4d35	5p25			1.96E + 09	0.88	0.52	D+
674.378	5	148 284.8	4d55	5p23			5.80E + 08	1.40	0.08	D+
683.926	3	146 214.6	4d57	5p45			4.04E + 08	1.55	0.07	D+
687.812	50	145 388.6	4d63	5p51			2.24E + 09	0.80	0.63	C
688.367	5	145 271.3	4d65	5p53			7.18E + 08	1.29	0.24	D+
694.411	2	144 006.9	4d45	5p25			1.44E + 08	1.99	0.03	D+
698.082	100	143 249.6	4d35	5p15			1.45E + 09	0.98	0.27	D+
700.055	5	142 845.9	4d65	5p43			4.85E + 08	1.45	0.18	D+
701.587	10	142 534.0	4d53	5p15			3.91E + 08	1.54	0.17	D+
701.674	20	142 516.3	4d35	5p13			8.50E + 08	1.20	0.11	D+
705.214	2	141 800.9	4d53	5p13			9.27E + 07	2.16	0.02	D+
708.275	2	141 188.1	4d85	5p83	708.2769	0.0020	6.05E + 08	1.34	0.10	D+
708.456	5	141 152.0	4d47	5p25			5.80E + 08	1.36	0.05	D+
709.488	2	140 946.7	4d65	5p35			2.36E + 08	1.75	0.30	D+
715.604	10	139 742.1	4d63	5p73			9.63E + 08	1.13	0.27	D+

Table 1. (Continued.)

$\lambda_{\text{obs}}(\text{\AA})$	Intensity	$\sigma_{\text{obs}}(\text{cm}^{-1})$	Even level <sup>a</sup>	Odd level <sup>a</sup>	$\lambda_{\text{Ritz}}(\text{\AA})$	Unc( $\lambda_{\text{Ritz}}-\text{\AA}$ )	$g_U A(\text{s}^{-1})$	$\log(g_L f)$	ICFI	Acc.	
720.052	10	138 878.9	4d45	5p15			4.34E + 08	1.47	0.09	D+	
723.873	2	138 145.8	4d45	5p13			1.22E + 08	2.02	0.02	D+	
729.724	10	137 038.1	4d57	5p35			5.03E + 08	1.39	0.15	D+	
732.372	5	136 542.6	4d63	5p63			7.52E + 08	1.22	0.23	D+	
736.276	10	135 818.6	4d65	5p23			7.16E + 08	1.23	0.23	D+	
746.246	20	134 004.1	4d75	5p55			1.24E + 09	0.98	0.55	D+	
784.259	50	127 508.9	4d65	5p25			3.45E + 08	1.50	0.21	D+	
789.090	50	x	126 728.3	4d83	5p83		6.11E + 08	1.24	0.38	D+	
792.305	1		126 214.0	6s13	5p13		1.55E + 09	0.84	0.20	C	
796.541	10		125 542.8	4d63	5p53		1.14E + 08	1.97	0.29	D+	
802.832	1		124 559.1	6s23	5p21		3.50E + 09	0.47	0.90	C	
803.010	500		124 531.5	4d83	5p61		2.80E + 09	0.57	0.64	C	
803.806	20		124 408.1	5d65	5p13		1.45E + 08	1.85	0.01	D+	
803.974	20		124 382.1	4d41	5p73		6.16E + 08	1.22	0.64	D+	
805.445	10		124 155.0	4d75	5p45		7.02E + 07	2.16	0.13	D+	
808.568	200	D, x	123 675.4	5d65	5p15		9.03E + 07	2.05	0.01	D+	
809.056	100		123 600.8	4d57	5p25		3.76E + 08	1.43	0.08	D+	
809.255	50		123 570.4	6s33	5p45		9.49E + 09	0.03	0.72	C	
810.226	200		123 422.4	6s15	5p15		1.26E + 10	0.09	0.92	C	
810.562	1		123 371.2	6s25	5p45		2.76E + 09	0.57	0.98	C	
812.226	1	x	123 118.4	4d63	5p43		5.80E + 07	2.24	0.05	D+	
820.482	5		121 879.6	6s23	5p33		3.80E + 09	0.42	0.60	C	
821.060	10		121 793.8	6s13	5p11		3.04E + 09	0.51	0.47	C	
824.069	20		121 349.1	6s11	5p31		3.31E + 09	0.47	0.90	C	
825.195	1000	p	121 183.5	4d41	5p63		1.62E + 09	0.78	0.57	C	
828.279	1		120 732.3	6s11	5p33		1.61E + 09	0.78	0.45	C	
830.886	1000		120 353.5	6s13	5p25		1.03E + 10	0.03	0.75	C	
832.618	1000		120 103.1	6s25	5p27		1.53E + 10	0.20	0.98	C	
834.044	5000		119 897.8	4d73	5p55	834.0424	0.0018	8.56E + 08	1.05	0.43	E
837.561	2000		119 394.3	4d73	5p73	837.5570	0.0018	1.52E + 09	0.80	0.35	C
841.738	500		118 801.8	6s23	5p35		1.12E + 10	0.07	0.95	C	
843.194	1		118 596.7	6s21	5p43		1.65E + 09	0.75	0.35	C	
844.072	2		118 473.3	4d57	5p15		9.53E + 07	1.99	0.06	D+	
844.754	500	x	118 377.7	4d51	5p51		2.32E + 09	0.61	0.72	C	
847.336	500	D, x	118 016.9	5d65	5p17		1.18E + 08	1.90	0.01	E	
849.157	500	dc	117 763.9	6s15	5p17		1.50E + 10	0.21	0.96	C	
849.157	500	dc	117 763.9	6s31	5p83		6.86E + 09	0.13	0.97	C	
851.623	1		117 422.9	6s33	5p63		2.66E + 09	0.54	0.52	C	
853.072	2	p, x	117 223.4	6s25	5p63		2.54E + 09	0.56	0.40	C	
856.823	2		116 710.2	6s21	5p41		2.72E + 09	0.52	0.80	C	
860.618	5000		116 195.6	4d73	5p63	860.6195	0.0018	2.28E + 09	0.60	0.44	C
860.800	5		116 171.0	6s21	5p53		3.66E + 09	0.39	0.75	C	
863.029	20		115 871.0	4d85	5p55	863.0271	0.0019	5.95E + 08	1.17	0.18	D+
863.893	50		115 755.1	6s11	5p43		3.78E + 09	0.37	0.94	C	
866.786	5000		115 368.7	4d85	5p73	866.7907	0.0019	1.90E + 09	0.66	0.39	C
873.541	2		114 476.6	6s23	5p53		1.88E + 09	0.67	0.49	C	
875.480	10		114 223.1	6s33	5p73		4.39E + 09	0.30	0.60	C	
877.011	1		114 023.7	6s25	5p73		1.77E + 09	0.69	0.80	C	
879.351	1		113 720.2	6s33	5p55		1.99E + 09	0.64	0.80	D	
880.897	200		113 520.6	6s25	5p55		7.80E + 09	0.04	0.79	D	
887.057	500		112 732.3	4d51	5p73		6.69E + 08	1.11	0.46	D+	
891.516	5000		112 168.5	4d85	5p63	891.5150	0.0020	3.05E + 09	0.44	0.63	C
892.506	5		112 044.1	6s13	5p23		3.83E + 09	0.34	0.49	C	
914.995	20		109 290.2	4d85	5p27		3.91E + 08	1.30	0.47	D+	
921.000	2		108 577.6	6s33	5p51		1.79E + 09	0.64	0.60	C	
925.122	1	x	108 093.9	5d35	5p13		5.65E + 08	1.14	0.03	D+	
928.000	1		107 758.6	4d41	5p43		1.24E + 08	1.80	0.15	D+	
938.478	5000		106 555.5	4d83	5p51		2.04E + 09	0.57	0.49	C	



Table 1. (Continued.)

$\lambda_{\text{obs}}(\text{\AA})$	Intensity		$\sigma_{\text{obs}}(\text{cm}^{-1})$	Even level <sup>a</sup>	Odd level <sup>a</sup>	$\lambda_{\text{Ritz}}(\text{\AA})$	Unc( $\lambda_{\text{Ritz}}-\text{\AA}$ )	$g_U A(\text{s}^{-1})$	$\log(g_L f)$	ICFI	Acc.
943.213	100		106 020.6	4d85	5p45			3.05E + 08	1.38	0.30	D+
945.016	150		105 818.3	5d41	5p33			2.19E + 09	0.53	0.74	C
(955.500)		A	(104 657.28)	4d73	5p41			1.05E + 09	0.85	0.32	C
972.924	5000	p	102 783.0	4d41	5p33			2.28E + 08	1.49	0.33	D+
973.902	5		102 679.7	5d31	5p11			1.21E + 08	1.76	0.01	D+
983.256	50	x	101 702.9	5d35	5p17			7.73E + 07	1.95	0.04	D+
988.431	5000		101 170.4	4d85	5p53			5.81E + 08	1.07	0.57	D+
990.984	1000		100 909.8	4d83	5p73			4.24E + 08	1.20	0.19	D+
991.356	50		100 871.9	4d73	5p35			4.03E + 07	2.23	0.14	D+
992.272	2000		100 778.8	5d25	5p13			1.82E + 09	0.57	0.11	C
1009.339	200		99 074.74	5d73	5p45			2.04E + 09	0.51	0.64	C
1012.720	1000		98 743.98	4d85	5p43			4.34E + 08	1.17	0.19	D+
1017.202	500		98 308.89	5d55	5p23			8.45E + 08	0.89	0.03	D
1020.467	1000		97 994.35	4d51	5p41			4.49E + 08	1.17	0.28	D+
1021.266	200		97 917.68	5s21	5p61			7.83E + 07	1.91	0.03	D+
1022.554	200		97 794.35	4d73	5p33			9.17E + 07	1.85	0.05	D+
1023.436	2		97 710.07	4d83	5p63			1.96E + 07	2.51	0.01	D+
1025.821	5000		97 482.89	5d75	5p45			1.07E + 10	0.23	0.73	C
1029.063	500		97 175.78	4d73	5p31			2.53E + 08	1.40	0.35	D+
1030.122	500		97 075.88	5d53	5p33			1.48E + 09	0.63	0.16	C
1032.576	1000		96 845.17	4d85	5p35			4.39E + 08	1.15	0.55	D+
1038.852	5000		96 260.10	5d55	5p33			2.90E + 09	0.33	0.20	C
1040.906	2000		96 070.15	5d27	5p15			3.87E + 09	0.20	0.36	C
1041.006	2000		96 060.93	5d23	5p11			6.16E + 09	0.00	0.60	C
1044.492	2000		95 740.32	5d43	5p21			7.26E + 09	0.08	0.47	C
1050.577	2000		95 185.79	5d11	5p13			6.10E + 09	0.00	0.91	C
1051.358	2000		95 115.08	4d73	5p21			8.84E + 07	1.84	0.09	D+
1052.487	100	D, x	95 013.05	5s13	5p51			5.10E + 07	2.07	0.02	D+
1053.458	500		94 925.47	5d45	5p33			2.32E + 09	0.41	0.24	D
1053.556	2000		94 916.64	5d25	5p25			8.76E + 09	0.16	0.72	C
1055.367	200		94 753.77	5s15	5p55			5.68E + 07	2.02	0.01	D+
1055.966	200	J	94 700.02	5d21	5p11			3.98E + 09	0.17	0.89	C
1059.473	2000		94 386.55	5d25	5p17			1.03E + 08	1.76	0.12	D+
1061.816	1000	dc	94 178.28	5d33	5p21			1.79E + 09	0.52	0.17	C
1061.816	1000	dc, J	94 178.28	5d57	5p27			1.13E + 10	0.28	0.78	C
1064.694	1000		93 923.70	5d35	5p23			4.46E + 09	0.12	0.22	C
1064.821	5000		93 912.50	5d13	5p13			1.28E + 10	0.34	0.88	C
1068.842	2000		93 559.20	5d31	5p21			6.85E + 09	0.07	0.93	C
1068.964	200		93 548.52	5d33	5p23			1.05E + 09	0.75	0.17	C
1072.874	5000		93 207.59	5d15	5p13			1.02E + 10	0.25	0.43	C
1073.192	2000		93 179.97	5d13	5p15			4.58E + 09	0.10	0.88	C
1074.556	1000	p	93 061.69	5d43	5p33			5.19E + 09	0.05	0.55	C
1081.130	1000	dc	92 495.81	5d17	5p15			2.21E + 10	0.59	0.61	C
1081.130	1000	dc	92 495.81	5d47	5p45			3.61E + 10	0.80	0.95	C
1081.395	5000		92 473.15	5d15	5p15			1.65E + 10	0.46	0.90	C
1084.707	500		92 190.79	5d83	5p61			1.48E + 10	0.42	0.94	C
1085.589	2000	p	92 115.89	5d33	5p31			1.32E + 10	0.37	0.92	C
1085.784	90		92 099.35	5d53	5p43			8.62E + 08	0.82	0.15	C
1088.440	2000		91 874.61	5d35	5p33			1.32E + 10	0.37	0.74	C
1088.758	1000		91 847.78	5d45	5p35			5.43E + 09	0.02	0.59	C
1090.297	500		91 718.13	4d85	5p23			3.06E + 08	1.26	0.18	D+
1092.917	500		91 498.26	5d31	5p31			7.50E + 08	0.87	0.14	C
1094.784	500		91 342.22	5s25	5p83			2.89E + 08	1.29	0.30	D+
1095.491	2000		91 283.27	5d55	5p43			1.30E + 10	0.37	0.76	C
1097.314	5		91 131.62	4d51	5p33			2.98E + 07	2.28	0.06	D+
1099.589	5000		90 943.07	5d27	5p25			3.23E + 10	0.77	0.98	C
1100.351	1000		90 880.09	5d31	5p33			9.06E + 08	0.79	0.37	C
1101.745	2000		90 765.10	5d11	5p11			2.82E + 09	0.29	0.49	C

Table 1. (Continued.)

$\lambda_{\text{obs}}(\text{\AA})$	Intensity		$\sigma_{\text{obs}}(\text{cm}^{-1})$	Even level <sup>a</sup>	Odd level <sup>a</sup>	$\lambda_{\text{Ritz}}(\text{\AA})$	Unc( $\lambda_{\text{Ritz}}-\text{\AA}$ )	$g_U A(\text{s}^{-1})$	$\log(g_L f)$	ICFI	Acc.
1104.807	200	x	90 513.55	4d51	5p31			5.83E + 07	1.98	0.16	D+
(1108.491)		B	(90 215.17)	5d53	5p41			1.16E + 10	0.34	0.90	C
1111.222	200		89 991.02	5d83	5p83			2.82E + 09	0.28	0.78	C
1111.745	200		89 948.68	5d45	5p43			1.34E + 09	0.60	0.07	D
(1113.735)		E	(89 787.93)	5d65	5p63			1.13E + 10	0.32	0.79	C
1114.480	2000		89 727.94	5d73	5p73			7.73E + 09	0.16	0.70	C
1114.688	10 000	J	89 711.20	5d19	5p17			4.43E + 10	0.92	0.99	C
1115.161	1000		89 673.15	5d53	5p53			1.16E + 09	0.67	0.32	C
1115.532	2000		89 643.33	5d29	5p27			4.44E + 10	0.92	1.00	C
1116.101	1000		89 597.63	5d85	5p83			2.49E + 10	0.67	0.98	C
1117.413	1000		89 492.43	5d13	5p11			1.66E + 09	0.51	0.20	C
1118.689	2000		89 390.35	5d37	5p35			3.49E + 10	0.82	0.99	C
1118.987	500	D, x	89 366.54	5s13	5p73			6.71E + 07	1.90	0.01	D+
1125.394	2000		88 857.77	5d55	5p53			5.54E + 09	0.02	0.36	D+
1126.166	500		88 796.86	5d35	5p35			1.19E + 09	0.65	0.11	C
(1127.231)		G	(88 712.97)	5d51	5p73			2.14E + 09	0.39	0.57	C
(1129.374)		C	(88 544.61)	5d63	5p63			7.98E + 09	0.18	0.62	C
1134.603	2000		88 136.56	5d75	5p73			1.17E + 10	0.35	0.65	C
1135.257	500		88 085.78	5d43	5p43			9.15E + 08	0.75	0.10	C
1141.121	1000		87 633.13	5d75	5p55			3.11E + 09	0.22	0.33	D
1142.544	5000		87 523.98	5d45	5p53			1.45E + 10	0.46	0.73	C
1143.696	1000		87 435.82	4d73	5p25			1.58E + 07	2.51	0.04	D+
1143.930	2000		87 417.94	5d41	5p63			3.49E + 09	0.16	0.57	C
1144.579	5000		87 368.37	5d17	5p25			3.33E + 09	0.18	0.25	C
1150.770	2000		86 898.34	5d35	5p43			7.27E + 09	0.16	0.67	C
1151.571	2000		86 837.89	5d17	5p17			1.13E + 10	0.35	0.99	C
1151.851	1000		86 816.78	5d15	5p17			1.81E + 09	0.45	0.83	C
1154.620	2000		86 608.58	5d25	5p23			1.26E + 10	0.40	0.59	C
1154.902	1000		86 587.43	5d65	5p73			2.10E + 09	0.38	0.21	C
1155.225	1000		86 563.22	4d41	5p13			6.92E + 07	1.86	0.23	D+
1158.574	2000		86 313.00	5d23	5p23			6.05E + 09	0.08	0.76	C
(1161.638)		F	(86 085.32)	5d65	5p55			8.72E + 09	0.24	0.53	D+
1162.848	1000		85 995.76	4d73	5p11			9.04E + 07	1.75	0.08	D+
1164.083	500		85 904.53	5d31	5p43			2.39E + 08	1.32	0.10	D+
1167.411	2000		85 659.63	5d43	5p53			2.74E + 09	0.25	0.39	C
1187.404	50	x	84 217.33	5d41	5p73			1.15E + 09	0.61	0.81	C
(1189.322)		I	(84 081.49)	5d73	5p51			4.76E + 09	0.04	0.74	C
1204.078	150	H, x	83 051.10	5d51	5p51			4.76E + 09	0.00	0.86	C
1314.039	10		76 101.24	5s23	5p63			1.45E + 09	0.43	0.68	C
1330.353	1	x	75 168.02	5s13	5p53			7.65E + 08	0.69	0.18	C
1406.536	10		71 096.65	5s21	5p63			2.55E + 08	1.12	0.65	D+
1411.561	5		70 843.56	5s13	5p35			1.64E + 08	1.31	0.02	D+
1416.418	500		70 600.63	5s15	5p23			4.67E + 08	0.85	0.20	C
1417.866	2000		70 528.53	5s33	5p51			2.39E + 09	0.14	0.84	C
1483.078	500		67 427.34	5s11	5p53			4.13E + 08	0.87	0.27	C
1489.263	100		67147.31	5s13	5p31			2.61E + 08	1.06	0.15	C
1495.035	50		66 888.07	5s11	5p41			1.55E + 08	1.29	0.35	D+
1514.569	50 000		66 025.38	5s25	5p55			5.87E + 09	0.31	0.74	D+
1521.702	10 000		65 715.89	5s13	5p23			2.94E + 09	0.01	0.63	C
1526.201	5000		65 522.17	5s25	5p73			1.39E + 09	0.31	0.84	C
1529.397	5000		65 385.25	5s33	5p55			1.53E + 09	0.27	0.87	D
1536.037	2000		65 102.60	5s23	5p53			1.04E + 09	0.44	0.36	C
1538.423	5000		65 001.63	5s11	5p43			2.19E + 09	0.11	0.91	C
1541.255	10 000		64 882.19	5s33	5p73			3.10E + 09	0.05	0.62	C
1548.859	2000		64 563.66	5s23	5p41			1.73E + 08	1.21	0.12	D+
1591.797	50000		62 822.08	5s15	5p17			8.70E + 09	0.52	0.97	C
1595.481	50		62 677.02	5s23	5p43			2.75E + 08	0.98	0.10	C
1604.549	20 000		62 322.81	5s25	5p63			1.63E + 09	0.20	0.42	C

Table 1. (Continued.)

$\lambda_{\text{obs}}(\text{\AA})$	Intensity	$\sigma_{\text{obs}}(\text{cm}^{-1})$	Even level <sup>a</sup>	Odd level <sup>a</sup>	$\lambda_{\text{Ritz}}(\text{\AA})$	Unc( $\lambda_{\text{Ritz}}-\text{\AA}$ )	$g_{\text{L}}A(\text{s}^{-1})$	$\log(g_{\text{L}}f)$	ICFI	Acc.
1605.358	10	62 291.40	5s15	5p25			1.29E + 08	1.30	0.06	D+
1621.198	20 000	61 682.78	5s33	5p63			1.28E + 09	0.30	0.49	C
1621.441	20000	61 673.54	5s31	5p83			3.96E + 09	0.19	0.96	C
1645.331	50 000	60 778.04	5s23	5p35			5.80E + 09	0.37	0.97	C
1663.953	50 000	60 097.85	5s21	5p53			2.02E + 09	0.08	0.93	C
1665.978	20000	60 024.80	5s11	5p33			8.35E + 08	0.46	0.54	C
1679.024	20 000	59 558.41	5s21	5p41			1.35E + 09	0.25	0.94	C
1681.349	10000	59 476.05	5s31	5p61			1.84E + 09	0.11	0.97	C
1682.238	50 000	59 444.62	5s25	5p27			7.47E + 09	0.50	0.98	C
1683.307	20 000	59 406.87	5s11	5p31			1.48E + 09	0.20	0.94	C
1724.855	1000	57 975.89	5s11	5p23			6.61E + 08	0.53	0.36	C
1733.090	50 000	57 700.41	5s23	5p33			1.77E + 09	0.10	0.65	C
1733.928	50000	57 672.52	5s21	5p43			1.09E + 09	0.31	0.65	C
1741.944	100 000	57407.13	5s13	5p25			5.00E + 09	0.36	0.98	C
1749.353	50 000	57 163.99	5s15	5p15			4.87E + 09	0.35	0.96	C
1751.844	50	57 082.71	5s23	5p31			1.76E + 08	1.09	0.16	C
1772.078	50 000	56 430.92	5s15	5p13			2.43E + 09	0.06	0.92	C
1780.139	2000	56 175.39	5s25	5p45			9.92E + 08	0.32	0.95	C
1786.788	20000	55 966.35	5s13	5p11			1.38E + 09	0.19	0.95	C
1800.659	50 000	55 535.22	5s33	5p45			3.62E + 09	0.25	0.78	C
1817.490	5000	55 020.94	5s23	5p21			1.22E + 09	0.22	0.96	C
1940.003	10 000	51 546.31	5s13	5p13			4.54E + 08	0.59	0.35	C
1974.492	3 h	50 645.94	5s21	5p23			2.04E + 08	0.92	0.19	C

<sup>a</sup> Level codes are explained in table 2.

Symbols: dc, doubly classified; p, perturbed; u, unresolved from close line; s, shaded to shorter wavelength;  $\ell$ , shaded to longer wavelength; x, not included in level optimization; h, hazy.

A, not observed due to break in spectrum—Ritz value.

B, greatly perturbed by Si III line—Ritz value.

C, covered by ghost of Si IV line—Ritz value.

D, intensity much higher than expected, not used in level optimization.

E, covered by ghost of Zr V line—Ritz value.

F, covered by Si III line—Ritz value.

G, covered by ghost of Si IV line—Ritz value.

H, uncertain classification, not included in level optimization.

I, covered by neighboring strong lines—Ritz value.

J, even level for this line not included in least-squares fit.

### 3.3. $4s^2 4p^4 5p$ levels

As already mentioned, all levels of this configuration were given in [6]. However, we find that 13 of the 21 levels of this configuration given in [6] were spurious. The following levels from [6] have been replaced by new levels in table 2. (We use here the LS designations from [6], although for this coupling scheme, it is not possible to specify the  $J$ -value of the core term.):

- (1) ( $^3P_2$ ) $^4P_{3/2}$  at 423 114; now 5p13 at 421 257.96  $\text{cm}^{-1}$
- (2) ( $^3P_2$ ) $^4P_{5/2}$  at 424 592; now 5p15 at 421 991.19  $\text{cm}^{-1}$
- (3) ( $^3P_1$ ) $^2P_{1/2}$  at 436 172; now 5p21 at 434 797.76  $\text{cm}^{-1}$
- (4) ( $^3P_0$ ) $^4D_{3/2}$  at 437 474; now 5p23 at 435 427.69  $\text{cm}^{-1}$
- (5) ( $^3P_0$ ) $^4D_{1/2}$  at 438 427; now 5p31 at 436 859.11  $\text{cm}^{-1}$
- (6) ( $^3P_2$ ) $^2P_{3/2}$  at 440 224; now 5p33 at 437 477.01  $\text{cm}^{-1}$
- (7) ( $^3P_0$ ) $^4S_{3/2}$  at 444 078; now 5p43 at 442 453.66  $\text{cm}^{-1}$
- (8) ( $^3P_1$ ) $^2D_{3/2}$  at 445 849; now 5p53 at 444 879.34  $\text{cm}^{-1}$
- (9) ( $^3P_1$ ) $^2S_{1/2}$  at 447 709; now 5p41 at 444 340.07  $\text{cm}^{-1}$
- (10) ( $^1D_2$ ) $^2F_{7/2}$  at 452 408; now 5p27 at 452 999.87  $\text{cm}^{-1}$

- (11) ( $^1D_2$ ) $^2P_{3/2}$  at 472 926; now 5p73 at 459 077.64  $\text{cm}^{-1}$
- (12) ( $^1S_0$ ) $^2P_{3/2}$  at 483 178; now 5p83 at 484 897.26  $\text{cm}^{-1}$
- (13) ( $^1S_0$ ) $^2P_{1/2}$  at 487 131; now 5p61 at 482 699.28  $\text{cm}^{-1}$

The structure of the  $4p^4 5p$  levels is shown in figure 4. The levels are designated in  $jl$ -coupling.

### 3.4. $4s^2 4p^4 5d$ and $4s^2 4p^4 6s$ levels

The structures of the  $4p^4 5d$  and  $4p^4 6s$  configurations are shown in figure 5. As these configurations lie very close in energy, we treat them together.

A number of  $4p^4 5d$  and  $4p^4 6s$  levels were established by Chaghtai *et al* [5], based on their observation of resonance lines in the 174–200  $\text{\AA}$  region. They reported almost all of the levels that could make transitions to the ground term, that is levels with  $J = 1/2, 3/2$  or  $5/2$ . Only  $4p^4(^3P)5d^4D_{5/2}$  was missing. These levels were given again in [6], some with improved accuracy. Our present work confirms most of these levels, improves their accuracies, and provides values for the

**Table 2.** Odd parity energy levels ( $\text{cm}^{-1}$ ) of Zr VI.

Configuration	Term	$J$	Desig. <sup>a</sup>	Energy	Uncert.	No. trans. <sup>b</sup>
$4s^2 4p^5$	$^2P$	3/2	p5 3	0.00	0.80	55
		1/2	p5 1	15 602.78	0.97	32
$4s^2 4p^4 5p$	$(^3P_2)[1]$	3/2	5p13	421 257.96	0.12	20
		5/2	5p15	421 991.19	0.19	17
	$(^3P_2)[1]$	1/2	5p11	425 678.16	0.18	15
		5/2	5p25	427 118.65	0.14	17
	$(^3P_2)[3]$	7/2	5p17	427 649.11	0.20	13
		1/2	5p21	434 797.76	0.21	12
	$(^3P_2)[2]$	3/2	5p23	435 427.69	0.15	20
		1/2	5p31	436 859.11	0.16	13
	$(^3P_1)[2]$	3/2	5p33	437 477.01	0.13	26
		5/2	5p35	440 554.88	0.17	20
	$(^3P_0)[1]$	3/2	5p43	442 453.66	0.15	24
		1/2	5p41	444 340.07	0.17	10
	$(^3P_1)[1]$	3/2	5p53	444 879.34	0.13	20
		5/2	5p45	449 730.72	0.12	16
	$(^1D_2)[3]$	7/2	5p27	452 999.87	0.21	11
		3/2	5p63	455 878.16	0.12	19
	$(^1D_2)[2]$	3/2	5p73	459 077.64	0.15	20
		5/2	5p55	459 580.77	0.14	15
	$(^1D_2)[1]$	1/2	5p51	464 724.05	0.25	9
		1/2	5p61	482 699.28	0.36	6
$(^1S_0)[1]$	3/2	5p83	484 897.26	0.33	9	

<sup>a</sup> Designations are given with a short form of the configuration (two places) followed by the ordinal number of the calculated  $J$  value for the configuration (one place) and the  $J$  value (one place). For example 5p73 indicates the seventh level with  $J = 3/2$  for the  $4p^4 5p$  configuration. p5 3 and p5 1 indicate the  $J = 3/2$  and  $1/2$  levels of the  $4p^5$  configuration, respectively.

<sup>b</sup> Total number of transitions for each level, including those omitted from the level optimization procedure.

$J = 7/2, 9/2$  levels, which cannot radiate to the ground term. Five of the levels of [5, 6] were found to be spurious, and several  $J$ -values were revised. The spurious levels were  $4p^4(^3P)5d\ ^4P_{1/2}$ ,  $4p^4(^1S)5d\ ^2D_{3/2}$ ,  $4p^4 6s\ (^3P_2)_{5/2}$ ,  $4p^4 6s\ (^3P_0)_{1/2}$ , and  $4p^4 6s\ (^1S_0)_{1/2}$  (designations from [6]). We confirm the level  $4p^4 6s(^1D_2)_{5/2}$  given in [5] ( $573\ 105\ \text{cm}^{-1}$ ), but reject the revised value given in [6] ( $573\ 135\ \text{cm}^{-1}$ ). Our present value is  $573\ 101.84\ \text{cm}^{-1}$ .

Our results for the  $4p^4 5d$  and  $4p^4 6s$  levels are given in table 3. Although this is a complete set, for some levels only tentative values can be given:

- (1) The  $4p^4 5d\ (^3P_2)[0]_{1/2}$  level (5d21) is established by two lines:  $192.182\ \text{\AA}$  to p5 3 and  $1055.966\ \text{\AA}$  to 5p11. However, the  $192.182\ \text{\AA}$  line is largely obscured by a strong line of O IV and so was given a large uncertainty in the level optimization. The value of  $4p^4 5d\ (^3P_2)[0]_{1/2}$  is thus based almost entirely on  $1055.966\ \text{\AA}$ , 5d21–5p11. A possible confirming transition predicted at  $1008.876\ \text{\AA}$ , 5d21–5p13, was not observed. This could occur because of our use of a filter to eliminate higher order lines that has low-wavelength cutoff near  $1000\ \text{\AA}$ . The level is thus uncertain and was not included in the LSF.
- (2) The  $4p^4 5d\ (^1D_2)[4]_{7/2}$  level (5d47) is established by a single line,  $1081.130\ \text{\AA}$ , 5d47–5p45. This transition is

predicted to be extremely strong, so this is likely correct. However,  $1081.130\ \text{\AA}$  is also classified as 5d17–5p15. We thus consider  $4p^4 5d\ (^1D_2)[4]_{7/2}$  to be tentative and exclude it from the LSF.

- (3) The  $4p^4 5d\ (^1D_2)[3]_{7/2}$  level (5d57) is established by a single line,  $1061.816\ \text{\AA}$ , 5d57–5p27. This transition is predicted to be strong, so this is likely correct. A possible confirming transition 5d55–5d57 cannot be observed due to the presence of a strong line of Si III. Unfortunately,  $1061.816\ \text{\AA}$  is also classified as 5d33–5p21, which makes our value for 5d57 tentative at best. It was not included in the LSF.
- (4) The  $4p^4 5d\ (^3P_2)[4]_{9/2}$  level (5d19) is established by a single line,  $1114.688\ \text{\AA}$ , 5d19–5p17. This transition is predicted to be strong, so this is likely correct. However, since there are no confirming transitions, we consider the level to be tentative.
- (5) The  $4p^4 5d\ (^1D_2)[4]_{9/2}$  level (5d29) is established by a single line,  $1115.532\ \text{\AA}$ , 5d29–5p27. This transition is predicted to be strong, so this is likely correct. However, since there are no confirming transitions, we consider the level to be tentative.

As can be seen, the lines that establish 5d19 and 5d29,  $1114.688\ \text{\AA}$  and  $1115.532\ \text{\AA}$ , have nearly the same wavelength. The matching of these two lines with the 5d19 and

**Table 3.** Even parity energy levels ( $\text{cm}^{-1}$ ) of Zr VI.

Configuration	Term	$J$	Desig.	Energy	Note <sup>a</sup>	Uncert.	No. trans. <sup>b</sup>	
4s4p <sup>6</sup> 4s <sup>2</sup> 4p <sup>4</sup> 4d	<sup>2</sup> S	1/2	4p61	191 570.67		0.89	8	
	( <sup>3</sup> P) <sup>4</sup> D	5/2	4d15	248 940.11		0.85	6	
	( <sup>3</sup> P) <sup>4</sup> D	7/2	4d17	249 322.89		0.90	4	
	( <sup>3</sup> P) <sup>4</sup> D	3/2	4d13	250 017.63		0.79	9	
	( <sup>3</sup> P) <sup>4</sup> D	1/2	4d11	251 818.7		1.3	5	
	( <sup>3</sup> P) <sup>4</sup> F	9/2	4d19	261 642.9		1.4	1	
	( <sup>3</sup> P) <sup>4</sup> F	7/2	4d27	266 145.41		0.71	5	
	( <sup>1</sup> D) <sup>2</sup> P	1/2	4d21	266 278.49		0.73	9	
	( <sup>3</sup> P) <sup>4</sup> F	3/2	4d23	271 296.05		0.57	13	
	( <sup>3</sup> P) <sup>4</sup> F	5/2	4d25	271 374.36		0.72	8	
	( <sup>3</sup> P) <sup>4</sup> P	1/2	4d31	272 091.26		0.73	7	
	( <sup>3</sup> P) <sup>4</sup> P	3/2	4d33	272 834.44		0.69	10	
	( <sup>1</sup> D) <sup>2</sup> D	3/2	4d43	274 665.60		0.50	11	
	( <sup>3</sup> P) <sup>2</sup> F	7/2	4d37	276 491.34		0.69	6	
	( <sup>3</sup> P) <sup>4</sup> P	5/2	4d35	278 742.23		0.47	10	
	( <sup>1</sup> D) <sup>2</sup> P	3/2	4d53	279 457.21		0.41	14	
	( <sup>1</sup> D) <sup>2</sup> D	5/2	4d45	283 112.00		0.39	12	
	( <sup>1</sup> D) <sup>2</sup> G	7/2	4d47	285 967.09		0.65	4	
	( <sup>1</sup> D) <sup>2</sup> G	9/2	4d29	286 411.5		1.4	1	
	( <sup>3</sup> P) <sup>2</sup> F	5/2	4d55	287 142.42		0.52	9	
	( <sup>1</sup> D) <sup>2</sup> F	5/2	4d65	299 608.66		0.45	9	
	( <sup>1</sup> D) <sup>2</sup> F	7/2	4d57	303 517.22		0.48	6	
	( <sup>1</sup> S) <sup>2</sup> D	3/2	4d63	319 336.18		0.60	8	
	( <sup>1</sup> S) <sup>2</sup> D	5/2	4d75	325 576.82		0.75	4	
	( <sup>1</sup> D) <sup>2</sup> S	1/2	4d41	334 694.92		0.33	7	
	( <sup>3</sup> P) <sup>2</sup> P	3/2	4d73	339 682.78		0.21	11	
	( <sup>3</sup> P) <sup>2</sup> D	5/2	4d85	343 709.55		0.22	11	
	( <sup>3</sup> P) <sup>2</sup> P	1/2	4d51	346 345.56		0.42	7	
	( <sup>3</sup> P) <sup>2</sup> D	3/2	4d83	358 168.09		0.32	7	
	4s <sup>2</sup> 4p <sup>4</sup> 5s	( <sup>3</sup> P <sub>2</sub> )[2]	5/2	5s15	364 827.11		0.12	7
		( <sup>3</sup> P <sub>2</sub> )[2]	3/2	5s13	369 711.65		0.11	11
		( <sup>3</sup> P <sub>0</sub> )[0]	1/2	5s11	377 452.05		0.12	8
		( <sup>3</sup> P <sub>1</sub> )[1]	3/2	5s23	379 776.65		0.11	10
( <sup>3</sup> P <sub>1</sub> )[1]		1/2	5s21	384 781.44		0.16	8	
( <sup>1</sup> D <sub>2</sub> )[2]		5/2	5s25	393 555.34		0.11	7	
( <sup>1</sup> D <sub>2</sub> )[2]		3/2	5s33	394 195.47		0.11	7	
( <sup>1</sup> S <sub>0</sub> )[0]		1/2	5s31	423 223.46		0.33	4	
4s <sup>2</sup> 4p <sup>4</sup> 5d		( <sup>3</sup> P <sub>2</sub> )[2]	5/2	5d15	514 465.31		0.46	3
		( <sup>3</sup> P <sub>2</sub> )[3]	7/2	5d17	514 487.01		0.30	3
	( <sup>3</sup> P <sub>2</sub> )[2]	3/2	5d13	515 170.73		0.31	4	
	( <sup>3</sup> P <sub>2</sub> )[1]	1/2	5d11	516 443.48		0.37	2	
	( <sup>3</sup> P <sub>2</sub> )[4]	9/2	5d19	517 360.31	*	0.45	1	
				517 292.44	#	0.45	1	
	( <sup>3</sup> P <sub>2</sub> )[4]	7/2	5d27	518 061.55		0.35	2	
	( <sup>3</sup> P <sub>2</sub> )[0]	1/2	5d21	520 378.18	*	0.48	2	
	( <sup>3</sup> P <sub>2</sub> )[1]	3/2	5d23	521 740.06		0.63	4	
	( <sup>3</sup> P <sub>2</sub> )[3]	5/2	5d25	522 035.99		0.34	5	
	( <sup>3</sup> P <sub>1</sub> )[1]	1/2	5d31	528 357.52		0.31	7	
	( <sup>3</sup> P <sub>0</sub> )[2]	3/2	5d33	528 976.13		0.44	4	
	( <sup>3</sup> P <sub>0</sub> )[2]	5/2	5d35	529 351.71		0.24	7	
	( <sup>3</sup> P <sub>1</sub> )[3]	7/2	5d37	529 945.22		0.43	1	
	( <sup>3</sup> P <sub>1</sub> )[1]	3/2	5d43	530 538.91		0.37	6	
	( <sup>3</sup> P <sub>1</sub> )[2]	5/2	5d45	532 402.86		0.34	5	
	( <sup>3</sup> P <sub>1</sub> )[3]	5/2	5d55	533 736.95		0.25	5	
	( <sup>3</sup> P <sub>1</sub> )[2]	3/2	5d53	534 552.78		0.29	5	
	( <sup>1</sup> D <sub>2</sub> )[4]	7/2	5d47	542 226.54	*	0.45	1	
	( <sup>1</sup> D <sub>2</sub> )[4]	9/2	5d29	542 643.20	*	0.45	1	
				542 711.07	#	0.45	1	
	( <sup>1</sup> D <sub>2</sub> )[0]	1/2	5d41	543 295.84		0.41	5	

Table 3. (Continued.)

Configuration	Term	$J$	Desig.	Energy	Note <sup>a</sup>	Uncert.	No. trans. <sup>b</sup>
4s <sup>2</sup> 4p <sup>4</sup> 6s	( <sup>1</sup> D <sub>2</sub> )[1]	3/2	5d63	544 423		10	2
	( <sup>1</sup> D <sub>2</sub> )[2]	5/2	5d65	545 666.07		0.78	5
	( <sup>1</sup> D <sub>2</sub> )[3]	7/2	5d57	547 178.00	*	0.50	1
	( <sup>1</sup> D <sub>2</sub> )[3]	5/2	5d75	547 213.94		0.28	4
	( <sup>1</sup> D <sub>2</sub> )[1]	1/2	5d51	547 791		11	3
	( <sup>1</sup> D <sub>2</sub> )[2]	3/2	5d73	548 805.54		0.33	4
	( <sup>1</sup> S <sub>0</sub> )[2]	5/2	5d85	574 494.88		0.52	2
	( <sup>1</sup> S <sub>0</sub> )[2]	3/2	5d83	574 889.14		0.74	3
	( <sup>3</sup> P <sub>2</sub> )[2]	5/2	6s15	545 413.52		0.77	3
	( <sup>3</sup> P <sub>2</sub> )[2]	3/2	6s13	547 471.92		0.42	5
	( <sup>3</sup> P <sub>0</sub> )[0]	1/2	6s11	558 208.73		0.48	4
	( <sup>3</sup> P <sub>1</sub> )[1]	3/2	6s23	559 356.47		0.41	6
	( <sup>3</sup> P <sub>1</sub> )[1]	1/2	6s21	561 050.32		0.41	5
	( <sup>1</sup> D <sub>2</sub> )[2]	5/2	6s25	573 101.84		0.48	6
	( <sup>1</sup> D <sub>2</sub> )[2]	3/2	6s33	573 301.14		0.35	6
	( <sup>1</sup> S <sub>0</sub> )[0]	1/2	6s31	602 661.0		4.0	3

<sup>a</sup> Designations are explained in table 2; 4p61 indicates the <sup>2</sup>S<sub>1/2</sub> level of 4s4p<sup>6</sup>.

<sup>b</sup> Total number of transitions for each level, including those omitted from the level optimization procedure.

Notes:

\*Tentative value; not included in least-squares fit.

#Alternate value for interchange of classifications of □1114.688 and 1115.532 Å.

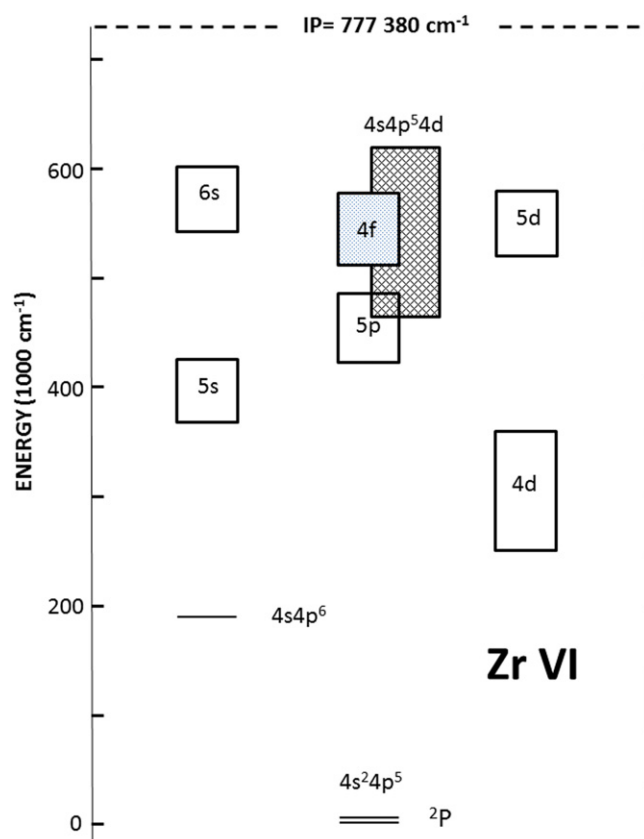


Figure 1. Schematic overview of the configurations of Zr VI. The calculated positions of the 4s<sup>2</sup>4p<sup>4</sup>4f and 4s4p<sup>5</sup>4d configurations, for which no levels are known, are also shown.

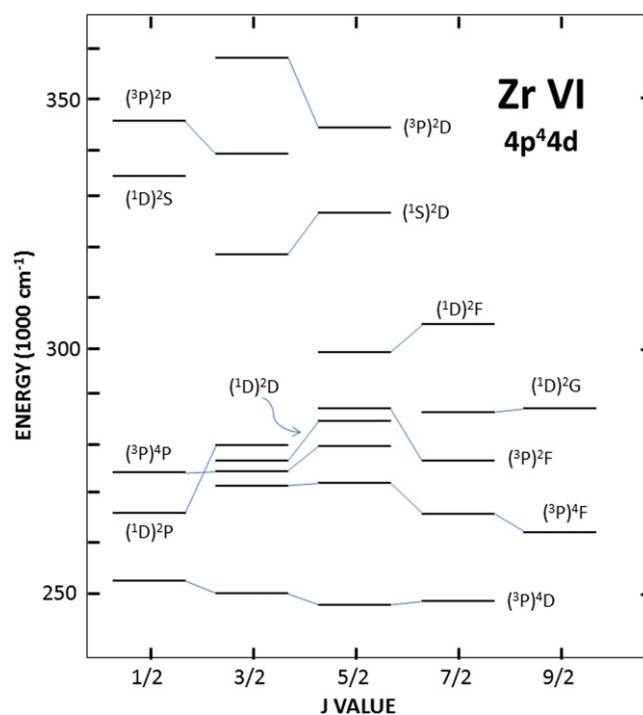
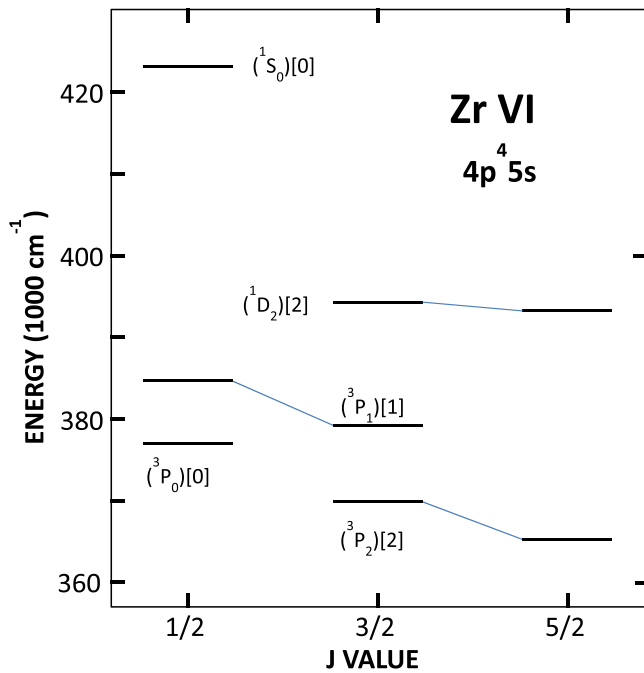
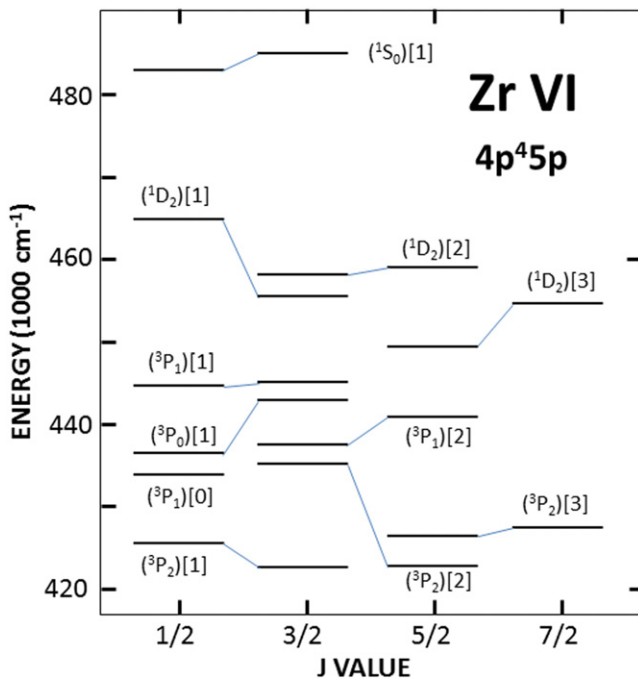


Figure 2. Structure of the 4s<sup>2</sup>4p<sup>4</sup>4d configurations of Zr VI.

5d29 levels was done so as to produce the best agreement with the LSF predictions. An effort was made to resolve the question by an isoelectronic comparison. However, the lines were again predicted to be so close that a clear resolution was



**Figure 3.** Structure of the  $4s^2 4p^4 5s$  configurations of Zr VI. The levels are designated in  $jl$ -coupling.

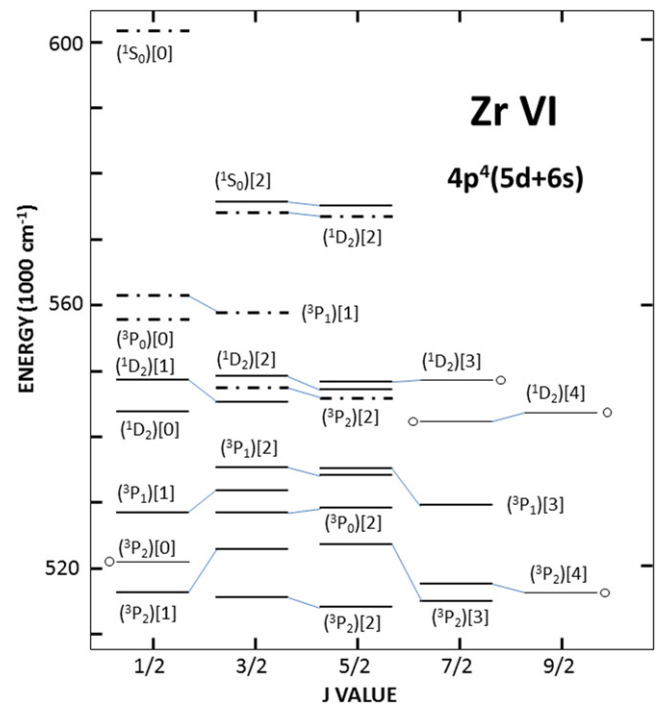


**Figure 4.** Structure of the  $4s^2 4p^4 5p$  configuration of Zr VI. The levels are designated in  $jl$ -coupling.

not possible. In table 3, we list alternative values for the 5d19 and 5d29 levels that would apply if the designations were interchanged.

### 3.5. Higher $4p^4 nd$ and $4p^4 ns$ levels

In [5] some levels of these configurations were located on the basis of resonance lines in the region around 159 Å. In [6] a



**Figure 5.** Structures of the  $4s^2 4p^4 5d$  and  $4s^2 4p^4 6s$  configurations of Zr VI. The levels are designated in  $jl$ -coupling. The  $4s^2 4p^4 6s$  levels are shown as dashed. Levels noted by open circles are tentative.

number of these levels were reported to make transitions to levels of  $4p^4 5p$ . In our present observations many of these lines do not appear as belonging to Zr VI, and we thus conclude that the results for these configurations in [5, 6] cannot be accepted without further confirmation.

## 4. Theoretical Interpretation

### 4.1. Odd parity configurations

As in [11] ‘the observed configurations were interpreted theoretically by making LSFs of the energy parameters to the observed levels with the Cowan suite of codes, RCN (Hartree–Fock), RCG (energy matrix diagonalization), and RCE (least-squares parameter fitting) [12]. The Hartree–Fock code was run in a relativistic mode (HFR) with a correlation term in the potential. Breit energies were not included. For the initial calculations the HFR values were scaled by a factor of 0.85 for the direct electrostatic parameters  $F^k$ , the exchange electrostatic parameters  $G^k$ , and the configuration interaction (CI) parameters  $R^k$ . The odd configurations  $4s^2 4p^5$ ,  $4s^2 4p^4 5p$ ,  $4s^2 4p^4 4f$ , and  $4s 4p^5 4d$  were treated as a single group.

The Hartree–Fock and LSF parameters for the odd configurations are given in table 4. For these calculations, the  $4p^4 5p$  exchange electrostatic parameters,  $G^0(4p5p)$  and  $G^2(4p5p)$ , were linked at their HFR ratio. The LSF/HFR ratio of 0.856 is satisfactory. The CI parameters for the  $4s^2 4p^5$ – $4s^2 4p^4 5p$  interaction were held fixed at their scaled HFR values. All other CI parameters and parameters for  $4s^2 4p^4 4f$

**Table 4.** Hartree–Fock and least-squares fitted parameters ( $\text{cm}^{-1}$ ) for the odd configurations of Zr VI. Mean error of fit  $229 \text{ cm}^{-1}$ .

Configuration	Parameter	HFR	LSF	Unc.	LSF/HFR
$4s^2 4p^5$	$E_{\text{av}}(4s^2 4p^5)$	9676	9927	172	
	$\zeta_{4p}$	9986	10481	217	1.049
$4s^2 4p^4 5p$	$E_{\text{av}}(4s^2 4p^4 5p)$	448691	443928	52	0.989
	$F^2(4p4p)$	84030	69669	504	0.829
	$\alpha(4p4p)$		$-59^{\text{a}}$		
	$\zeta_{4p}$	10556	10858	133	1.031
	$\zeta_{5p}$	2371	2725	108	1.148
	$F^2(4p5p)$	26016	24044	484	0.924
	$G^0(4p5p)$	5518	4725	62 <sup>b</sup>	0.856
	$G^2(4p5p)$	7441	6372	84 <sup>b</sup>	0.856
Config. interaction $4s^2 4p^5-4s^2 4p^4 5p$	$R^0(4p4p, 4p5p)$	2417	2054 <sup>c</sup>		0.850
	$R^2(4p4p, 4p5p)$	11574	9837 <sup>c</sup>		0.850

<sup>a</sup> Fixed at value from  $4p^4$  of Zr VII [15].<sup>b</sup> Linked in LSF fit.<sup>c</sup> Fixed at scaled HFR value.**Table 5.** Calculated energy levels ( $\text{cm}^{-1}$ ) and percentage compositions for the odd levels of Zr VI.

$J$	Observed	Calculated	O–C	% $jl$	Percentage composition (LS-coupling)					
3/2	0	0	0		99%	$4s^2 4p^5(^1S)^2P$				
1/2	15 603	15 603	0		99%	$4s^2 4p^5(^1S)^2P$	1%	$4s4p^5 4d(^1P)^2P$		
3/2	421 258	421 351	–93	40%( $^3P_2$ )[1]	63%	$4p^4 5p(^3P)^4P$	9%	$4p^4 5p(^3P)^4S$	9%	$4p^4 5p(^1D)^2P$
5/2	421 991	421 956	36	79%( $^3P_2$ )[2]	68%	$4p^4 5p(^3P)^4P$	24%	$4p^4 5p(^3P)^4D$	4%	$4p^4 5p(^1D)^2D$
1/2	425 678	426 061	–383	54%( $^3P_2$ )[1]	44%	$4p^4 5p(^3P)^4P$	24%	$4p^4 5p(^3P)^2P$	20%	$4p^4 5p(^1D)^2P$
5/2	427 119	427 158	–40	73%( $^3P_2$ )[3]	60%	$4p^4 5p(^3P)^2D$	15%	$4p^4 5p(^3P)4P$	13%	$4p^4 5p(^3P)^4D$
7/2	427 649	427 446	203	90%( $^3P_2$ )[3]	90%	$4p^4 5p(^3P)^4D$	10%	$4p^4 5p(^1D)^2F$		
1/2	434 798	434 708	89	55%( $^3P_1$ )[0]	38%	$4p^4 5p(^3P)^4P$	27%	$4p^4 5p(^3P)^4D$	17%	$4p^4 5p(^3P)^2P$
3/2	435 428	435 079	348	35%( $^3P_2$ )[2]	33%	$4p^4 5p(^3P)^4D$	23%	$4p^4 5p(^3P)^2D$	18%	$4p^4 5p(^3P)^2P$
1/2	436 859	436 807	52	57%( $^3P_0$ )[1]	56%	$4p^4 5p(^3P)^4D$	16%	$4p^4 5p(^3P)^4P$	15%	$4p^4 5p(^3P)^2S$
3/2	437 477	437 528	–51	35%( $^3P_1$ )[2]	49%	$4p^4 5p(^3P)^4D$	32%	$4p^4 5p(^3P)^2P$	10%	$4p^4 5p(^1D)^2P$
5/2	440 555	440408	147	96%( $^3P_1$ )[2]	60%	$4p^4 5p(^3P)^4D$	25%	$4p^4 5p(^3P)^2D$	14%	$4p^4 5p(^3P)^4P$
3/2	442 454	442 494	–40	67%( $^3P_0$ )[1]	25%	$4p^4 5p(^3P)^2D$	25%	$4p^4 5p(^3P)^4S$	17%	$4p^4 5p(^3P)^4P$
3/2	444 879	444 863	17	64%( $^3P_1$ )[1]	44%	$4p^4 5p(^3P)^2D$	43%	$4p^4 5p(^3P)^4S$	5%	$4p^4 5p(^3P)^4P$
1/2	444 340	444 928	–587	63%( $^3P_1$ )[1]	68%	$4p^4 5p(^3P)^2S$	13%	$4p^4 5p(^3P)^2P$	10%	$4p^4 5p(^3P)^4D$
5/2	449 731	449 565	166	84%( $^1D_2$ )[3]	84%	$4p^4 5p(^1D)^2F$	9%	$4p^4 5p(^3P)^2D$	4%	$4p^4 5p(^1D)^2D$
7/2	453 000	452 862	138	89%( $^1D_2$ )[3]	89%	$4p^4 5p(^1D)^2F$	10%	$4p^4 5p(^3P)^4D$		
3/2	455 878	455 924	–46	58%( $^1D_2$ )[1]	58%	$4p^4 5p(^1D)^2P$	20%	$4p^4 5p(^1D)^2D$	10%	$4p^4 5p(^3P)^2P$
3/2	459 078	458 938	139	71%( $^1D_2$ )[2]	71%	$4p^4 5p(^1D)^2D$	20%	$4p^4 5p(^3P)^2P$	8%	$4p^4 5p(^1D)^2P$
5/2	459 581	459 514	67	90%( $^1D_2$ )[2]	90%	$4p^4 5p(^1D)^2D$	4%	$4p^4 5p(^1D)^2F$	3%	$4p^4 5p(^3P)^4P$
1/2	464 724	464 776	–52	62%( $^1D_2$ )[1]	62%	$4p^4 5p(^1D)^2P$	34%	$4p^4 5p(^3P)^2P$	2%	$4p^4 5p(^1S)^2P$
1/2	482 699	482 755	–56	79%( $^1S_0$ )[1]	79%	$4p^4 5p(^1S)^2P$	9%	$4p^4 5p(^3P)^2P$	6%	$4p^4 5p(^3P)^4D$
3/2	484 897	484 952	–55	81%( $^1S_0$ )[1]	81%	$4p^4 5p(^1S)^2P$	4%	$4p^4 5p(^3P)^2D$	4%	$4p^4 5p(^3P)^4D$

and  $4s4p^5 4d$  were fixed at their scaled HFR values. The value of the effective interaction parameter  $\alpha(4p4p)$  for the  $4p^4 5p$  configuration was fixed at the value observed for the  $4p^4$  core of Zr VII [15]. In table 4 only values for the observed configurations  $4s^2 4p^5$  and  $4s^2 4p^4 5p$  are given.

The calculated level values and eigenvector compositions for the odd configurations are given in table 5. This table gives the percentage compositions for the three leading eigenvector states in LS-coupling and the percentage for the leading eigenvector state in  $jl$ -coupling. As can be seen there is not much mixing between the  $4s^2 4p^5$  and the  $4s^2 4p^4 5p$

configurations. Their mutual repulsion is only about  $320 \text{ cm}^{-1}$ .

#### 4.2. Even parity configurations

The parameters for the even configurations are given in table 6. Here, the  $4s4p^6$ ,  $4p^4 4d$ ,  $5s$ ,  $5d$ ,  $6s$ ,  $6d$ , and  $7s$  configurations were treated as single group. For the initial calculations the HFR values were scaled by a factor of 0.85 for the direct electrostatic parameters  $F^k$ , the exchange electrostatic parameters  $G^k$ , and the CI parameters  $R^k$ . All the



**Table 6.** Hartree–Fock and least-squares fitted parameters ( $\text{cm}^{-1}$ ) for the even configurations of Zr VI. Mean error of fit  $303 \text{ cm}^{-1}$ .

Configuration	Parameter	HF	LSF	Unc.	LSF/HFR
$4s4p^6$	$E_{\text{av}}(4s4p^6)$	238 204	225 794	545	0.945
$4s^24p^44d$	$E_{\text{av}}(4s^24p^44d)$	291 306	286 394	61	0.982
	$F^2(4p4p)$	82 691	68 538	720	0.829
	$\alpha(4p4p)$		$-59^{\text{a}}$		
	$\zeta_{4p}$	10 169	10 463	168	1.029
	$\zeta_{4d}$	719	853	81	1.186
	$F^2(4p4d)$	69 587	60 676	549	0.872
	$G^1(4p4d)$	86 663	69 960	180	0.807
	$G^3(4p4d)$	53 745	45 371	1036	0.844
$4s^24p^45s$	$E_{\text{av}}(4s^24p^45s)$	388 500	383 302	110	0.986
	$F^2(4p4p)$	83 691	69 792	1010	0.834
	$\alpha(4p4p)$		$-59^{\text{a}}$		
	$\zeta_{4p}$	10 481	10 832	274	1.033
	$G^1(4p5s)$	8701	7486	414	0.860
$4s^24p^45d$	$E_{\text{av}}(4s^24p^45d)$	538 379	533 803	70	0.991
	$F^2(4p4p)$	84 085	70 231	594	0.835
	$\alpha(4p4p)$		$-59^{\text{a}}$		
	$\zeta_{4p}$	10 550	10 927	141	1.036
	$\zeta_{5d}$	217	274	76	1.265
	$F^2(4p5d)$	19 526	16 999	721	0.871
	$G^1(4p5d)$	10 862	7658 <sup>b</sup>	275	0.705
	$G^3(4p5d)$	8028	5660 <sup>b</sup>	203	0.705
$4s^24p^46s$	$E_{\text{av}}(4s^24p^46s)$	566 615	562 487	112	0.992
	$F^2(4p4p)$	84 157	69 956	914	0.831
	$\alpha(4p4p)$		$-59^{\text{a}}$		
	$\zeta_{4p}$	10 581	11 023	237	1.042
	$G^1(4p6s)$	2783	2415	380	0.868
Config. interaction					
$4s4p^6-4s^24p^44d$	$R^1(4p4p, 4s4d)$	95 949	74 285 <sup>c</sup>	461	0.774
$4s4p^6-4s^24p^45d$	$R^1(4p4p, 4s5d)$	32 261	24 977 <sup>c</sup>	155	0.774
$4s4p^6-4s^24p^45s$	$R^1(4p4p, 4s5s)$	3749	3186 <sup>d</sup>		0.850
$4s4p^6-4s^24p^46s$	$R^1(4p4p, 4s6s)$	875	744 <sup>d</sup>		0.850
$4s^24p^44d-4s^24p^45s$	$R^2(4p4d, 4p5s)$	-8467	-7197 <sup>d</sup>		0.850
	$R^1(4p4d, 5s4p)$	-1073	-912 <sup>d</sup>		0.850
$4s^24p^44d-4s^24p^46s$	$R^2(4p4d, 4p6s)$	-5150	-4378 <sup>d</sup>		0.850

<sup>a</sup> Fixed at value from  $4p^4$  of Zr VII [15].<sup>b, c</sup> Linked in groups in LSF fit.<sup>d</sup> Fixed at scaled HFR value.

parameters that were allowed to vary were well defined in the fit and have reasonable ratios to the HFR values. The exchange parameters  $G^1(4p5d)$  and  $G^3(4p5d)$  were linked at their HFR ratio. The CI parameters for the  $4s4p^6-4s^24p^44d$  and  $4s4p^6-4s^24p^45d$  interactions were also linked at their HFR ratio. The fitted values are reasonable. The other CI parameters and those for  $4p^46d$  and  $4p^47s$  were held fixed at their scaled HFR values. As described in [4] the interaction of  $4s4p^6\ ^2S_{1/2}$  with the  $4s^24p^4(^1D)4d\ ^2S$  level is great, with a mutual repulsion of  $\sim 33\,000 \text{ cm}^{-1}$ . On the other hand, interaction between  $4s4p^6$  and  $4s^24p^45d$  is negligible. The value of the effective interaction parameter  $\alpha(4p4p)$  for the  $4p^44d$ ,  $5s$ ,  $5d$ , and  $6s$  configurations was again fixed at the value observed for the  $4p^4$  core of Zr VII [15]. The calculated level values and eigenvector compositions for the even levels are given in table 7. This table gives the percentage compositions for the three leading eigenvector states in LS-coupling and the percentage for the leading eigenvector state in

$jl$ -coupling, where appropriate. As can be seen, the purity of the states of the  $4p^44d$  configuration in LS-coupling is low, leading to low leading percentages for many of the levels. In order to avoid duplicate names, we have used the second component for the level observed at  $279\,457 \text{ cm}^{-1}$  to designate the level. Even though the  $4p^45d$  and  $4p^46s$  configurations are practically coincident, there is not much mixing of states. The percentage compositions for the  $4s4p^6$ ,  $4s^24p^44d$ , and  $4s^24p^45s$  configurations are close to those given in [4].

### 5. $4s4p^6-4s^24p^45p$ transitions

Transitions between the  $4s4p^6$  and  $4s^24p^45p$  configurations are normally forbidden as two electron jumps. However, because of CI between  $4s4p^6$  and  $4s^24p^44d$ , they can in fact take place. We observe six of them in Zr VI. In lower members of the isoelectronic sequence, these transitions occur

**Table 7.** Calculated energy levels ( $\text{cm}^{-1}$ ) and percentage compositions for the even levels of Zr VI. Observed levels with asterisk were not included in the least-squares fits.

$J$	Observed	Calculated	O–C	% $jl$	Percentage composition (LS-coupling)					
1/2	191 571	191 569	2		77%	4s4p <sup>6</sup> ( <sup>2</sup> S) <sup>2</sup> S	23%	4p <sup>4</sup> 4d( <sup>1</sup> D) <sup>2</sup> S		
5/2	248 940	248 803	137		88%	4p <sup>4</sup> 4d( <sup>3</sup> P) <sup>4</sup> D	3%	4p <sup>4</sup> 4d( <sup>3</sup> P) <sup>4</sup> F	3%	4p <sup>4</sup> 4d( <sup>3</sup> P) <sup>4</sup> P
7/2	249 323	249 305	18		91%	4p <sup>4</sup> 4d( <sup>3</sup> P) <sup>4</sup> D	6%	4p <sup>4</sup> 4d( <sup>3</sup> P) <sup>4</sup> F	2%	4p <sup>4</sup> 4d( <sup>1</sup> D) <sup>2</sup> F
3/2	250 018	249 861	157		86%	4p <sup>4</sup> 4d( <sup>3</sup> P) <sup>4</sup> D	4%	4p <sup>4</sup> 4d( <sup>3</sup> P) <sup>4</sup> P	3%	4p <sup>4</sup> 4d( <sup>1</sup> D) <sup>2</sup> D
1/2	251 819	251 854	–35		85%	4p <sup>4</sup> 4d( <sup>3</sup> P) <sup>4</sup> D	7%	4p <sup>4</sup> 4d( <sup>1</sup> D) <sup>2</sup> P	5%	4p <sup>4</sup> 4d( <sup>3</sup> P) <sup>2</sup> P
9/2	26 1643	261 550	93		90%	4p <sup>4</sup> 4d( <sup>3</sup> P) <sup>4</sup> F	10%	4p <sup>4</sup> 4d( <sup>1</sup> D) <sup>2</sup> G		
7/2	266 145	265 981	164		66%	4p <sup>4</sup> 4d( <sup>3</sup> P) <sup>4</sup> F	17%	4p <sup>4</sup> 4d( <sup>3</sup> P) <sup>2</sup> F	13%	4p <sup>4</sup> 4d( <sup>1</sup> D) <sup>2</sup> G
1/2	266 279	267 364	–1085		44%	4p <sup>4</sup> 4d( <sup>1</sup> D) <sup>2</sup> P	37%	4p <sup>4</sup> 4d( <sup>3</sup> P) <sup>2</sup> P	14%	4p <sup>4</sup> 4d( <sup>3</sup> P) <sup>4</sup> D
3/2	271 296	271 001	295		47%	4p <sup>4</sup> 4d( <sup>3</sup> P) <sup>4</sup> F	16%	4p <sup>4</sup> 4d( <sup>3</sup> P) <sup>4</sup> P	13%	4p <sup>4</sup> 4d( <sup>1</sup> S) <sup>2</sup> D
5/2	271 374	271 025	349		93%	4p <sup>4</sup> 4d( <sup>3</sup> P) <sup>4</sup> F	3%	4p <sup>4</sup> 4d( <sup>3</sup> P) <sup>4</sup> D	2%	4p <sup>4</sup> 4d( <sup>1</sup> S) <sup>2</sup> D
1/2	272 091	272 034	57		91%	4p <sup>4</sup> 4d( <sup>3</sup> P) <sup>4</sup> P	5%	4p <sup>4</sup> 4d( <sup>3</sup> P) <sup>2</sup> P	3%	4p <sup>4</sup> 4d( <sup>1</sup> D) <sup>2</sup> P
3/2	272 834	272 884	–50		38%	4p <sup>4</sup> 4d( <sup>3</sup> P) <sup>4</sup> P	30%	4p <sup>4</sup> 4d( <sup>3</sup> P) <sup>4</sup> F	18%	4p <sup>4</sup> 4d( <sup>1</sup> D) <sup>2</sup> P
3/2	274 666	274 573	93		36%	4p <sup>4</sup> 4d( <sup>1</sup> D) <sup>2</sup> D	21%	4p <sup>4</sup> 4d( <sup>3</sup> P) <sup>2</sup> D	15%	4p <sup>4</sup> 4d( <sup>3</sup> P) <sup>4</sup> F
7/2	276 491	276 813	–322		42%	4p <sup>4</sup> 4d( <sup>3</sup> P) <sup>2</sup> F	25%	4p <sup>4</sup> 4d( <sup>3</sup> P) <sup>4</sup> F	20%	4p <sup>4</sup> 4d( <sup>1</sup> D) <sup>2</sup> G
5/2	278 742	278 634	108		74%	4p <sup>4</sup> 4d( <sup>3</sup> P) <sup>4</sup> P	9%	4p <sup>4</sup> 4d( <sup>1</sup> S) <sup>2</sup> D	7%	4p <sup>4</sup> 4d( <sup>3</sup> P) <sup>2</sup> D
3/2	279 457	279 886	–429		40%	4p <sup>4</sup> 4d( <sup>3</sup> P) <sup>4</sup> P	24%	4p <sup>4</sup> 4d( <sup>1</sup> D) <sup>2</sup> P	22%	4p <sup>4</sup> 4d( <sup>3</sup> P) <sup>2</sup> P
5/2	283 112	282 808	304		41%	4p <sup>4</sup> 4d( <sup>1</sup> D) <sup>2</sup> D	21%	4p <sup>4</sup> 4d( <sup>3</sup> P) <sup>2</sup> D	18%	4p <sup>4</sup> 4d( <sup>3</sup> P) <sup>4</sup> P
7/2	285 967	285 629	338		65%	4p <sup>4</sup> 4d( <sup>1</sup> D) <sup>2</sup> G	24%	4p <sup>4</sup> 4d( <sup>3</sup> P) <sup>2</sup> F	10%	4p <sup>4</sup> 4d( <sup>1</sup> D) <sup>2</sup> F
9/2	286 412	285 935	477		90%	4p <sup>4</sup> 4d( <sup>1</sup> D) <sup>2</sup> G	10%	4p <sup>4</sup> 4d( <sup>3</sup> P) <sup>4</sup> F		
5/2	287 142	287 795	–653		65%	4p <sup>4</sup> 4d( <sup>3</sup> P) <sup>2</sup> F	21%	4p <sup>4</sup> 4d( <sup>1</sup> D) <sup>2</sup> F	9%	4p <sup>4</sup> 4d( <sup>1</sup> D) <sup>2</sup> D
5/2	299 609	299 713	–104		76%	4p <sup>4</sup> 4d( <sup>1</sup> D) <sup>2</sup> F	13%	4p <sup>4</sup> 4d( <sup>3</sup> P) <sup>2</sup> F	9%	4p <sup>4</sup> 4d( <sup>1</sup> D) <sup>2</sup> D
7/2	303 517	303 641	–124		80%	4p <sup>4</sup> 4d( <sup>1</sup> D) <sup>2</sup> F	17%	4p <sup>4</sup> 4d( <sup>3</sup> P) <sup>2</sup> F	2%	4p <sup>4</sup> 4d( <sup>1</sup> D) <sup>2</sup> G
3/2	319 336	319 335	1		63%	4p <sup>4</sup> 4d( <sup>1</sup> S) <sup>2</sup> D	25%	4p <sup>4</sup> 4d( <sup>1</sup> D) <sup>2</sup> D	5%	4p <sup>4</sup> 4d( <sup>1</sup> D) <sup>2</sup> P
5/2	325 577	325 582	–5		73%	4p <sup>4</sup> 4d( <sup>1</sup> D) <sup>2</sup> D	14%	4p <sup>4</sup> 4d( <sup>1</sup> D) <sup>2</sup> D	5%	4p <sup>4</sup> 4d( <sup>3</sup> P) <sup>4</sup> F
1/2	334 695	334 774	–79		69%	4p <sup>4</sup> 4d( <sup>1</sup> D) <sup>2</sup> S	20%	4s4p <sup>6</sup> ( <sup>2</sup> S) <sup>2</sup> S	5%	4p <sup>4</sup> 4d( <sup>1</sup> D) <sup>2</sup> P
3/2	339 683	339 272	411		50%	4p <sup>4</sup> 4d( <sup>3</sup> P) <sup>2</sup> P	36%	4p <sup>4</sup> 4d( <sup>1</sup> D) <sup>2</sup> P	7%	4p <sup>4</sup> 4d( <sup>1</sup> D) <sup>2</sup> D
5/2	343 710	344 309	–599		64%	4p <sup>4</sup> 4d( <sup>3</sup> P) <sup>2</sup> D	21%	4p <sup>4</sup> 4d( <sup>1</sup> D) <sup>2</sup> D	11%	4p <sup>4</sup> 4d( <sup>1</sup> S) <sup>2</sup> D
1/2	346 346	345 581	764		48%	4p <sup>4</sup> 4d( <sup>3</sup> P) <sup>2</sup> P	41%	4p <sup>4</sup> 4d( <sup>1</sup> D) <sup>2</sup> P	7%	4p <sup>4</sup> 4d( <sup>1</sup> D) <sup>2</sup> S
3/2	358 168	358 453	–285		57%	4p <sup>4</sup> 4d( <sup>3</sup> P) <sup>2</sup> D	19%	4p <sup>4</sup> 4d( <sup>1</sup> S) <sup>2</sup> D	14%	4p <sup>4</sup> 4d( <sup>1</sup> D) <sup>2</sup> D
5/2	364 827	364 804	23	92%( <sup>3</sup> P <sub>2</sub> )[2]	92%	4p <sup>4</sup> 5s( <sup>3</sup> P) <sup>4</sup> P	8%	4p <sup>4</sup> 5s( <sup>1</sup> D) <sup>2</sup> D		
3/2	369 712	369 708	4	82%( <sup>3</sup> P <sub>2</sub> )[2]	51%	4p <sup>4</sup> 5s( <sup>3</sup> P) <sup>2</sup> P	38%	4p <sup>4</sup> 5s( <sup>3</sup> P) <sup>4</sup> P	10%	4p <sup>4</sup> 5s( <sup>1</sup> D) <sup>2</sup> D
1/2	377 452	377 471	–19	63%( <sup>3</sup> P <sub>0</sub> )[0]	90%	4p <sup>4</sup> 5s( <sup>3</sup> P) <sup>4</sup> P	9%	4p <sup>4</sup> 5s( <sup>1</sup> S) <sup>2</sup> S		
3/2	379 777	379 741	36	92%( <sup>3</sup> P <sub>1</sub> )[1]	61%	4p <sup>4</sup> 5s( <sup>3</sup> P) <sup>4</sup> P	37%	4p <sup>4</sup> 5s( <sup>3</sup> P) <sup>2</sup> P	2%	4p <sup>4</sup> 5s( <sup>1</sup> D) <sup>2</sup> D
1/2	384 781	384 780	1	72%( <sup>3</sup> P <sub>1</sub> )[1]	94%	4p <sup>4</sup> 5s( <sup>3</sup> P) <sup>2</sup> P	5%	4p <sup>4</sup> 5s( <sup>1</sup> S) <sup>2</sup> S	1%	4p <sup>4</sup> 5s( <sup>3</sup> P) <sup>4</sup> P
5/2	393 555	393 590	–35	92%( <sup>1</sup> D <sub>2</sub> )[2]	92%	4p <sup>4</sup> 5s( <sup>1</sup> D) <sup>2</sup> D	8%	4p <sup>4</sup> 5s( <sup>3</sup> P) <sup>4</sup> P		
3/2	394 196	394 238	–42	87%( <sup>1</sup> D <sub>2</sub> )[2]	87%	4p <sup>4</sup> 5s( <sup>1</sup> D) <sup>2</sup> D	12%	4p <sup>4</sup> 5s( <sup>3</sup> P) <sup>2</sup> P	1%	4p <sup>4</sup> 5s( <sup>3</sup> P) <sup>4</sup> P
1/2	423 224	423 190	34	85%( <sup>1</sup> S <sub>0</sub> )[0]	85%	4p <sup>4</sup> 5s( <sup>1</sup> S) <sup>2</sup> S	8%	4p <sup>4</sup> 5s( <sup>3</sup> P) <sup>4</sup> P	6%	4p <sup>4</sup> 5s( <sup>3</sup> P) <sup>2</sup> P
5/2	514 465	514 521	–56	55%( <sup>3</sup> P <sub>2</sub> )[2]	70%	4p <sup>4</sup> 5d( <sup>3</sup> P) <sup>4</sup> D	10%	4p <sup>4</sup> 5d( <sup>3</sup> P) <sup>4</sup> F	10%	4p <sup>4</sup> 5d( <sup>3</sup> P) <sup>4</sup> P
7/2	514 487	514 569	–82	91%( <sup>3</sup> P <sub>2</sub> )[3]	73%	4p <sup>4</sup> 5d( <sup>3</sup> P) <sup>4</sup> D	19%	4p <sup>4</sup> 5d( <sup>3</sup> P) <sup>4</sup> F	6%	4p <sup>4</sup> 5d( <sup>1</sup> D) <sup>2</sup> F
3/2	515 171	515 206	–35	61%( <sup>3</sup> P <sub>2</sub> )[2]	59%	4p <sup>4</sup> 5d( <sup>3</sup> P) <sup>4</sup> D	20%	4p <sup>4</sup> 5d( <sup>3</sup> P) <sup>4</sup> P	6%	4p <sup>4</sup> 5d( <sup>1</sup> D) <sup>2</sup> D
1/2	516 444	516 516	–72	77%( <sup>3</sup> P <sub>2</sub> )[1]	43%	4p <sup>4</sup> 5d( <sup>3</sup> P) <sup>4</sup> D	27%	4p <sup>4</sup> 5d( <sup>3</sup> P) <sup>4</sup> P	17%	4p <sup>4</sup> 5d( <sup>3</sup> P) <sup>2</sup> P
9/2	517 360	* 517 149	211	90%( <sup>3</sup> P <sub>2</sub> )[4]	90%	4p <sup>4</sup> 5d( <sup>3</sup> P) <sup>4</sup> F	10%	4p <sup>4</sup> 5d( <sup>1</sup> D) <sup>2</sup> G		
7/2	518 062	* 517 900	162	87%( <sup>3</sup> P <sub>2</sub> )[4]	65%	4p <sup>4</sup> 5d( <sup>3</sup> P) <sup>2</sup> F	22%	4p <sup>4</sup> 5d( <sup>3</sup> P) <sup>4</sup> F	11%	4p <sup>4</sup> 5d( <sup>1</sup> D) <sup>2</sup> G
1/2	520 378	* 520 366	12	82%( <sup>3</sup> P <sub>2</sub> )[0]	53%	4p <sup>4</sup> 5d( <sup>3</sup> P) <sup>4</sup> P	29%	4p <sup>4</sup> 5d( <sup>3</sup> P) <sup>2</sup> P	11%	4p <sup>4</sup> 5d( <sup>1</sup> D) <sup>2</sup> S
3/2	521 740	521 749	–9	65%( <sup>3</sup> P <sub>2</sub> )[1]	37%	4p <sup>4</sup> 5d( <sup>3</sup> P) <sup>4</sup> P	34%	4p <sup>4</sup> 5d( <sup>3</sup> P) <sup>2</sup> D	13%	4p <sup>4</sup> 5d( <sup>3</sup> P) <sup>2</sup> P
5/2	522 036	521 991	45	54%( <sup>3</sup> P <sub>2</sub> )[3]	40%	4p <sup>4</sup> 5d( <sup>3</sup> P) <sup>2</sup> D	24%	4p <sup>4</sup> 5d( <sup>3</sup> P) <sup>2</sup> F	15%	4p <sup>4</sup> 5d( <sup>3</sup> P) <sup>4</sup> P
1/2	528 358	528 514	–156	88%( <sup>3</sup> P <sub>1</sub> )[1]	53%	4p <sup>4</sup> 5d( <sup>3</sup> P) <sup>4</sup> D	30%	4p <sup>4</sup> 5d( <sup>3</sup> P) <sup>2</sup> P	9%	4p <sup>4</sup> 5d( <sup>3</sup> P) <sup>4</sup> P
3/2	528 976	528 938	38	68%( <sup>3</sup> P <sub>0</sub> )[2]	69%	4p <sup>4</sup> 5d( <sup>3</sup> P) <sup>4</sup> F	12%	4p <sup>4</sup> 5d( <sup>3</sup> P) <sup>4</sup> D	11%	4p <sup>4</sup> 5d( <sup>1</sup> S) <sup>2</sup> D
5/2	529 352	529 301	51	52%( <sup>3</sup> P <sub>0</sub> )[2]	59%	4p <sup>4</sup> 5d( <sup>3</sup> P) <sup>4</sup> F	14%	4p <sup>4</sup> 5d( <sup>3</sup> P) <sup>4</sup> D	13%	4p <sup>4</sup> 5d( <sup>3</sup> P) <sup>4</sup> P
7/2	529 945	529 891	54	97%( <sup>3</sup> P <sub>1</sub> )[3]	54%	4p <sup>4</sup> 5d( <sup>3</sup> P) <sup>4</sup> F	23%	4p <sup>4</sup> 5d( <sup>3</sup> P) <sup>2</sup> F	22%	4p <sup>4</sup> 5d( <sup>3</sup> P) <sup>4</sup> D
3/2	530 539	530 479	60	59%( <sup>3</sup> P <sub>1</sub> )[1]	28%	4p <sup>4</sup> 5d( <sup>3</sup> P) <sup>4</sup> P	26%	4p <sup>4</sup> 5d( <sup>3</sup> P) <sup>4</sup> D	19%	4p <sup>4</sup> 5d( <sup>3</sup> P) <sup>2</sup> D
5/2	532 403	532 272	131	97%( <sup>3</sup> P <sub>1</sub> )[2]	52%	4p <sup>4</sup> 5d( <sup>3</sup> P) <sup>4</sup> P	27%	4p <sup>4</sup> 5d( <sup>3</sup> P) <sup>2</sup> F	11%	4p <sup>4</sup> 5d( <sup>3</sup> P) <sup>4</sup> F
5/2	533 737	533 656	81	59%( <sup>3</sup> P <sub>1</sub> )[3]	43%	4p <sup>4</sup> 5d( <sup>3</sup> P) <sup>2</sup> D	42%	4p <sup>4</sup> 5d( <sup>3</sup> P) <sup>2</sup> F	4%	4p <sup>4</sup> 5d( <sup>1</sup> S) <sup>2</sup> D
3/2	534 553	* 534 777	–224	46%( <sup>3</sup> P <sub>1</sub> )[2]	64%	4p <sup>4</sup> 5d( <sup>3</sup> P) <sup>2</sup> P	17%	4p <sup>4</sup> 5d( <sup>3</sup> P) <sup>2</sup> D	7%	4p <sup>4</sup> 5d( <sup>1</sup> D) <sup>2</sup> P
7/2	542 227	* 542 081	146	88%( <sup>1</sup> D <sub>2</sub> )[4]	88%	4p <sup>4</sup> 5d( <sup>1</sup> D) <sup>2</sup> G	8%	4p <sup>4</sup> 5d( <sup>3</sup> P) <sup>2</sup> F	3%	4p <sup>4</sup> 5d( <sup>3</sup> P) <sup>4</sup> F
9/2	542 643	* 542 576	67	90%( <sup>1</sup> D <sub>2</sub> )[4]	90%	4p <sup>4</sup> 5d( <sup>1</sup> D) <sup>2</sup> G	10%	4p <sup>4</sup> 5d( <sup>3</sup> P) <sup>4</sup> F		
1/2	543 296	543 203	93	79%( <sup>1</sup> D <sub>2</sub> )[0]	79%	4p <sup>4</sup> 5d( <sup>1</sup> D) <sup>2</sup> S	10%	4p <sup>4</sup> 5d( <sup>3</sup> P) <sup>4</sup> P	9%	4p <sup>4</sup> 5d( <sup>1</sup> D) <sup>2</sup> P
3/2	544 423	544 296	127	76%( <sup>1</sup> D <sub>2</sub> )[1]	76%	4p <sup>4</sup> 5d( <sup>1</sup> D) <sup>2</sup> P	7%	4p <sup>4</sup> 5d( <sup>3</sup> P) <sup>4</sup> P	6%	4p <sup>4</sup> 6s( <sup>3</sup> P) <sup>2</sup> P

Table 7. (Continued.)

$J$	Observed	Calculated	O–C	% $jl$	Percentage composition (LS-coupling)					
5/2	545 413	545 437	–23	91%( <sup>3</sup> P <sub>2</sub> )[2]	91%	4p <sup>4</sup> 6s( <sup>3</sup> P)4P	9%	4p <sup>4</sup> 6s( <sup>1</sup> D) <sup>2</sup> D		
5/2	545 666	545 709	–43	76%( <sup>1</sup> D <sub>2</sub> )[2]	76%	4p <sup>4</sup> 5d( <sup>1</sup> D) <sup>2</sup> D	17%	4p <sup>4</sup> 5d( <sup>1</sup> D) <sup>2</sup> F	2%	4p <sup>4</sup> 5d( <sup>3</sup> P) <sup>4</sup> D
5/2	547 214	547 087	127	73%( <sup>1</sup> D <sub>2</sub> )[3]	73%	4p <sup>4</sup> 5d( <sup>1</sup> D) <sup>2</sup> F	15%	4p <sup>4</sup> 5d( <sup>1</sup> D) <sup>2</sup> D	7%	4p <sup>4</sup> 5d( <sup>3</sup> P) <sup>2</sup> D
3/2	547 472	547 461	11	82%( <sup>3</sup> P <sub>2</sub> )[2]	63%	4p <sup>4</sup> 6s( <sup>3</sup> P) <sup>2</sup> P	20%	4p <sup>4</sup> 6s( <sup>3</sup> P) <sup>4</sup> P	9%	4p <sup>4</sup> 6s( <sup>1</sup> D) <sup>2</sup> D
7/2	547 178	547 229	–51	92%( <sup>1</sup> D <sub>2</sub> )[3]	92%	4p <sup>4</sup> 5d( <sup>1</sup> D) <sup>2</sup> F	3%	4p <sup>4</sup> 5d( <sup>3</sup> P) <sup>4</sup> D	2%	4p <sup>4</sup> 5d( <sup>3</sup> P) <sup>2</sup> F
1/2	547 791	547 844	–53	67%( <sup>1</sup> D <sub>2</sub> )[1]	67%	4p <sup>4</sup> 5d( <sup>1</sup> D) <sup>2</sup> P	23%	4p <sup>4</sup> 5d( <sup>3</sup> P) <sup>2</sup> P	8%	4p <sup>4</sup> 5d( <sup>1</sup> D) <sup>2</sup> S
3/2	548 806	549 016	–210	78%( <sup>1</sup> D <sub>2</sub> )[2]	78%	4p <sup>4</sup> 5d( <sup>1</sup> D) <sup>2</sup> D	18%	4p <sup>4</sup> 5d( <sup>3</sup> P) <sup>2</sup> D	1%	4p <sup>4</sup> 5d( <sup>1</sup> D) <sup>2</sup> P
1/2	558 209	558 212	–3	70%( <sup>3</sup> P <sub>0</sub> )[0]	86%	4p <sup>4</sup> 6s( <sup>3</sup> P) <sup>4</sup> P	12%	4p <sup>4</sup> 6s( <sup>1</sup> S) <sup>2</sup> S	2%	4p <sup>4</sup> 6s( <sup>3</sup> P) <sup>2</sup> P
3/2	559 357	559 340	17	99%( <sup>3</sup> P <sub>1</sub> )[1]	78%	4p <sup>4</sup> 6s( <sup>3</sup> P) <sup>4</sup> P	22%	4p <sup>4</sup> 6s( <sup>3</sup> P) <sup>2</sup> P		
1/2	561 050	561 077	–27	81%( <sup>3</sup> P <sub>1</sub> )[1]	92%	4p <sup>4</sup> 6s( <sup>3</sup> P) <sup>2</sup> P	4%	4p <sup>4</sup> 6s( <sup>3</sup> P) <sup>4</sup> P	3%	4p <sup>4</sup> 6s( <sup>1</sup> S) <sup>2</sup> S
5/2	573 102	573 108	–6	91%( <sup>1</sup> D <sub>2</sub> )[2]	91%	4p <sup>4</sup> 6s( <sup>1</sup> D) <sup>2</sup> D	9%	4p <sup>4</sup> 6s( <sup>3</sup> P) <sup>4</sup> P		
3/2	573 301	573 265	36	88%( <sup>1</sup> D <sub>2</sub> )[2]	88%	4p <sup>4</sup> 6s( <sup>1</sup> D) <sup>2</sup> D	9%	4p <sup>4</sup> 6s( <sup>3</sup> P) <sup>2</sup> P	2%	4p <sup>4</sup> 5d( <sup>1</sup> S) <sup>2</sup> D
5/2	574 495	574 483	12	85%( <sup>1</sup> S <sub>0</sub> )[2]	85%	4p <sup>4</sup> 5d( <sup>1</sup> S) <sup>2</sup> D	4%	4p <sup>4</sup> 5d( <sup>3</sup> P) <sup>2</sup> F	3%	4p <sup>4</sup> 5d( <sup>3</sup> P) <sup>4</sup> P
3/2	574 889	574 920	–31	81%( <sup>1</sup> S <sub>0</sub> )[2]	81%	4p <sup>4</sup> 5d( <sup>1</sup> S) <sup>2</sup> D	6%	4p <sup>4</sup> 5d( <sup>3</sup> P) <sup>4</sup> F	4%	4p <sup>4</sup> 5d( <sup>3</sup> P) <sup>2</sup> D
1/2	602 660	602 671	–11	85%( <sup>1</sup> S <sub>0</sub> )[0]	85%	4p <sup>4</sup> 6s( <sup>1</sup> S) <sup>2</sup> S	9%	4p <sup>4</sup> 6s( <sup>3</sup> P) <sup>4</sup> P	5%	4p <sup>4</sup> 6s( <sup>3</sup> P) <sup>2</sup> P

at wavelengths that are long relative to the resonance lines and serve to improve the accuracy of the excited levels. However, as the separation of configurations with different principal quantum number increases with increasing ionization stage, these transitions move to lower wavelength, and their inclusion does not improve the accuracy of the excited levels. For Zr VI, these transitions fall in the same wavelength region as the  $4s^2 4p^5 - 4s^2 4p^4 d$  resonance transitions, so they have practically no effect on the Ritz values for the resonance lines.

## 6. Ritz wavelengths

We determined Ritz wavelengths for a number of the lines by differencing the energy level values in tables 2 and 3. The uncertainties of the calculated wavelengths were taken to correspond to the square root of the sum of the squares of the uncertainties of the combining levels. In table 1 we show the Ritz wavelengths and uncertainties for lines likely to be suitable as wavelength standards, that is where the uncertainty of the Ritz wavelength is  $\pm 0.0020$  Å or less. (This table contains all observed lines together with those with Ritz values.) The Ritz values have uncertainties that vary from  $\pm 0.0003$  Å to  $\pm 0.0020$  Å.

## 7. Oscillator strengths

Table 1 lists the transition probabilities  $g_U A$  and  $\log g_U f$  for each observed line as calculated with wavefunctions obtained from the fitted energy parameters. Here,  $f$  is the oscillator strength,  $g_U$  is the statistical weight of the upper level  $2J_U + 1$  and  $g_L$  is the statistical weight of the lower level  $2J_L + 1$ . The  $A$ -values are compared with recently published *ab initio* values in section 9 below.

Since there are no experimental values for the transition probabilities of Zr VI, it is difficult to estimate the uncertainty

of the calculated values. One guide is the cancellation factor. This is the ratio of the calculated transition probability to a value calculated with all parts of the wave function taken as positive [12]. Low cancellation factors generally indicate a larger uncertainty in the calculated values. Indeed, many of the values in table 1 have low cancellation factors. To try to obtain a more quantitative estimate of the uncertainties, we attempted to judge the sensitivity of the values to the parameter values used for the calculation. For this, an alternate calculation was performed with parameters that varied by small amounts from those used for the main calculation. The differences in the results were then used to put the uncertainties on a semi-quantitative basis with code letters, as are often used for this purpose. The letter codes define categories of uncertainties in  $A$ -values: C ( $\leq 25\%$ ), D + ( $\leq 40\%$ ), D ( $\geq 50\%$ ), E ( $> 50\%$ ).

## 8. Ionization energy

In [4] an estimated value of  $n^*(4p^4 5s)$  of  $3.12 \pm 0.02$  was used to determine an ionization energy of  $773\,000 \pm 5000$  cm<sup>–1</sup>. In [6] this was revised upward to  $776\,500 \pm 500$  cm<sup>–1</sup> on the basis of a Ritz diagram for the  $4p^4 5s$ ,  $6s$ , and  $7s$  configurations. (No details of the determination were given.) Since four of the eight levels of  $4p^4 6s$  in [6] have now been found to be spurious, this value must be re-determined.

For our new determination we use the centers-of-gravity of the  $4p^4 5s$  and  $4p^4 6s$  configurations together with an estimated value for the change in effective quantum number  $\Delta n^*(4p^4 6s - 4p^4 5s) = n^*(4p^4 6s) - n^*(4p^4 5s)$ . This allows us to find the limit of the  $4p^4 ns$  series, which is the center-of-gravity of the  $4p^4$  configuration of Zr VII.

From the observed levels in table 3, we find the centers-of-gravity of the  $4p^4 5s$  and  $4p^4 6s$  configurations as  $383\,198.13$  and  $562\,514.9$  cm<sup>–1</sup>, respectively. Our value for  $\Delta n^*(4p^4 6s - 4p^4 5s)$  is taken from  $\Delta n^*(4p^6 6s - 4p^6 5s)$  for the

**Table 8.** Comparison of wavelengths  $\lambda(\text{\AA})$  and transition probabilities  $A(\text{s}^{-1})$  for Zr VI calculated with the MCDF2 method of Singh *et al* [18] and the GRASP3 method of Aggarwal and Keenan [19] with present values. Numerals following level names are index numbers used in [18] and [19]. Blank spaces indicate that line was not observed. Acc. is the accuracy estimate.

Lower level	Upper level	$\lambda$ [18]	$\lambda$ [19]	$\lambda$ (pres.)	$A$ [18]	$A$ [19]	$A$ (pres.)	ICF1	Acc.	Int.(obs)				
4s <sup>2</sup> 4p <sup>5</sup> <sup>2</sup> P <sub>3/2</sub>	1 4s4p <sup>6</sup> <sup>2</sup> S <sub>1/2</sub>	3	528	494.113	522.000	5.30E + 08	1.0518E + 09	1.31E + 09	0.04	D+	2000			
		4s <sup>2</sup> 4p <sup>4</sup> 4d ( <sup>3</sup> P) <sup>4</sup> D <sub>5/2</sub>	4	410	392.117	401.701	1.17E + 07	2.0308E + 07	9.49E + 06	0.00	E	80		
			6	408	390.213	399.967	7.76E + 06	1.1017E + 07	1.22E + 07	0.00	E	80		
		( <sup>3</sup> P) <sup>4</sup> D <sub>3/2</sub>	7	405	387.245	397.112	4.75E + 06	5.6982E + 06	1.40E + 07	0.01	E	30		
		( <sup>1</sup> D) <sup>2</sup> P <sub>1/2</sub>	10	376	359.833	375.546	1.28E + 07	2.1200E + 08	1.49E + 07	0.00	E	30		
		( <sup>3</sup> P) <sup>4</sup> F <sub>3/2</sub>	12	372	359.150	368.600	3.35E + 05	5.1086E + 05	2.13E + 08	0.01	D+	250		
		( <sup>3</sup> P) <sup>4</sup> F <sub>5/2</sub>	11	374	360.799	368.494	1.41E + 08	1.0789E + 07	2.14E + 08	0.61	D+	300		
		( <sup>3</sup> P) <sup>4</sup> P <sub>1/2</sub>	13	368	353.993	367.523	4.67E + 08	5.9759E + 08	8.61E + 08	0.15	D+	300		
		( <sup>3</sup> P) <sup>4</sup> P <sub>3/2</sub>	14	368	353.991	366.522	5.50E + 08	7.0038E + 08	5.27E + 08	0.02	D+	200		
		( <sup>1</sup> D) <sup>2</sup> D <sub>3/2</sub>	15	365	351.232	364.080	3.37E + 08	2.5390E + 08	3.80E + 08	0.01	D+	300		
		( <sup>3</sup> P) <sup>4</sup> P <sub>5/2</sub>	17	360	346.875	358.755	1.60E + 08	1.5603E + 08	2.85E + 08	0.02	D+	300		
		( <sup>1</sup> D) <sup>2</sup> P <sub>3/2</sub>	18	358	344.980	357.837	6.97E + 07	1.7608E + 07	5.52E + 07	0.00	D+	30		
		( <sup>1</sup> D) <sup>2</sup> D <sub>5/2</sub>	19	354	340.992	353.221	3.82E + 08	2.6359E + 08	4.00E + 08	0.01	D+	250		
		( <sup>3</sup> P) <sup>2</sup> F <sub>5/2</sub>	22	348	335.698	348.262	1.96E + 08	3.0306E + 08	1.56E + 08	0.01	D+	200p		
		( <sup>1</sup> D) <sup>2</sup> F <sub>5/2</sub>	23	330	318.897	333.768	3.24E + 08	3.9608E + 08	4.95E + 08	0.10	D+	400		
		( <sup>1</sup> S) <sup>2</sup> D <sub>3/2</sub>	25	306	304.453	313.150	1.68E + 09	4.0018E + 09	3.18E + 09	0.11	D+	300		
		( <sup>1</sup> S) <sup>2</sup> D <sub>5/2</sub>	26	301	300.149	307.148	3.16E + 02	2.1104E + 09	5.26E + 05	0.00	E	30		
		( <sup>1</sup> D) <sup>2</sup> S <sub>1/2</sub>	28	279	280.532	298.779	1.63E + 11	9.7116E + 10	1.41E + 11	0.71	C	300		
		( <sup>3</sup> P) <sup>2</sup> P <sub>3/2</sub>	27	281	283.619	294.395	1.56E + 11	1.2527E + 11	1.46E + 11	0.90	C	500		
		( <sup>3</sup> P) <sup>2</sup> D <sub>5/2</sub>	30	274	277.998	290.949	1.29E + 10	1.6154E + 11	1.75E + 11	0.85	C	500		
		( <sup>3</sup> P) <sup>2</sup> P <sub>1/2</sub>	29	275	273.019	288.730	1.91E + 11	6.3978E + 10	1.38E + 10	0.11	D+	200		
		( <sup>3</sup> P) <sup>2</sup> D <sub>3/2</sub>	31	265	268.277	279.198	7.17E + 09	7.1045E + 09	4.46E + 09	0.05	D+	90p		
		4s <sup>2</sup> 4p <sup>5</sup> <sup>2</sup> P <sub>1/2</sub>	2 4s4p <sup>6</sup> <sup>2</sup> S <sub>1/2</sub>	3	574	534.239	568.284	2.40E + 08	4.7253E + 08	5.97E + 08	0.05	D+	2000	
				4s <sup>2</sup> 4p <sup>4</sup> 4d ( <sup>3</sup> P) <sup>4</sup> D <sub>3/2</sub>	6	435	414.818		3.21E + 05	1.2890E + 00	2.31E + 06	0.00	E	
					7	431	411.465	423.344	4.55E + 06	4.8266E + 06	9.63E + 06	0.00	E	5
				( <sup>1</sup> D) <sup>2</sup> P <sub>1/2</sub>	10	398	380.653	398.919	6.32E + 07	6.0598E + 07	7.66E + 07	0.00	E	80
				( <sup>3</sup> P) <sup>4</sup> F <sub>3/2</sub>	12	395	379.890	391.094	3.56E + 07	5.1666E + 07	9.18E + 06	0.00	E	100p
				( <sup>3</sup> P) <sup>4</sup> P <sub>1/2</sub>	13	390	374.124	389.881	2.37E + 07	2.6970E + 07	7.14E + 07	-0.01	E	100p
				( <sup>3</sup> P) <sup>4</sup> P <sub>3/2</sub>	14	390	374.122	388.754	1.58E + 07	3.2332E + 06	8.46E + 06	0.00	E	20
				( <sup>1</sup> D) <sup>2</sup> D <sub>3/2</sub>	15	386	371.042	386.007	3.78E + 08	4.0027E + 08	3.88E + 08	-0.01	D+	250
				( <sup>1</sup> D) <sup>2</sup> P <sub>3/2</sub>	18	379	364.072	378.992	2.06E + 07	1.1180E + 07	1.51E + 07	0.00	E	80
( <sup>1</sup> S) <sup>2</sup> D <sub>3/2</sub>	25			321	319.226	329.242	2.20E + 09	6.9689E + 08	3.28E + 09	-0.06	D+	300		
( <sup>1</sup> D) <sup>2</sup> S <sub>1/2</sub>	28			291	293.028	313.389	8.16E + 09	3.9101E + 10	1.27E + 10	-0.11	C	300		
( <sup>3</sup> P) <sup>2</sup> P <sub>3/2</sub>	27			294	296.397	308.569	3.20E + 09	2.5940E + 09	1.16E + 09	0.02	D+	100		
( <sup>3</sup> P) <sup>2</sup> P <sub>1/2</sub>	29			286	284.840	302.351	1.52E + 11	9.6829E + 10	1.28E + 11	-0.87	C	300		
( <sup>3</sup> P) <sup>2</sup> D <sub>3/2</sub>	31			276	279.682	291.920	1.80E + 11	1.5364E + 11	1.65E + 11	0.85	C	500p		

**Table 9.** Comparison of level energies  $E(\text{cm}^{-1})$  for Zr VI calculated with the MCDF2 method of Singh *et al* [18] and the GRASP3 method of Aggarwal and Keenan [19] with present experimental energies. Index numbers are those used in [18] and [19].

Configuration	Term	$J$	Index	$E[18]$	$E[19]$	$E(\text{present})$
$4s^24p^5$	$^2P$	3/2	1	0	0.00	0.00
	$^2P$	1/2	2	15 132.68	15 200.72	15 602.78
$4s4p^6$	$^2S$	1/2	3	189 416.50	202 382.92	191 570.67
$4s^24p^44d$	$(^3P)^4D$	5/2	4	243 856.87	255 025.79	248 940.11
	$(^3P)^4D$	7/2	5	243 977.58	255 226.61	249 322.89 <sup>a</sup>
	$(^3P)^4D$	3/2	6	245 129.81	256 270.21	250 017.63
	$(^3P)^4D$	1/2	7	247 050.21	258 234.49	251 818.7 <sup>a</sup>
	$(^3P)^4F$	9/2	8	257 617.85	268 478.41	261 642.9 <sup>a</sup>
	$(^3P)^4F$	7/2	9	262 852.29	273 655.78	266 145.41
	$(^1D)^2P$	1/2	10	266 287.05	277 906.98	266 278.49
	$(^3P)^4F$	3/2	12	267 351.49	278 434.81	271 296.05
	$(^3P)^4F$	5/2	11	268 547.62	277 162.97	271 374.36
	$(^3P)^4P$	1/2	13	271 422.72	282 491.78	272 091.26
	$(^3P)^4P$	3/2	14	271 795.83	282 492.88	272 834.44
	$(^1D)^2D$	3/2	15	274 341.72	284 711.75	274 665.60
	$(^3P)^2F$	7/2	16	275 087.93	285 754.25	276 491.34 <sup>a</sup>
	$(^3P)^4P$	5/2	17	278 072.77	288 288.07	278 742.23
	$(^1D)^2P$	3/2	18	279 170.13	289 871.57	279 457.21
	$(^1D)^2D$	5/2	19	282 736.58	293 262.43	283 112.00
	$(^1D)^2G$	7/2	20	285 041.05	295 528.49	285 967.09 <sup>a</sup>
	$(^1D)^2G$	9/2	21	285 304.42	295 244.28	286 411.5
	$(^3P)^2F$	5/2	22	287 334.54	297 886.73	287 142.42
	$(^1D)^2F$	5/2	23	303 235.39	313 598.83	299 608.66
	$(^1D)^2F$	7/2	24	306 845.73	317 300.25	303 517.22
	$(^1S)^2D$	3/2	25	327 037.28	328 458.27	319 336.18
	$(^1S)^2D$	5/2	26	332 337.56	333 168.17	325 576.82 <sup>a</sup>
	$(^1D)^2S$	1/2	28	358 608.52	356 465.26	334 694.92
	$(^3P)^2P$	3/2	27	355 733.42	352 586.07	339 682.78
	$(^3P)^2D$	5/2	30	364 819.62	359 714.56	343 709.55
	$(^3P)^2P$	1/2	29	363 414.99	366 274.62	346 345.56
	$(^3P)^2D$	3/2	31	377 428.37	372 749.08	358 168.09

<sup>a</sup> Level energy revised in present work.

one-electron atom Mo VI [16], 1.0338. We use Cowan's Hartree-Fock code to estimate the change in going from Mo VI to Zr VI. For Mo we calculate  $\Delta n^*(4p^66s-4p^55s)$  as 1.0367 and for Zr VI we calculate  $\Delta n^*(4p^46s-4p^45s)$  as 1.0341, a difference of 0.0026. We thus estimate  $\Delta n^*(4p^46s-4p^45s)$  for Zr VI as  $1.0338 - 0.0026 = 1.0312$ , with an estimated uncertainty of  $\pm 0.0015$ . This produces a limit of  $793\,780 \pm 300 \text{ cm}^{-1}$ . The effective quantum numbers for Zr VI are  $n^*(5s) = 3.102(1)$  and  $n^*(6s) = 4.133(3)$ . Correcting for the energy of the center-of-gravity of  $4p^4$  in Zr VII,  $16\,402 \text{ cm}^{-1}$  [15], we obtain for the ionization energy of Zr VI the value  $777\,380 \pm 300 \text{ cm}^{-1}$  ( $96.38 \pm 0.04 \text{ eV}$ ) [17].

## 9. Comparison with *ab initio* calculations

Recently, two sets of *ab initio* calculations for the levels and oscillator strengths of Zr VI have appeared. Singh *et al* [18] used a multiconfiguration Dirac-Fock approach to make calculations for transitions within the  $n = 4$  complex;  $4s^24p^5$ ,  $4s4p^6$ ,  $4s^24p^44d$ . Aggarwal and Keenan [19] used the general-purpose relativistic atomic structure package GRASP for

calculations within the same complex of  $n = 4$  configurations. Both calculations are based on new versions of the Grant atomic structure code, as described in their papers [18, 19]. Froese Fischer [20] has recently discussed the accuracy that might be expected from calculations for complex atoms with GRASP, in particular as applied to the Br-like ion  $W^{39+}$ . Aggarwal and Keenan also used the flexible atomic code [21].

A comparison of the results of the *ab initio* calculations [18, 19] for the wavelengths and transition probabilities with our present values is given in table 8. The wavelengths for Aggarwal and Keenan [19] in this table are differences of the GRASP3 energies in their table 4. Overall, the wavelengths obtained by Singh *et al* [18] are in better agreement with our present observed wavelengths than those of Aggarwal *et al* [19]. A notable disagreement for the transition probabilities is for the  $4s^24p^5 \ ^2P_{3/2} - 4s^24p^44d \ (^3P)^4F_{3/2}$  transition (indices 1–12), observed at  $368.600 \text{ \AA}$ . (The indices are sequential numbers used in [18] and [19] in their enumeration of the energy levels.) Both Singh *et al* [18] and Aggarwal and Keenan [19] find an extremely low transition probability. However, we obtain a fairly high  $A$ -value, and it is indeed

**Table 10.** Comparison of present percentages (in bold type) for the  $4s4p^6$  and  $4s^24p^44d$  configurations with the percentage compositions of Singh *et al* [18] (in parentheses). Level values are in  $\text{cm}^{-1}$ . Index numbers are those used in [18] and [19]. Where there are no values in parentheses, no percentage was given by Singh *et al* [18].

Index	Singh label	$J$	$E(\text{obs})^a$	Percentage composition				
3	$4s^2S$	1/2	191571	<b>77(72)%</b>	$4s^2S$	<b>23(27)%</b>	$(^1D)^2S$	
4	$(^3P)^4D$	5/2	248940	<b>88(90)%</b>	$(^3P)^4D$	<b>3%</b>	$(^3P)^4F$	<b>3%</b> $(^3P)^4P$
5	$(^3P)^4D$	7/2	249323	<b>91(93)%</b>	$(^3P)^4D$	<b>6%</b>	$(^3P)^4F$	<b>2%</b> $(^1D)^2F$
6	$(^3P)^4D$	3/2	250018	<b>86(88)%</b>	$(^3P)^4D$	<b>4%</b>	$(^3P)^4P$	<b>3%</b> $(^1D)^2D$
7	$(^3P)^4D$	1/2	251819	<b>85(89)%</b>	$(^3P)^4D$	<b>7%</b>	$(^1D)^2P$	<b>5%</b> $(^3P)^2P$
8	$(^3P)^4F$	9/2	261643	<b>90(92)%</b>	$(^3P)^4F$	<b>10%</b>	$(^1D)^2G$	
9	$(^3P)^4F$	7/2	266145	<b>66(75)%</b>	$(^3P)^4F$	<b>17%</b>	$(^3P)^2F$	<b>13%</b> $(^1D)^2G$
10	$(^1D)^2P$	1/2	266279	<b>44(44)%</b>	$(^1D)^2P$	<b>37(39)%</b>	$(^3P)^2P$	<b>14%</b> $(^3P)^4D$
12	$(^3P)^4F$	3/2	271296	<b>48(74)%</b>	$(^3P)^4F$	<b>16%</b>	$(^3P)^4P$	<b>13%</b> $(^1S)^2D$
11	$(^3P)^4F$	5/2	271374	<b>93(94)%</b>	$(^3P)^4F$	<b>3%</b>	$(^3P)^4D$	<b>2%</b> $(^1S)^2D$
13	$(^3P)^4P$	1/2	272091	<b>91(91)%</b>	$(^3P)^4P$	<b>5%</b>	$(^3P)^2P$	<b>3%</b> $(^1D)^2P$
14	$(^3P)^4P$	3/2	272834	<b>38(50)%</b>	$(^3P)^4P$	<b>30%</b>	$(^3P)^4F$	<b>18(20)%</b> $(^1D)^2P$
15	$(^1D)^2D$	3/2	274666	<b>36(40)%</b>	$(^1D)^2D$	<b>21(24)%</b>	$(^3P)^2D$	<b>15%</b> $(^3P)^4F$
16	$(^3P)^2F$	7/2	276491	<b>42(50)%</b>	$(^3P)^2F$	<b>25(17)%</b>	$(^3P)^4F$	<b>20(20)%</b> $(^1D)^2G$
17	$(^3P)^4P$	5/2	278742	<b>74(84)%</b>	$(^3P)^4P$	<b>9%</b>	$(^1S)^2D$	<b>7%</b> $(^3P)^2D$
18	$(^3P)^4P$	3/2	279457 <sup>b</sup>	<b>40(24)%</b>	$(^3P)^4P$	<b>24(36)%</b>	$(^1D)^2P$	<b>22(22)%</b> $(^3P)^2P$
19	$(^1D)^2D$	5/2	283112	<b>40(43)%</b>	$(^1D)^2D$	<b>21(23)%</b>	$(^3P)^2D$	<b>18%</b> $(^3P)^4P$
20	$(^1D)^2G$	7/2	285967	<b>65(69)%</b>	$(^1D)^2G$	<b>24(21)%</b>	$(^3P)^2F$	<b>10%</b> $(^1D)^2F$
21	$(^1D)^2G$	9/2	286412	<b>90(92)%</b>	$(^1D)^2G$	<b>10%</b>	$(^3P)^4F$	
22	$(^3P)^2F$	5/2	287142	<b>65(64)%</b>	$(^3P)^2F$	<b>21(19)%</b>	$(^1D)^2F$	<b>9%</b> $(^1D)^2D$
23	$(^1D)^2F$	5/2	299609	<b>77(79)%</b>	$(^1D)^2F$	<b>12%</b>	$(^3P)^2F$	<b>9%</b> $(^1D)^2D$
24	$(^1D)^2F$	7/2	303517	<b>80(81)%</b>	$(^1D)^2F$	<b>16(16)%</b>	$(^3P)^2F$	<b>2%</b> $(^1D)^2G$
25	$(^1S)^2D$	3/2	319336	<b>63(66)%</b>	$(^1S)^2D$	<b>25(25)%</b>	$(^1D)^2D$	<b>5%</b> $(^1D)^2P$
26	$(^1S)^2D$	5/2	325577	<b>73(74)%</b>	$(^1S)^2D$	<b>14%</b>	$(^1D)^2D$	<b>5%</b> $(^3P)^2F$
28	$(^1D)^2S$	1/2	334695	<b>69(42)%</b>	$(^1D)^2S$	<b>20%</b>	$4s^2S$	<b>5(21)%</b> $(^1D)^2P$ <b>4(20)%</b> $(^3P)^2P$
27	$(^3P)^2P$	3/2	339683	<b>50(52)%</b>	$(^3P)^2P$	<b>36(40)%</b>	$(^1D)^2P$	<b>7%</b> $(^1D)^2D$
30	$(^3P)^2D$	5/2	343710	<b>64(66)%</b>	$(^3P)^2D$	<b>21(22)%</b>	$(^1D)^2D$	<b>11%</b> $(^1S)^2D$
29	$(^3P)^2P$	1/2	346346	<b>48(32)%</b>	$(^3P)^2P$	<b>41(27)%</b>	$(^1D)^2P$	<b>7(30)%</b> $(^1D)^2S$
31	$(^3P)^2D$	3/2	358168	<b>57(60)%</b>	$(^3P)^2D$	<b>19(17)%</b>	$(^1S)^2D$	<b>14(17)%</b> $(^1D)^2D$

<sup>a</sup> Present value from table 3.<sup>b</sup> Label for this level in present work is  $4p^44d(^1D)^2P_{3/2}$ .

observed as a fairly strong line. This transition is nominally forbidden as an inter-combination line in LS-coupling because of the change of spin. However, although the  $4p^44d$  level ( $271\,296\text{ cm}^{-1}$  observed value) has a leading percentage composition in LS coupling of 47%  $4p^44d(^3P)^4F_{3/2}$ , the full percentage compositions show that it actually has a total doublet character of about 36%. This accounts for our calculated transition probability and observed line strength. Singh *et al* [18] report a composition of 74%  $4p^44d(^3P)^4F_{3/2}$  for this level, with no secondary percentage mentioned. Percentage compositions were not reported by Aggarwal and Keenan [19].

A number of other striking differences can be seen in table 8. The values found by all three calculations for the  $4s^24p^5^2P_{3/2}-4s^24p^44d(^1S)^4D_{5/2}$  transition (indices 1–26) are extremely discrepant. The present value is about in the middle of the two found with GRASP. The values for the  $4s^24p^5^2P_{1/2}-4s^24p^44d(^3P)^4D_{3/2}$  transition (indices 2–6) also disagree by a large amount. Still, they all predict that this will be a very weak line, and in fact it has not been observed.

Both Singh *et al* [18] and Aggarwal and Keenan [19] compare their calculated level values with the observed values given in the NIST Atomic Spectra Database [22].

Since we have made a number of revisions to the  $4p^44d$  levels, a new comparison is called for. This is given in table 9.

The percentage compositions for the states of the  $4s4p^6$  and  $4s^24p^44d$  configurations obtained in the present work are compared with those obtained in the MCDF calculations of Singh *et al* [18] in table 10. The general agreement is qualitatively reasonable. However, there are some striking differences. For example, as a result of the large  $4s4p^6^2S_{1/2}-4s^24p^44d(^1D)^2S_{1/2}$  interaction mentioned above, we find that the level designated as  $4s4p^6^2S_{1/2}$  (index 3) has an admixture of 23%  $4p^44d(^1D)^2S_{1/2}$ . Singh *et al* [18] find a similar admixture for this level. Correspondingly, we find the level designated as  $4p^44d(^1D)^2S_{1/2}$  (index 28) to have an admixture of 20%  $4s4p^6^2S_{1/2}$ , as would be generally expected. No such admixture is given by Singh *et al* [18]. Presumably, their  $4s4p^6^2S_{1/2}$  percentage calculated for this state is below about 16%, the lowest percentage present in their table 3. Other striking differences can be seen for the levels at  $271\,296$  (index 12),  $272\,834$  (index 14),  $279\,457$  (index 18), and  $346\,346$  (index 29)  $\text{cm}^{-1}$ . Of course, the calculated oscillator strengths depend largely on the admixtures represented by the percentages.

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