### The Properties, Reactivity and Variability of RP-1 and RP-2

MIPR F1SBAA8022G001 MIPR F1SBAA9118G001 MIPR-F4FBEX9205G001

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# First, a bit of history

# **RP-1**:

- Rocket Propellant 1 (refined petroleum 1)
- Kerosene base, used with LOX in rockets such as the Saturn V
- Density 0.81 1.02 g/mL
- Oxidizer to fuel ratio = 2.56
- Temperature of combustion = 3,670 K



# Good old days: <u>Fire it</u>, <u>Forget it</u> Nowadays: <u>Find it</u>, <u>Fix it and Fly it</u>



## Fuel Composition Becomes More Critical:

- Sulfur spec. 500 ppm to 30 ppm to 1 ppm
- Ultimately in the ppb level
  - Required remeasuring all thermophysical properties of RP-1
- The debut of "ultra"
  - A very low S kerosene; became RP-2

### Executive Summary, Project 1: AFRL-MIPR F1SBAA8022G001

- Characterization of a real fuel: RP-1/2

   i.e., chemical analysis, VLE, ρ, μ, λ, ss
- Complete RefProp fluids files for RP-1 and RP-2
- Perform thermal decomposition studies on RP-2:
  - no additives
  - with THQ, tetralin, +100 package



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- Huber, M. L., Lemmon, E., Bruno, T.J., Effect of RP-1 compositional variability on thermophysical properties. *Energy & Fuels* 2009, in press.

### Perform thermal decomposition studies on RP-2:

- no additives
- with THQ, tetralin, +100 package

# Last Year, for the third task,

all I had was a teaser!



# Executive Summary:

AFRL-MIPR F1SBAA8022G001

#### Perform thermal decomposition studies on RP-2:

- no additives
- with THQ, tetralin, +100 package
- All measurements have since been completed, and were presented at:
  - Joint NIST/AFRL Workshop on Rocket Propellants and Hypersonic Vehicle Fuels, September 25 and 26, 2008 at the Boulder, Colorado Laboratories of NIST
  - JANNAF 6th Modeling and Simulation / 4th Liquid Propulsion / 3rd Spacecraft Propulsion Joint Subcommittee Meeting, Orlando, Florida, 8-12 December, 2008.

### Executive Summary, Project 2: AFRL-MIPR F1SBAA9118G001

• Study the additive concentration dependence of thermal decomposition for THQ



### Executive Summary, Project 3: AFRL-MIPR-F4FBEX9205G001

- Evaluate the variability of RP-1:
  - For a set of orthogonal\* samples
    - Measure composition, VLE (ADC),  $\rho,\,\mu,\,ss$
    - Compare with RefProp predictions

\*orthogonal means separate batches or different recipes.



• That's the administrative layout,

technical aspects will be presented in soap opera order.



# **Thermal Decomposition:**

#### **NIST-specific:**

Ensure the quality of property data at high *T*Protect our expensive instruments from decomposition products

Insoluble deposit on a 4 µm wire used to measure the thermal conductivity of RP-1 at 427 °C



#### The kinetics of decomposition are important!

#### **Application:**

- The fuel cools the walls of the thrust chamber
- Avoid engine failure caused by fuel decomposition



# Fuels are thermally stressed in stainless steel ampoule reactors



#### **Reactors:**



#### Maximum T and p:

500 °C / 773 K 15,000 psi / 103 MPa

### **Thermostat**



## **Reaction conditions**

- Initial pressure of 5000 psia (34.5 MPa)
- Temperature range: 375, 400, 425, 450 °C 648, 673, 698, 723 K
- Reaction times from 10 min to 24 h
- Thermal equilibration time of ~2 min

# Extent of decomposition determined by analysis

#### **Emergent suite of GC-FID chromatograms for RP-2**



Light decomposition products are used for the kinetic analysis.

## Pseudo-first-order kinetics on the emergent suite of decomposition products $A \xrightarrow{k'} B$

$$-\frac{d[A]}{dt} = \frac{d[B]}{dt} = k'[A]$$

The assumption of first-order kinetics is a necessary approximation for these complex mixtures.

 $t_{1/2} = \frac{\ln 2}{k'}$ 



The rate constant for decomposition, k', is obtained from the fit.



The rate constant for decomposition, k', is obtained from the fit.



# Rate constants for RP-2 decomposition

<i>T</i> / °C	(k′ ± 1σ) / s <sup>−1</sup>
375	$(1.33 \pm 0.30) \times 10^{-5}$
400	$(9.28 \pm 2.01) \times 10^{-5}$
425	$(1.33 \pm 0.33) \times 10^{-4}$
450	$(5.47 \pm 0.80) \times 10^{-4}$

An Arrhenius plot is useful because it is predictive.



# Decomposition of RP-2 with additives

![](_page_26_Figure_1.jpeg)

RP-2 with 256 ppm of the additive mixture in JP-8+100
 metal deactivator, anti-oxidant, and dispersant

# Decomposition of RP-2 with additives

![](_page_27_Figure_1.jpeg)

5% THQ lowers the rate of decomposition by about an order of magnitude.

![](_page_28_Figure_1.jpeg)

The decomposition of RP-1 and RP-2 is very similar.

#### Comparison of RP-1 and RP-2 decomposition -7 $\diamond$ -8 -9 ln K $\overline{\diamond}$ -10 • RP-1 -11 ♦ RP-2 -12 1.35 1.40 1.45 1.55 1.50 1000/T

There is no significant difference between RP-1 and RP-2.

# High-temperature shock tube data from Stanford

![](_page_30_Figure_1.jpeg)

MacDonald, M. E.; Davidson, D. F.; Hanson, R. K. Decomposition Rate Measurements of RP-1, RP-2, n-Dodecane, and RP-1 with Fuel Stabilizers. 44th AIAA/ASME/SAE/ASEE Joint Propulsion Conference & Exhibit, Hartford, CT, 2008; AIAA Paper 2008-4766.

![](_page_31_Figure_0.jpeg)

MacDonald, M. E.; Davidson, D. F.; Hanson, R. K. Decomposition Rate Measurements of RP-1, RP-2, n-Dodecane, and RP-1 with Fuel Stabilizers. 44th AIAA/ASME/SAE/ASEE Joint Propulsion Conference & Exhibit, Hartford, CT, 2008; AIAA Paper 2008-4766.

Andersen, P.C., Bruno, T.J., Thermal decomposition kinetics of RP-1 rocket propellant. *Ind. Eng. Chem. Res.* 2005, 44, (6), 1670-1676.

![](_page_32_Figure_0.jpeg)

MacDonald, M. E.; Davidson, D. F.; Hanson, R. K. Decomposition Rate Measurements of RP-1, RP-2, n-Dodecane, and RP-1 with Fuel Stabilizers. 44th AIAA/ASME/SAE/ASEE Joint Propulsion Conference & Exhibit, Hartford, CT, 2008; AIAA Paper 2008-4766.

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- Widegren, J. A., Bruno, T.J. The Properties of RP-1 and RP-2, Interim Report, MIPR F1SBAA8022G001; March, 2008.
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### Current Project on Determining the Concentration Dependence of THQ stabilization

# Repeatability of RP-2 decomposition measurements taken 12 months apart

Measurements from last year overlay measurements from this year.

To toot our own horn a bit!

Yeah!

![](_page_35_Figure_3.jpeg)

# Summary of additive effects of THQ as a function of concentration:

![](_page_36_Figure_1.jpeg)

### RP-1, RP-2 Compositional Variability

• The RefProp EOS was based on single "reference" samples of RP-1 and RP-2.

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# So what about variability?

Compositional variability

 Distribution of paraffins, isoparaffins, aromatics, etc.

#### GC-MS

![](_page_40_Figure_1.jpeg)

Approved for public release; distribution unlimited.

**MS Ion Count** 

# So what about variability?

- Compositional variability
  - Distribution of paraffins, isoparaffins, aromatics, etc.
- Property Variability
   VLE, ρ, υ, λ, ss, Cp, Cv, …

- One Manufacturer,
- one set of tight specs,
- many years of experience.

![](_page_43_Picture_0.jpeg)

Treated as if "the sample"

has been passed down from on high

# So, everything is fine, right?

- Questions arise in a Joint USAF, NASA NIST conference:
  - Launch contractors report p variations
    - note that ρ is insensitive
  - Rocket OEMs report kinetic variations in coking

# So, everything is fine, right?

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# Bottom Line: We need to assess the variability of this sacrosanct fluid once and for all!

![](_page_46_Figure_0.jpeg)

**MS Ion Count** 

### If a peak by peak comparison were needed for every sample, rocket scientists would soon become screaming lunatics

![](_page_47_Figure_1.jpeg)

# Can we use any of the thermophysical properties for this?

- Density, ρ (PVT surface), for a kerosene
   write in 0.8 g/mL and you'll be close
- Speed of sound, heat capacities, etc., change by a few %
- viscosity and thermal conductivity change by 4 %
- In contrast, volatility changes appreciably with composition

#### The ADC:

-true thermodynamic state points

–consistent with historical data

-temperature, volume and pressure measurements of low uncertainty

-qualitative, quantitative and trace analysis of fractions

-energy content of each fraction

-corrosivity of each fraction

-greenhouse gas output of each fraction

-thermal and oxidative stability of the fluids

![](_page_49_Figure_9.jpeg)

Apparatus for ADC.

# **Comparison of RP Samples**

- Obtain orthogonal batches of RP-1 and RP-2
- Measure ADC:
  - Initial boiling behavior
  - Full curves
- Examine, and model divergence

- We measure three parameters:
  - Onset
  - Sustained
  - Vapor rise

- We measure three parameters:
  - Onset (first bubbles appear)
  - Sustained
  - Vapor rise

- We measure three parameters:
  - Onset
  - Sustained (bubbles continue w/o stirrer)
  - Vapor rise

- We measure three parameters:
  - Onset
  - Sustained
  - Vapor rise (vapor rises into head)

- We measure three parameters:
  - Onset
  - Sustained
  - Vapor rise (vapor rises into head)
- The vapor rise temperature is the IBT of the fluid, thermodynamically consistent, modeled by EOS.

## Experiments thus far:

- 3 samples of RP-1
  - We think we can find 3-4 more
    - searching AFRL, NASA, engine makers, launch contractors, etc.
- 2 samples of RP-2

The only samples produced as yet

#### Vapor Rise Temperature

![](_page_57_Figure_1.jpeg)

#### **Vapor Rise Temperature**

![](_page_58_Figure_1.jpeg)

![](_page_59_Figure_0.jpeg)

![](_page_60_Figure_0.jpeg)

# **Conclusions:**

- The variability of RP-1 is far more significant than previously thought
  - all measurements and modeling done previously must be questioned.
- The variability of RP-2 is extremely large;
  - Only 2 batches have been made; plant upset?
  - regardless, this is disturbing.

# Acknowledgements:

- AFRL-EAFB – Matt Billingsley
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- Tom Bruno
- Jason Widegren
- Marcia Huber
- Eric Lemmon

# and Students:

- Beverly Smith
- Lisa Ott
- Kari Brumbeck
- Amelia Hadler
- Tara Lovestead

# And, of course, the NIST management team:

![](_page_65_Picture_1.jpeg)

![](_page_66_Picture_0.jpeg)

![](_page_67_Picture_0.jpeg)