

# **Certification of the Relative Molecular Mass and the Intrinsic Viscosity of SRM 2885, a Polyethylene**

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Certain commercial materials and equipment are identified in this paper in order to specify adequately the experimental procedure. In no case does such identification imply recommendation or endorsement by the National Institute of Standards and Technology, nor does it imply necessarily the best available for the purpose.

According to ISO 31-8, the term "Molecular Weight" has been replaced by Relative Molecular Mass, symbol  $M_r$ . Thus, if this nomenclature and notation were followed in this publication, one should write  $M_{r,w}$  instead of the historically conventional  $M_w$  for the weight average molecular weight with similar changes for  $M_n$ ,  $M_z$ , and  $M_v$ .  $M_w$  would be called the "Mass Average Relative Molecular Mass." The conventional notation, rather than the ISO notation, has been used in this publication.

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## ABSTRACT

The certification of a polyethylene standard reference material, SRM 2885, is described. The  $M_w$  of SRM 2885 by light scattering was determined to be  $6.28 \times 10^{+3}$  g/mol with a sample standard deviation of  $0.39 \times 10^{+3}$  g/mol. A combined expanded uncertainty for this light scattering  $M_w$  determination, including systematic and random uncertainties, was estimated to be  $0.56 \times 10^{+3}$  g/mol. The intrinsic viscosity of SRM 2885, by solution viscosity, in 1,2,4-trichlorobenzene was determined to be 22.3 mL/g with a sample standard deviation of 0.17 mL/g. A combined expanded uncertainty for this intrinsic viscosity determination, including systematic and random uncertainties, was 0.20 mL/g. The bottle-to-bottle variation of the SRM was checked by size exclusion chromatography (SEC) and found to be negligible.

## 1.0 Introduction

This report describes the certification of the  $M_w$  by light scattering and intrinsic viscosity (often called the limiting viscosity number [1]) in 1,2,4-trichlorobenzene (TCB) at 130 °C of a linear polyethylene, SRM 2885. The material was obtained from fractionating SRM 1475, as described previously [2]. In the early 1970's, some of this fractionated material was used in the preparation of SRM 1482, SRM 1483, and SRM 1484. Other fractions from the separation had been stored in the Polymers Division in the intervening years. From this material three new narrow mass fraction SRMs are being certified. This reports describes the cleanup, the  $M_w$  by light scattering and the intrinsic viscosity measurements on one of these fractions, a low molecular mass polyethylene. Bottle-to-bottle homogeneity on the final packaged material was determined by size exclusion chromatography (SEC).

## 2.0 Preparation, Bottling, and Handling of SRM 2885

### 2.1 Preparation of the SRM

The  $M_w$  standard, SRM 2885, is a fraction of SRM 1475. The fractionation was described in reference [2]. Fractions of SRM 1475 that had nearly the same SEC trace were combined to obtain enough material for the SRM 2885. The fractions contained both fine powders and larger aggregates and some dirt particles were evident, as well a slight yellowing. It was evident that these fractions needed to be cleaned by recrystallization from solution prior to certification. This process is described in section 2.1.1. Details of the recrystallization procedure and apparatus are given in Appendix I of reference [3].

Subsequent to recrystallization from solution as fine powders the material was sieved together through a sieve with 1.65 mm openings (C E Tyler, Mentor Ohio, 10 meshes to the inch) and then well mixed dry in a stainless steel tray 30 cm x 50 cm. SEC was performed on samples taken from different positions in this tray to confirm the adequacy of mixing. The contents of the tray were sent to NIST Standard Reference Materials Program (SRMP) for packaging.

### 2.2 Packaging and Sampling of SRM 2885

Of the approximately 240 g of purified material approximately 200 g was packaged in about 620 amber vials containing about 0.3 g each. In the following report, the containers holding SRM 2885 will be referred to as vials. The remaining polymer was divided into two lots, designated division 1 supply and division 2 supply. These large lot samples were used to supply some of the material used in the light scattering and intrinsic viscosity measurements. Prior to the use of material from these division supply lots, however, we ascertained that these samples were identical to the material in the vials (See Section 2.3).

The entire set of SRM 2885 vials was divided into 12 subsets of 51 or 52 vials. One vial was randomly selected from each subset of SRM 2885 for homogeneity testing. The first and last bottled vials were also taken. These vials and the two division supply lots were used in the SEC homogeneity testing described below. All these materials were used in the light scattering determinations and intrinsic viscosity determinations described in later sections.

### 2.3 Homogeneity Testing

Homogeneity testing was accomplished using SEC. In this study, a Waters 150-C ALC/GPC Liquid Chromatograph (Waters Corp., Milford, MA) with a differential refractive index (DRI) detector and three Waters styragel columns, HT-6, HT-4, and HT-3, were used. The chromatograms were taken at 0.8 mL/min solvent flow rate. The injector and column compartments of the Waters 150-C ALC/GPC were controlled at 130 °C for all measurements. The solvent, 1,2,4-trichlorobenzene (TCB), was obtained from Aldrich Chemical (1,2,4-trichlorobenzene, 99+ %, spectrophotometric grade, Aldrich Chemical, Milwaukee, WI) and used as received. Santonox (5-*tert*-Butyl-4-hydroxy-2-methylphenyl sulfide), also obtained from Aldrich Chemical, was added to the solvent at about 0.1 g/L as an antioxidant.

Vials of SRM 2885 were obtained from SRMP as described above. Polymer from the two division supply lots was also included in this test. A mass of 4.0 mg to 6.0 mg of the polyethylene was weighed into the 4 mL SEC glass vial with a Teflon septum in the cap assembly along with 4 mL of solvent yielding a concentration of approximately 1.0 g/L. No filtering was done on these samples as the purification done above produced a quite clean sample. Hexadecane, at 0.03 mL/L, was added to the solutions of polymer and solvent as a marker to indicate the reproducibility of the solvent volume delivered by the SEC pump for all measurements. Each SEC glass vial was heated to 150 °C in an oven for about 1.5 h and the solution was shaken at frequent intervals to aid the dissolution. The filter assemblies were placed in the Waters 150-C ALC/GPC injection compartment held at 130 °C. Chromatograms were then run with these solutions.

Solutions were prepared from each vial of SRM 2885 and from each of the division supply lots. Two solutions were prepared from each vial selected from those received from SRMP and four solutions were prepared from each division supply lot. The order used to run the solutions was randomized following the method described in section 1-4 of the handbook by Natrella [4]. Two injections were made from each solution. Because of difficulties with the instrument a few solutions had to be run twice. All chromatographic data were obtained during a five-day period, with 8 solutions measured per day.

After baseline subtraction, the SEC chromatograms were normalized to unit peak height and compared initially by overlaying to determine if there were visible differences outside the noise. We found both the pump peaks and the peak attributed to SRM 2885 shifted slightly over the

period during which we ran the experiment. This indicated variation in the pump during the run. A simple lining up of the pump peak showed that the chromatograms from different solutions of SRM 2885 superimpose fairly well on each other. For further data analysis the elution volume from each chromatograms for the SRM 2885 were shifted by the amount of the pump peak shift. Further statistical analysis of the chromatograms is discussed in section 2.3.1

### 2.3.1 Statistical Method to Compare Chromatograms

#### 2.3.1.1 Match Factor

In previous SEC studies on SRM homogeneity, the match factor was used to compare one chromatogram to all others [5]. The match factor is a correlation coefficient between one chromatogram and another. The match factor is defined by Huber [6] as

$$\text{Match Factor} = 10^3 \frac{\{3x*y-(3x*3y)/p\}^2}{[\{3x^2-3x*3x/p\}\{3y^2-3y*3y/p\}]} \quad (1)$$

The values x and y are the measured signal in the first and second chromatograms, respectively at the same time in the chromatograms; p is the number of data points. The sums are taken over all data points.

At the extremes, a match factor of zero indicates no match and 1000 indicates identical chromatograms. Generally, values above 990 indicate that the chromatograms are similar. Values between 900 and 990 indicate there is some similarity, but the result should be interpreted with care. All values below 900 are thought to mean that the chromatograms are different [6,7]. The method we describe here has been used previously [8]. We obtained the match factor of the entire set of chromatograms, which include two injections for each solution prepared, against the average chromatogram. In the following discussions we will compare chromatograms against the average chromatogram.

An ANOVA study, using OMNITAB [9], was made on the match factors obtained from the chromatograms. It indicated that the match factors for the chromatograms from the same vial were no different than those from different vials on a level of significance with  $\alpha = 0.05$  [10]. Moreover, the match factors of chromatograms from the two division supply lots and the vials were indistinguishable using the same significance level with  $\alpha = 0.05$ . The samples were run in groups of 10 on different days. Using the match factor we found that chromatograms showed no day to day variation. The same statements can be made for the match factor for the pump peaks.

From this we conclude that there is no statistically significant difference between the contents of vials sampled from the SRMP supply of SRM 2885 and no difference between the SRMP supply and the two division supply lots.

### 3.0 Estimation of Impurity Peaks and Polydispersity Index of SRM 2885

SEC measurements described in the Section 2.3 were used to estimate the polydispersity index (PD). We used the solvents as described in Section 2. Columns for this part of the work were two Waters Styragel HT-6E and one Waters Styragel HT-2 (Waters Corp., Milford, MA). The instrument used for this work was a Waters Alliance GPCV 2000 (Waters Corp., Milford, MA), which is equipped with a differential refractive index detector (DRI) and a viscosity detector. Columns were calibrated with SRM 1482, SRM 1483, SRM 1484, SRM 1475, SRM 2885, SRM 2886, and SRM 2887. From the SEC curves for SRM 2885 we estimated the PD ( $PD = M_w/M_n$ ) to be 1.13. No effects of column broadening were taken into account in this measurement, so we expect the value of 1.13 to be an overestimate of the PD.

In a separate calculation, we tried to take the effects of column broadening into account using the Waters Corporation Millennium Software (Waters Corp., Milford, MA) . Using their Axial Dispersion Calculation with peak compression, we found a PD of 1.09.

We should note that while using the viscosity detector of the Waters Alliance system we saw a shoulder on the high molecular mass edge of the SRM 2885 signal. We call this peak the minor component. From the elution volume assigned to the shoulder, we judged the minor component molecular mass to be about  $72 \times 10^3$  g/mol. There is little or no signal from the DRI detector in this range aside from the expected main peak upsweep, which explains why we initially did not see this peak using the older Waters 150-C ALC/GPC, which had only a DRI detector.

From a study of 9 chromatograms of this material, we estimated, using data from the Alliance DRI detector, the area attributable to the minor component. The area attributable to the minor component on the chromatograms gave an estimate of the mass fraction of 0.36% to a mass fraction of 0.61% with an average mass fraction of 0.46%. Thus, we take 0.6 % as the upper limit of the maximum fractional mass in the minor component. The  $M_w$  measured by light scattering will, of course, include the minor fraction.

$$M_{w-LS} = (1-f) M_{w-main} + f M_{w-minor}$$

where  $M_{w-LS}$  is the mass averaged molecular mass from light scattering,  $M_{w-main}$  is the mass averaged molecular mass of the main SRM 2885 peak,  $M_{w-minor}$  is the mass averaged molecular mass of the minor component, taken to be  $72 \times 10^3$  g/mol, and  $f$  is the mass fraction of signal in the minor component. We can then estimate the main peak  $M_{w-main}$  as

$$M_{w-main} = (M_{w-LS} - f M_{w-minor})/(1-f)$$

Using our estimate of  $M_{w-minor}$  and  $f$  we calculate the value of

$$M_{w-main} = 5880 \text{ g/mol.}$$

The maximum error in taking the measured light scattering mass average molecular mass,  $M_{w-LS}$ , as the estimation of the  $M_{w-main}$  is 400 g/mol, less than our estimated overall uncertainty in the

light scattering mass average molecular mass,  $M_{w-LS}$ .

## 4.0 Intrinsic Viscosity of SRM 2885

### 4.1 Measurement of the Intrinsic Viscosity

Viscosity measurements were made with a Schott-Gerate Ubbelohde micro-viscometer (Schott-Gerate GMBH, Hofheim, Germany) with a Schott-Gerate constant temperature bath held at 130 °C. Flow times were measured by the Schott-Gerate AVS 400. The solvent, 1,2,4-trichlorobenzene (TCB), was obtained from Aldrich Chemical (1,2,4-trichlorobenzene, 99+ %, spectrophotometric grade, Aldrich Chemical, Milwaukee, WI) and used as received. Butylated hydroxytoluene (2,6-Di-*tert*-butyl-4-methylphenol), also obtained from Aldrich Chemical, was added to the solvent at about 0.7 g/L as an antioxidant.

Solution concentrations ranging from 0.2 g/L to 2 g/L were prepared from independent weighing of polymer and solvent, rather than employing successive dilution techniques. Concentrations were calculated from densities and partial specific volumes determined earlier in this laboratory [11].

The polymer was dissolved by heating the mixture to 135 °C to 140 °C in a hot air oven with occasional stirring. Solutions were then transferred to a viscometer by filtering the solution through a syringe and syringe filter heated in the same oven. The syringe filter assembly used was a Swinny Stainless 25 mm (Millipore Corp., Bedford, MA) while the filter membrane was a Pall-Gelman Sciences ZEFLOUR all Teflon 0.5  $\mu\text{m}$  pore size 25 mm diameter membrane (Pall Corp., Port Washington, NY).

For each polymer concentration, flow times were measured for both solvent and solutions. The AVS 400 is designed to perform a number of preconditioning runs to insure that the solution or solvent comes to temperature equilibrium before the actual measurements were made and recorded. The operation of the AVS 400 took about 2 min to 2.5 min for each of the five preconditioning runs. Five flow times were measured on each aliquot of the solvent or the solution. Flow times measured in this viscometer ranged from 40 s to 60 s.

At the beginning of an overall measurement on a solution, the viscometer was flushed with at least three solvent aliquots. Then, at least two aliquots of solvent were introduced for flow time measurements. Three aliquots of solution were used to flush the viscometer. Three aliquots of solution were then measured. Three aliquots of solvent were used to flush the viscometer. Finally, flow time measurements were made on three aliquots of solvent.

### 4.2 Results of Solution Viscosity

The solution viscosity,  $\eta(c)$ , may be expanded as a power series in solution concentration,  $c$ ,

[12]

$$\eta(c) = \eta(0) (1 + a_1 c + a_2 c^2 + \dots) \quad (2)$$

where  $\eta(0)$  is the solvent viscosity.

The viscosity is defined as

$$(\eta(c) - \eta(0)) / (\eta(0) c) = a_1 + a_2 c \quad (3)$$

The intrinsic viscosity,  $[\eta] = a_1$ , is the zero concentration limit of the viscosity.

For a properly designed capillary viscometer, the solution viscosity is almost proportional to the product of the solution density,  $\rho(c)$ , and the measured flow time,  $t(c)$ . The deviation from proportionality is due to a combination of kinetic energy effects and hydrodynamic effects at the end of the capillary. The manufacturer of the viscometer gives tables to correct the measured times for each viscometer. These corrections, designated by the manufacturer as the Hagenbach correction [13], are approximately of the form  $1/t_m^2$ , where  $t_m$  is the measured time. The manufacturer's corrections were fitted to this form to interpolate their correction data. This correction is applied to each average flow time for solvent or solution yielding  $t(c)$  where the  $c$  refers to the concentration of the solution being measured.

From eq. 2 then

$$K \rho(c)t(c) = K \rho(0)t(0)(1 + a_1 c + a_2 c^2 + \dots) \quad (4)$$

where the solvent viscosity is

$$\eta(0) = K \rho(0)t(0) \quad (5)$$

and where  $K$  is the viscometer constant.

Finally, we do not need to know  $K$  since the quantity of interest is the limiting value of

$$[\eta] = (\eta(c) - \eta(0)) / (\eta(0) c) = a_1 \quad (6)$$

Thus, we may rewrite eq. 4 as

$$\rho(c) t(c) = \rho(0)t(0) (1 + a_1 c + a_2 c^2 + \dots) \quad (7)$$

On any given day measurements on only one concentration and related solvents as described



above were practical. As viscometers became dirty, they were taken out of service and similar, but not identical, clean ones used in their place. Thus, the ratio,  $T(c)$ , is expected to be invariant at any concentration where  $T(c)$  is

$$T(c) = (\rho(c)t(c) - \rho(0)t(0))/(\rho(0)t(0)) \quad (8)$$

Following the normal definition of  $[\eta]$  as the zero concentration limit of  $T(c)/c$ , we fit  $T(c)/c$  to the expression

$$T(c)/c = a_1 + a_2 c. \quad (9)$$

The value of  $a_1$  so obtained was 22.3 mL/g with a standard deviation of 0.17 mL/g. For our study of uncertainty, we consider the value of the standard deviation reported above to be the expanded uncertainty in the repeatability of the measurement. This is reported in Table 1 with other contributions to the reported uncertainty of this measurement.

Earlier, Wagner and Verdier [12] studied other fractions of the same base material, SRM 1475, certified as SRM 1482, SRM 1483 and SRM 1484. They measured and reported intrinsic viscosities in TCB on these materials. Fitting their data for the intrinsic viscosities,  $[\eta]$ , of SRM 1482, SRM 1483 and SRM 1484, we obtain

$$\ln_e \{ [\eta]_w \} = 0.7312 \ln_e \{ M_w \} - 3.247 \quad (11)$$

where  $[\eta]_w$  is their measured intrinsic viscosity.

Using the  $M_w$  of our polymer obtained in Section 5, we estimate a extrapolated value of  $[\eta]_w$  from eq. 11 for SRM 2885 of 23.3 mL/g, in good agreement with our measured value.

#### 4.3 Estimating Uncertainties in the Intrinsic Viscosity Measurement

The likely sources of uncertainty are discussed in the following subsections and the table referred to herein. For this analysis, we largely follow the paper of Wagner and Verdier [12].

##### 4.3.1 Shear Rate Dependence of Viscosity

Low molecular mass polymers in dilute solution are expected to show little, or no shear rate dependence. Wagner and Verdier [2] were unable to detect shear rate dependence, even for SRM 1484, a linear polyethylene with an  $M_w$  of 114,000 g/mol. The capillary in their viscometer had a smaller diameter than that in the Schotte-Gerate viscometer we are using. Thus, we expect no shear rate dependence of the intrinsic viscosity of SRM 2885, which has a lower mass average molecular mass than SRM 1484. We assume the uncertainty introduced in the intrinsic viscosity

by disregarding this contribution is zero.

#### 4.3.2 Solution Concentration and Density

According to Wagner and Verdier [12], their reported value of  $\rho(0)$  has an estimated relative expanded uncertainty of 0.2 % . We used their values  $\rho(0)$  in our calculations. The solvent density uncertainty leads to 0.05 mL/g expanded uncertainty in intrinsic viscosity. Wagner and Verdier [12] estimated a relative uncertainty 0.03 % in intrinsic viscosity due to the disregard of the buoyancy correction. Since we corrected for buoyancy, we take this uncertainty to be less than 0.01 %, or negligible.

All solutions but one were prepared so that at least 100 mg SRM 2885 was used. For the remaining solution 100 mg of SRM 2885 was used. We estimated that the balance used for this measurement had an expanded uncertainty of less than 0.1 mg. For those solutions where at least 100 mg was used, we estimate a 0.1 mg expanded uncertainty due to weighing would lead to an expanded uncertainty of 0.003 mL/g, which is negligible.

Solvent masses were measured with an expanded uncertainty of 0.01 g. A minimum of 30 g of solvent was used. This uncertainty had negligible effect on the results and so was taken to be zero.

#### 4.3.3 Specific Volume of the Polymer

The intrinsic viscosity,  $[\eta]$ , is the limit of

$$[\eta] = \lim_{c \rightarrow 0} \{(\rho(c)t(c) - \rho(0)t(0))/(\rho(0)t(0)c)\} \quad (12)$$

where  $\lim_{c \rightarrow 0} \{ \}$  is taken to mean the limit at zero concentration. Following Wagner and Verdier [12] using the fact that the limit of the product is the product of the limit, they find

$$[\eta] = \rho(0)^{-1}(1+2K'/t_m(0)^{+3})/(1-K'/t_m(0)^{+3}) * \lim_{c \rightarrow 0} \{(t_m(c)-t_m(0))/(t_m(0)w)\} + \rho(0)^{-1} - v_{avg} \quad (13)$$

where  $w$  is the mass fraction of solute in the solution and  $K'$  is the kinetic energy term derived from corrections given by the viscometer manufacturer [13].

This formula corrects a typographical error in their formula 11. The formula shows that the intrinsic viscosity as made up of two terms if we disregard the kinetic energy (KE) corrections of the viscometer. Assuming these KE corrections are zero we get then

$$[\eta] = \rho(0)^{-1} \mathbf{L} \{ (t_m(c) - t_m(0)) / (t_m(0)w) \} + \rho(0)^{-1} - v_{\text{avg}} \quad (14)$$

The last two terms are the difference between the specific volume of the solvent,  $\rho(0)^{-1}$ , and the specific volume of the polymer in solution,  $v_{\text{avg}}$ . This difference is small, about a few tenths of an mL/g, compared to an overall intrinsic viscosity of about 22.4 mL/g for this polymer. Since  $v_{\text{avg}}$  was determined on other fractions of this polymer previously [11,12], we estimate that our value of  $v_{\text{avg}}$  has an uncertainty of no more than 0.04 mL/g. Thus, we take 0.04 mL/g to be the expanded uncertainty in intrinsic viscosity from this contribution.

#### 4.3.4 Timer Uncertainties

Individual flow times were recorded to 0.01 s. We take this to be the expanded uncertainty of the timer measurements. Since the intrinsic viscosity is the ratio of the time differences over a time, only the uncertainty in the time in the denominator is important. Since total flow times were between 40 s and 60 s, a 0.01 s timer uncertainty would cause an expanded uncertainty of no more than 0.01 mL/g.

#### 4.3.5 Kinetic Energy or Hagenbach Corrections

As noted above, kinetic energy, or Hagenbach, corrections were estimated from tables given by the viscometer manufacturer [13] and obey a  $G/t(c)^2$  law. The value of  $G$  estimated from the manufacturer's table is  $412 \text{ s}^3$  for our viscometer. We take our value of  $G$  to have a relative expanded uncertainty of 20 %, twice that assumed by Wagner and Verdier [12] for their value of  $G$ . This leads to an expanded uncertainty of 0.07 mL/g in the intrinsic viscosity of SRM 2885.

If we do not consider kinetic energy corrections to the measured data, we compute the apparent intrinsic viscosity different from the measured intrinsic viscosity of 0.33 mL/g. If we take 20 % of this difference as a measure of the uncertainty, this result is consistent with the expanded uncertainty estimated above.

#### 4.3.6 Uncertainties Arising from Temperature Uncertainties

Wagner and Verdier [12] estimate the relative temperature dependence of the intrinsic viscosity of polyethylene to be no more than 0.2 % / °C for polyethylene in theta solvents. The temperature dependence is expected to be less in TCB, which is a good solvent for polyethylene. Following Wagner and Verdier, we take 1 % / °C as the outside limit of the temperature dependence of intrinsic viscosity. We believe the Schott-Gerate constant temperature bath controls the temperature much better than 0.3 °C, including effects of temperature gradients. This conclusion arises partly because we have a reproducibility of better than 0.10 s out of about 41 s for the

solvent flow times taken over a period of weeks. Further, we found a 1 °C change in temperature altered the measured flow time of the solvent by 0.32 s. Thus, we take 0.07 mL/g as the expanded uncertainty from the temperature.

#### 4.3.7 Estimated Combined Expanded Uncertainty

In Table 1, the estimated expanded uncertainties from all sources are listed. Following NIST guidelines [15] we obtain the combined expanded uncertainties as the root sum of squares of these quantities.

### 5.0 Determination of $M_w$ of SRM 2885 by Light Scattering

#### 5.1 Solvent Preparation for Light Scattering and for Specific Refractive Index Increment

The light scattering solvent, 1-chloronaphthalene, was purchased from Aldrich Chemical (Aldrich Chemical, Milwaukee, WI). According to the supplier, this 1-chloronaphthalene was 90 % pure with 2-chloronaphthalene as the only detectable impurity. A two-step purification method described in Appendix II of reference [3], involved crystallizing out the 2-chloronaphthalene followed by vacuum distillation of the 1-chloronaphthalene.

The antioxidant Santonox, 3-*tert*-Butyl-4-hydroxy-2-methylphenyl sulfide (Aldrich Chemical, Milwaukee, WI), was added to the purified 1-chloronaphthalene in order to protect the polyethylene from oxidative degradation during the high temperature light scattering experiments and differential refractive index determinations. The antioxidant was dissolved in the 1-chloronaphthalene at a concentration of 0.1 g/L at 130°C.

The 1-chloronaphthalene was sparged with dry nitrogen gas for a few hours immediately before adding solvent to polymer samples in preparing solutions to conduct experiments. The nitrogen sparging was used to minimize residual oxygen content in the solvent.

Solvent recovered from light scattering experiments was recycled. After the solutions had been allowed to cool and the polymer had separated out, the recovered material was drained through a filter. The collected solvent was redistilled by the process described in Appendix II of reference [3]. Since the 2-chloronaphthalene impurity had already been removed exhaustively from such recovered solvent earlier, the preparatory refluxing process to remove the isomer was omitted.

#### 5.2 Determination of Specific Refractive Index Increment

##### 5.2.1 Instrumentation

The specific refractive index increment ( $dn/dc$ ) for SRM 2885 was determined using a

Chromatix KMX-16 (Thermo-Separation Products, Sunnyvale, CA) differential refractometer. The refractometer light source was a helium-neon (He-Ne) laser operating at a wavelength of 632.8 nm. For room temperature calibration, the measurement cell was controlled at 25 °C. The measurement cell was heated to 130 °C for the solution and solvent measurements.

### 5.2.2 Calibration of Instrument at Room Temperature

The differential refractometer was calibrated with aqueous NaCl solutions at 25 °C. Krus [16] reported refractive increments versus concentration for several aqueous electrolyte solutions at several wavelengths of light. Refractive increments for the same solutions at the He-Ne laser wavelength, 632.8 nm, have been determined from interpolation of the data in the Krus' tables [16,17]. A cubic equation for these refractive increments as a function of NaCl concentration in aqueous solution at 25 °C is given in the instrument manual, and was used to compute the refractive increments of the aqueous NaCl solutions prepared as standards for calibrating the differential refractometer.

Analytical reagent NaCl (Baker and Adamson, Allied Chemical and Dye Corp, New York, NY) was dried in a hot air oven for approximately 18 h at a temperature of 140 °C in preparation to be used as a calibrant. Distilled water was degassed by boiling and left to cool to ambient temperature overnight in storage bottles tightly capped with zero headspace. The storage bottles had been leached out with several changes of boiling distilled water before being used to contain the degassed distilled water. Both salt and water components of each solution were measured gravimetrically, and atmospheric buoyancy corrections were applied to compute the concentrations as g NaCl/100 g H<sub>2</sub>O.

Following instructions in the instrument instruction manual [17] calibration measurements for the differential refractometer were conducted on four NaCl solutions ranging in concentration from 0.5 g NaCl/100 g H<sub>2</sub>O to 2.0 g NaCl/100 g H<sub>2</sub>O in intervals of 0.5 g NaCl/100 g H<sub>2</sub>O. The calculated refractive increments of the solutions were fitted to their average image displacements to generate a linear calibration equation of refractive increment versus image displacement,  $dn/dc$ . The instrument calibration was found to be insignificantly changed from calibrations made years earlier indicating that we were simply verifying an earlier calibration. In fact, the plot of the calibration verification points, when overlaid on an earlier instrument calibration plot, produced a graph in which the two data sets were indistinguishable.

### 5.2.3 Solution Preparation and Handling

Polymer solutions were prepared using 1-chloronaphthalene solvents with a mass fraction of 0.01% Santonox (Aldrich, Milwaukee, WI) antioxidant. The 1-chloronaphthalene (Aldrich, Milwaukee, WI) was purified by distillation before use as described in Appendix II of reference [3]. Solution concentrations in ranges described in section 5.2.4 were made directly by weighing, without employing successive dilution techniques. Concentrations were calculated from densities

and partial specific volumes determined earlier in this laboratory [11]. A general-purpose laboratory convection oven set at a temperature of approximately 145 °C was used to dissolve the polymer solutions. Glass bottles with ground glass necks and caps were used as dissolution vessels for the polymer samples. Experiments conducted earlier (private communication, R.C. Christensen) demonstrated that solvent loss at 130 °C through the ground glass joint was negligible.

Transfer of the polymer solutions from the glass dissolution vessels into the refractometer measurement cell was accomplished with a specially constructed glass funnel/valve assembly heated to approximately 145 °C. A 6.8 cm diameter Pyrex glass powder funnel was modified by having the barrel of a 5 mL glass luer lock syringe attached to the funnel stem. An on-off valve (Popper & Sons, Inc., New Hyde Park, NY) was attached to the luer fitting and a shortened 20-gage needle attached to the valve. The funnel was placed in a heating mantle (Glas-Col, Terre Haute, IN) and a flexible electric heating tape (Barnstead/Thermolyne, Dubuque, IA) was wrapped around the stem, valve and needle that protruded below the heating mantle. The funnel assembly was supported by a three-jaw clamp attached to the funnel stem and an adjustable height rack and pinion post (Edmund Industrial Optics, Barrington, NJ). The rack and pinion post was lowered to position the needle in the sample cell for filling the cell with polymer solution and raised above the cell to provide access to the cell by suction tubing, which was used to empty the cell. Heating mantle and heat tape temperature were measured with a digital thermocouple thermometer (John Fluke Mfg. Co., Palatine, IL) and adjusted by Variac autotransformers (General Radio Co., Cambridge, MA). Dissolved polymer solutions were removed from the oven and poured from the dissolution bottle into the heated funnel. Using the on-off valve on the funnel stem, the refractometer measurement cell was filled with hot polymer solution. Following the instrument instruction manual [18], the cell was filled and emptied five times before measurements were made on the solution.

#### 5.2.4 Measurement of $(dn/dc)$ at 130 °C

Refractive index increments between solvent and solutions of polyethylene in 1-chloronaphthalene were determined on solutions that had been prepared on the morning of the day the measurements were made. Five solutions with concentrations between 3.5 g/L to 7.2 g/L of SRM 2885 were prepared by the procedure describe in Section 5.2.2. For each solution two repeated image displacement measurements were conducted on these solutions of SRM 2885 following methods as outlined in KMX 16 manual. Solvent-versus-solvent measurements were made before and after each solution-versus-solvent measurement. The incremental image displacement by each solution was obtained by subtracting the mean of the bracketing solvent average image displacements from the average image displacement by the solution. The refractive index increment of each solution was computed by application of the calibration equation to the incremental image displacement of the solution. The specific refractive index increments were obtained by dividing the refractive index by the concentration of the solution. The average value of the specific refractive index increment of the solutions was found to be,  $dn/dc = -0.1867$  mL/g, for SRM 2885 in 1-chloronaphthalene at 130 °C with a standard deviation

of 0.0014 mL/g. The issues of uncertainty and fit of this measurement will be discussed in section 5.10.3.

Previous reports of the differential refractive index at 632.8 nm for other comparable polyethylenes in 1-chloronaphthalene gave values ranging from -0.178 mL/g to -0.183 mL/g at 135 °C [19-21]. Our value is slightly outside the range of these reported values. The molecular mass of the polymer is about 6000. This is in the range we expect end groups to contribute to  $dn/dc$  [19]. Earlier measurements on  $dn/dc$  at a wavelength of light of 546 nm on PE solutions in TCB and 1-chloronaphthalene showed the  $dn/dc$  getting more negative as the molecular mass decreases, consistent with our results [20, 21, 25].

### 5.3 Refractive Indices of Solvent and Calibrant

The primary standard for this measurement is benzene; other standards are derived from it. The refractive index of the benzene primary standard at 23 °C and 632.8 nm is taken to be 1.4941[12].

G. B. Arrowsmith, G. H. Jeffrey, and A. I. Vogel [24] tabulated the refractive index at the Sodium D line  $n_D=1.63315$  at 20 °C and a density at 20 °C of 1.1932 g/mL for 1-chloronaphthalene. Christensen [11] reports the density of 1-chloronaphthalene as 1.098 g/cm<sup>3</sup> at 130 °C and Wagner [25] reports the density of 1-chloronaphthalene as 1.098 g/cm<sup>3</sup> at 135 °C. The Lorentz-Lorenz molar refraction relation is used to estimate the refractive index for 1-chloronaphthalene at 130 °C from the densities at 20 °C and 130 °C and the refractive index at 20 °C. Since the refractive index of 1-chloronaphthalene at 130 °C,  $n_D=1.5772$ , is only used in the reflection correction to the  $M_w$  the limited accuracy of this value is acceptable.

Dow Corning 705 silicone oil is used as the vat fluid. The Lorentz-Lorenz molar refraction relation was applied to the refractive index at 632.8 nm at 25 °C, and the density at various temperatures (Dow technical consultant Gary McIntyre) to estimate the refractive index of the Dow Corning 705 silicone oil at 130 °C as  $n_D = 1.516$ . Since the refractive index of Dow Corning 705 silicone oil 130 °C is only used in the reflection correction to the  $M_w$  the limited accuracy of this value is acceptable.

### 5.4 Design of Light Scattering Instrument

Dr. Charles Han of the NIST Polymers Division designed and constructed the light scattering apparatus. We review here some of the details of the instrument. A Universal circular dividing table (Universal Vise & Tool Co.), with a center bore design, is used as the goniometer. This goniometer is mounted on a rigid optical table (Newport Research Corporation). A beam of vertically polarized incident light (wavelength = 632.8 nm) is provided by a 10 mW He-Ne laser (Melles-Griot) also mounted.

The goniometric axis is defined by the center of the goniometer and aligned with a tapered center

bore in the goniometer. The vat housing, which contains the sample cell, is mounted on an aligning rod with a precision-machined taper to engage the complementary taper of the center bore of the goniometer. The receptacle hole for the sample cell is machined at the cylindrical axis in the top flange plate of the vat housing. By this arrangement the center axis of the cylindrical cell and the vat housing are held coincident with the goniometric axis. The intensity of light scattered at varied angles from the sample cell is measured by a photomultiplier in the receiving optics mounted on a rigid beam attached to the goniometer.

The vat is thermostatted by a copper cylinder, which is built onto the underside of the vat housing cover plate, and extends down into the vat fluid. The vat temperature is controlled and indicated by a PID temperature controlling system, a copper constant current supplier, a four wire RTD and a voltage comparator. The controlling system receives a voltage imbalance signal from a four-wired platinum resistance temperature probe in the thermostating cylinder and the voltage comparator, and sends energy to cartridge heaters in the thermostating cylinder. When working at high temperatures, significant thermal gradients can develop inside the vat between the thermostating cylinder and the peripheral region of the vat. Such thermal gradients were repressed by applying a flexible heating mantle to the external cylindrical surface of the vat housing, and controlling the mantle temperature at a few degrees Celsius below the experimental temperature. The mantle was specially constructed for this apparatus, and the control provided by HPS Division, MKS Instrument, Inc. (MKS Instrument, Inc, 5330 Sterling Drive, Boulder, CO 80301).

Light scattering cells were fabricated from precision ground and polished glass tubing to uniform wall thickness (Wilmad Glass Co.), with both inside and outside cylindrical surfaces polished. The tubing is of 33 mm outside diameter and has a refractive index  $n_D = 1.50$ .

### 5.5 Instrument Calibration Protocol at 130°C

1,2,4-trichlorobenzene (TCB) (Aldrich Chemical high purity, Milwaukee, WI) was employed as the working light scattering calibration standard at 130 °C. The calibration of TCB as the working standard is traced to the Rayleigh ratio ( $R_V$ ) of benzene at ambient temperature (23 °C) in vertically polarized incident light of 632.8 nm wavelength, determined by Kaye & McDaniel [26].

First, a Durasil optical glass rod was calibrated by comparing its scattering intensity at a 90° angle with that of a benzene cell at the same angle, with the glass rod and benzene cell both at 21 °C. Then the vat temperature was increased to 130 °C in which environment three TCB cells were calibrated by comparison of their scattering intensities with that of the glass rod. The effective  $R_V$  of the glass rod is assumed to be invariant with temperature in this range. However, relating the scattering intensity measurements at the two temperatures requires conservation of the optical alignment with change in temperature. The only significant disturbance in the optical alignment results from the change in refractive index of the vat fluid with change in temperature. This problem was solved by conducting the measurements at 21°C with the vat filled with anisole



which has  $n_D = 1.5160$  at  $20\text{ }^\circ\text{C}$ , and conducting the measurements at  $130\text{ }^\circ\text{C}$  with the vat filled with Dow Corning 705 silicone oil which has  $n_D = 1.516$  at that temperature.

The scattering intensities at  $90^\circ$  angle ( $I_{90}$ ) of the benzene standard cell and the glass rod standard were measured alternately at  $21^\circ\text{C}$ . A total of 40 such pairs of measurements were conducted over an interval of two days. The resulting population of experimentally determined scattering intensity ratios yielded an average  $[I_{90}(\text{GLASS})/I_{90}(\text{BENZENE})]$  with a relative standard uncertainty of 1.16 %.

A series of TCB standard cells was prepared by filtering high purity TCB into each cell through a double layer of Millipore cellulose acetate-nitrate membrane with  $0.2\ \mu\text{m}$  pore size. Filtration of TCB into the cells was conducted at ambient temperature. It was found that a TCB sample could be maintained at the experimental temperature ( $130\text{ }^\circ\text{C}$ ) and slightly higher for at least two days without detectable change. A new TCB standard cell was prepared for use with each set of solutions during the characterization of this polymer by light scattering. The  $I_{90}$  of the glass rod standard was compared with the  $I_{90}$  of each of three TCB cells at  $130\text{ }^\circ\text{C}$ . The  $I_{90}$  values of the glass rod and the TCB cell were measured alternately. A total of 14 pairs of such  $I_{90}$  measurements were conducted with the glass rod and each of the TCB cells, resulting in three average values for the ratio  $[I_{90}(\text{TCB})/I_{90}(\text{GLASS})]$  in very close agreement. The three determinations resulted in a single average value for the ratio with a relative standard uncertainty of 0.2 %.

As small error was introduced because we measured the ratio of scattering from benzene to the glass cell,  $S$ , at  $21\text{ }^\circ\text{C}$ , not at  $23\text{ }^\circ\text{C}$  where the  $R_V$  was measured by Kaye and McDaniel [26]. Ehl, Loucheux, Reiss, and Beniot [27] have measured this temperature variation. Our measurements of  $S$  give us  $S_{21}$ , the  $S$  at  $21\text{ }^\circ\text{C}$ . We need  $S_{23}$ , the ratio measured with benzene and the glass rod at  $23\text{ }^\circ\text{C}$ . From Ehl, Loucheux, Reiss and Beniot [27] we estimate

$$S_{23} = 0.9946 S_{21}$$

As noted earlier, Kaye and McDaniel [26] determined the value  $R_V = 12.63 \times 10^{-6}$  for benzene under these optical conditions, with a standard uncertainty of  $0.21 \times 10^{-6}$ . The product of ratios,  $[I_{90}(\text{GLASS})/I_{90}(\text{BENZENE})]$  and  $[I_{90}(\text{TCB})/I_{90}(\text{GLASS})]$  gave a value of  $S_{21}$ . This was applied to the  $R_V$  for benzene by Kaye and McDaniel to estimated working value of  $R_V = 35.6 \times 10^{-6}$  for the TCB at  $130^\circ\text{C}$  in vertically polarized incident light of  $632.8\text{ nm}$  wavelength. The standard uncertainty for this value of  $S_{21}$  is computed as the root sum of squares of the standard uncertainties of the two ratios.

The molecular mass ( $M_w$ ) of the polyethylene standard SRM 1483 was determined to test this method of calibration using TCB as the working standard in light scattering experiments. The resulting  $M_w$  from these experiments conducted with TCB as the calibrating standard were statistically indistinguishable from the certificate value of the  $M_w$  for SRM 1483 [2].

## 5.6 Solution Preparation

SRM 2885 samples from the SRMP vials were weighed on an OHAUS GA200D analytical electrobalance (Ohaus Corp., Florham Park, NJ), with 0.0001 g resolution, and transferred to sample bottles. All polymer samples weighed 30 mg or greater in order to repress relative uncertainty in the sample mass. The 1-chloronaphthalene was sparged for 2 h with dry N<sub>2</sub> gas. The sparged solvent was then measured into bottles containing the polymer samples, plus two empty bottles to contain solvent samples. The solvent mass was determined by mass difference on a Mettler PE 3600 electrobalance (Mettler Toledo, Columbus, OH). Atmospheric buoyancy corrections and densities of solvent and polymer were applied to calculate absolute solution concentrations at the experimental temperature. Both balances were checked during the certification period often by a NIST calibrated 50 mg mass for the Ohaus balance and a NIST calibrated 50 g mass for the Mettler. The balances read with accuracy to the last reading value.

Solution concentrations in range described in Section 5.9 were made directly by weighing, without employing successive dilution techniques. Concentrations were calculated from densities and partial specific volumes determined earlier in this laboratory [11]. The bottles were capped with ground glass tops and placed in an oven at about 150 °C. They were heated and agitated occasionally for about 2 h before commencing filtration.

The syringe filter assembly used was a 25 mm diameter stainless steel Swinny type (Millipore Corp., Bedford, MA). The Swinny filter was attached to a glass syringe modified by adding a spherical joint at the top end, to provide connection to a dry nitrogen source used to apply an inert low-pressure gas to propel solution through the filter at a realistic rate. Each Swinny was assembled with a double layer of Pall-Gelman Sciences ZEFLUOR all-Teflon filtering membrane with 0.5 μm pore size (Pall Corp., Port Washington, NY). These filtering assemblies were heated to 150 °C in the oven along with the solvent and solution bottles.

After the polymer samples had dissolved to form clear homogeneous solutions, the solvent and solution samples were filtered into their respective light scattering cells.

The hot filtration was conducted in a thermostatted apparatus that maintained both cell and filtering assembly in the range 140°C to 150°C. The filtering assembly was heated in a vertical glass cylinder wrapped with a nichrome coil heating element. The cell was mounted in an aluminum block heater below.

After the solution sample was poured into the filtering assembly, and the low nitrogen gas pressure was applied, the first (5 to 10) cm<sup>3</sup> filtrate was collected in a waste vial and discarded. The next approximately 20 cm<sup>3</sup> filtrate was directed into the light scattering cell. The N<sub>2</sub> gas pressure was adjusted to obtain a filtration flux of about 1 drop per few seconds to a few drops per second.

Subsequent light scattering measurements generally indicated a high success rate in obtaining solution and solvent samples free from dust contamination. At the conclusion of an experiment,

the cell components and filtering assembly components were cleaned with refluxing hot xylene vapors. This cleaning process appeared successful in removing dust and polymer exhaustively.

### 5.7 Measurement Protocol

The temperature was controlled at  $130.0\text{ }^{\circ}\text{C} \pm 0.2\text{ }^{\circ}\text{C}$  in all light scattering measurements on polyethylene in 1-chloronaphthalene. In all experiments, the intensity measuring system was calibrated with the scattering intensity at  $90^{\circ}$  angle ( $I(90)$ ) by a TCB standard cell described above; the scattering intensity from the solvent and each solution was measured at seven angles in the range from  $60^{\circ}$  to  $120^{\circ}$ . Scattering intensity measurements versus angle ( $I(\theta)$ ) were conducted with the solvent cell immediately following the calibration against TCB, and twice more after  $I(\theta)$  measurements had been conducted on all the solution cells.

All cells containing the TCB secondary standard and samples of solvent or solution were stored in an oven at  $(140\text{ to }150)\text{ }^{\circ}\text{C}$ . Each cell was transferred from the oven to the vat in preparation for scattering intensity measurements, and allowed to remain undisturbed in the vat for at least 10 min to thermally equilibrate at the experimental temperature before initiating the measurements.

At the conclusion of each experiment, the TCB secondary standard cell was withdrawn from the oven and stored at ambient temperature. In two cases replicate light scattering experiments were conducted with a set of solution and solvent samples on the day following the initial experiment, after the polyethylene had been in hot solution environment for longer than 24 h. The TCB secondary standard cell was returned to the oven a few hours before initiating the replicate experiment in order to heat it up to the range of experimental temperature. These replicate experiments gave results, which appeared to indicate thermal stability of this polymer in its high temperature solution state over an interval of at least 24 h.

### 5.8 Analysis of Light Scattering Data

Light scattering data from polymer solutions of concentration  $c$  and scattering angle  $\Theta$  may be analyzed by fitting the scattering signal  $I(\Theta, c)$  to [28]

$$I(\Theta, c) = I(\Theta, 0) + c \sum_{ij} C_{ij} c^i \sin^{2j}(\Theta/2) / I_G \quad (15)$$

In eq. (5),  $I_G$  is the scattering signal from the TCB working standard at  $\Theta = 90^{\circ}$ .

We must first decide how many terms on the right-hand side of eq. (15) need to be included to provide an adequate fit to the experimental data. The dependence of  $c/I_c$ , where  $I_c = \sin\Theta[I(\Theta, c) - I(\Theta, 0)]/I_G$ , upon  $c$  and upon  $\sin^2(\Theta/2)$  reflects solute-solvent interactions and solute size, respectively. Accordingly, preliminary scattering data for SRM 2885 were first analyzed as  $c/I_c$

versus  $\sin^2(\Theta/2)$  and  $c$  and  $c^2$ , to see whether a series retaining only  $C_{00}$ ,  $C_{01}$ ,  $C_{10}$  and  $C_{20}$  would provide an adequate fit. The analysis revealed that this approximation was adequate at concentrations below 1.5 g/L for SRM 2885 (see Section 5.10.13 for a more complete discussion).

Thus, we used for the final analysis

$$I(\Theta,c) = I(\Theta,0) + c I_G / \{ \sin \Theta (C_{00} + C_{01} \sin^2(\Theta/2) + C_{10}c + C_{20}c^2) \} \quad (16)$$

The coefficients in eq. (16) are related to the  $M_w$ , molecular mean-square radius of gyration,  $R_G^2$ , the second virial coefficients,  $A_2$ , and the third virial coefficients,  $A_3$ , by [28,29]:

$$M_w = (K'C_{00})^{-1} \quad (17)$$

$$R_G^2 = 3[\lambda_0/(4\pi n)]^2 C_{01}/C_{00} \quad (18)$$

$$A_2 = K'C_{10}/2 \quad (19)$$

$$A_3 = K'C_{20}/3 \quad (20)$$

$$K' = 4\pi^2 n_B^2 (dn/dc)^2 / (\lambda_0^4 N_A R_v^B S_{23}) \quad (21)$$

where:

$\lambda_0$  is the wavelength in vacuum of the scattered light, 632.8 nm in this work,  $n$  and  $n_B$  are the indices of refraction of the solvent at 130 °C and benzene at 23 °C taken as 1.5772 and 1.4941, respectively calculated as described in Section 5.3,  $dn/dc$  is the specific refractive index increment of the solution, measured as described in 5.2,  $N_A$  is Avogadro's number, taken as  $6.022 \times 10^{23}$  /mol,  $R_v^B$  is the Rayleigh ratio for the total scattering of vertically polarized light from benzene at 23 °C, used as the calibration standard.  $S_{23}$  is the ratio of the scattering of the benzene at 23 °C to the TCB working standard at 130 °C. The method of obtaining  $S_{23}$  is described in section 5.5.

Preliminary fitting was done in the Zimm form, that is, plots of  $c/I_c$  versus  $\sin^2(\Theta/2)$  and  $c$ , or if we wish to include third virial terms as  $c/I_c$  versus  $\sin^2(\Theta/2)$  and  $c$  and  $c^2$ . We then fit to the nonlinear form in eq 16 using the parameters from the Zimm fit to estimate the starting parameters to the non-linear fit. This allows us to include the correct weighting of the data and also the zero concentration terms. We found only small changes in all fitting parameters between the fit to the Zimm form and the fit to the form of eq.16 even when we included  $c^2$  terms in the form of eq. 16.

## 5.9 Results for SRM 2885

Five sets of light scattering solutions were analyzed for SRM 2885 using 1-chloronaphthalene as solvent. Each set consisted of eight or ten independently prepared solutions with concentrations from (0.4 to 2.5) g/L. One set had a solution concentration of 0.2 g/L. The polymer for each solution within each set was taken from the SRM sample vials or the division supply lots. Intensities were measured at five to nine scattering angles in the range from 60° to 120°. The intensities of scattered light in each set were fitted by least squares as explained above, and the results were used to calculate  $M_w$ ,  $A_2$ ,  $A_3$  and  $R_g$  using eqns (17)-(21). The values of  $M_w$ ,  $A_2$ ,  $A_3$  and  $R_g$  obtained from the six sample sets were then averaged. Light scattering gave an  $M_w$  of about  $6.28 \times 10^3$  g/mol with a sample standard deviation of  $0.39 \times 10^3$  g/mol, a value of  $A_2$  of  $0.00204$  mol mL/g<sup>2</sup> with a sample standard deviation of  $0.00047$  mol mL/g<sup>2</sup>, a value of  $A_3$  of  $0.0045$  mol mL/g<sup>2</sup> with a sample standard deviation of  $0.017$  a value of  $R_g$  of  $16.9$  nm with a sample standard deviation of  $2.0$  nm. For one set the value of  $C_{10}$  was negative giving a negative value to  $R_g^2$ . We shall discuss this in the next paragraph.

The value of  $A_2$  is in close agreement with that estimated by Han, Wagner and Verdier [28] in the previous certification of SRM 1482, SRM 1483 and SRM 1484. They estimate  $A_2 = 0.00159$  mol mL/g<sup>2</sup> for SRM 1482 which has an  $M_w = 13.6 \times 10^3$  g/mol and  $A_2 = 0.00109$  mol mL/g<sup>2</sup> for SRM 1484 with  $M_w = 32.1 \times 10^3$  g/mol. Our value of  $0.00204$  mol mL/g<sup>2</sup> is consistent with the trend these values display as a function of molecular mass considering our estimated uncertainty in  $A_2$ . They estimate  $R_g = 13.2$  nm for SRM 1482 and  $R_g = 8.2$  nm for SRM 1483, clearly the wrong order for the molecular masses of these molecules. For SRM 1482, they consider the possibilities of large systematic uncertainties in  $R_g$ . We have the same problems with the  $R_g$  we estimate. This is due to an alignment problem we find with our  $I \sin(\tilde{E})$ . This is clear from the fact that for one of our set we obtain an apparent negative value of  $R_g^2$ . Considering all these problems, our value of  $16.9$  nm is in reasonable agreement with their values.

The standard deviation of the mean for the average  $M_w$  of SRM 2885 is  $0.20 \times 10^3$  g/mol. In compliance with the NIST policy [15] on reporting uncertainties in measurement, the component uncertainty due to variance among the five  $M_w$  determinations is computed as the standard deviation of the mean. Table 2 reports twice this value as the expanded uncertainty.

## 5.10 Estimation of Uncertainties Due to Systematic Effects in the Light Scattering

We list the likeliest sources of systematic uncertainty in the determination of  $M_w$  by light scattering measurements described in the preceding sections, and attempt to estimate upper limits for their magnitudes. For this purpose, we employ a scheme similar to that used in ref. [28] for the estimation of systematic uncertainties in SRM's 1482, 1483 and 1484 and ref [29] on the recertification of SRM 706a. These uncertainties are listed in Table 2 for SRM 2885.

### 5.10.1. Indices of Refraction

Following Ref. [28], we estimate that 0.1% is a proper upper limit for systematic relative

standard uncertainties in  $M_w$  arising from uncertainties in the literature values of benzene index of refraction, the calibrating liquid.

## 5.10.2 Calibration of the Differential Refractometer

### 5.10.2.1 Literature Values of $dn/dc$ for Aqueous NaCl

Calibration of the differential refractometer required interpolation of the data of Ref. [16,17,18] to the 632.8 nm wavelength used in the light-scattering measurements. We estimate the relative standard uncertainty in the interpolated values of  $\bar{A}_n$  as 0.6 %, due primarily to uncertainties in the interpolation process. The calibration factor determined for our differential refractometer had a relative standard deviation (rsd) of 0.097 %. Applying a coverage factor of 2 to this rsd yields a Type A expanded uncertainty of 0.19 % for this measurand [15]. Combining this uncertainty with an allowance for possible linear uncertainties in the refractometer, we estimate that a proper upper limit for relative uncertainty in  $dn/dc$  is 1%. Considered as a 95 percent confidence interval estimate, this quoted uncertainty provides a expanded uncertainty in  $dn/dc$  of 1 % which would contribute a 2 % or  $0.13 \times 10^{+3}$  g/mol expanded uncertainty in  $M_w$  determination.

### 5.10.3 Measured Value of $dn/dc$ of SRM 2885

The differential refractive index  $dn/dc$  of SRM 2885 in 1-chloronaphalene at a temperature of 130 °C was determined as described in Section 5.2.4. The mean value obtained for  $dn/dc$  was -0.1867 mL/g , with a standard deviation of 0.0013 mL/g. The uncertainty in the mean is then 0.0007 mL/g. We take the expanded uncertainty of this measurement as 0.0014 mL/g or a relative uncertainty of 0.8 %.

There appears to be no concentration drift in the data. When we refit the data dropping the highest concentration and found a  $dn/dc$  of -0.1869, a number well within our expected expanded uncertainty.

As the  $dn/dc$  appears as the second power in the  $M_w$  calculation, the uncertainty in the calculated  $M_w$  that results from the uncertainty in the  $dn/dc$  is estimated as twice the estimated relative expanded uncertainty in the  $dn/dc$ , or 1.6 % . This gives an expanded uncertainty in the  $M_w$  of  $0.1 \times 10^{+3}$  g/mole.

Contributions to the uncertainty of the value of the density of the solvent to  $dn/dc$  are discussed in section 5.10.8.

### 5.10.4 Wavelength of Radiation

For the He-Ne laser employed in this work, uncertainties in the wavelength of the radiation are

completely negligible compared with uncertainties from other sources.

#### 5.10.5 Calibration Constant for Light Scattering

The protocol for the calibration is described earlier. For each step, we estimate an uncertainty.

##### 5.10.5.1 Rayleigh Ratio of Benzene at room temperature

For benzene at 632.8 nm, Ref. [24] gives:  $R_{V,V+H} = 12.6_3 \times 10^{-6} \text{ cm}^{-1}$ . We abbreviate  $R_{V,V+H}$  by  $R$ . The authors of Ref. [24] apparently believed that their  $R$ -values have a relative standard uncertainty of  $< 2 \%$  (all from systematic uncertainty). They quote a relative standard deviation for their  $R$ -value for benzene of 0.21/12.63, or 1.7 %. This yields a relative expanded uncertainty of 3.9 %, or  $0.25 \times 10^{+3} \text{ g/mol}$ .

##### 5.10.5.2 Estimating Ratio of Benzene Scattering to Glass Rod Scattering at Room Temperature

We have run 20 repeats of the measurements of the ratio of the scattering of the benzene calibrant to the scattering of the glass rod as described in Section 5.5. We take the uncertainty in the repeatability of this experiment as the overall uncertainty of the measurement. The relative standard deviation of this measurement is given as 1.2 %. The relative standard deviation of the mean is 0.27 %. We take 0.6 %, or  $0.04 \times 10^{+3} \text{ g/mol}$ , as the expanded uncertainty from the ratio of the benzene scattering to the glass rod scattering.

A small correction is introduced arising from the fact we calibrated our rod against benzene at 21 °C rather than benzene at 23 °C. We estimated that correction was 0.9946 from literature value on the temperature variation of the scattering from benzene [27]. We estimate from that work as a generous estimate of the relative expanded uncertainty from this calculation to be 0.2 %, or less than  $0.01 \times 10^{+3} \text{ g/mol}$ .

From both above corrections we take an expanded uncertainty from all these contributions to be  $0.05 \times 10^{+3} \text{ g/mol}$ .

##### 5.10.5.3 Temperature Dependence of Scattering of Glass Rod from 21 °C to 130 °C

Han, Wagner and Verdier [28] discussed this issue in Section 4.1.3 of their paper on  $M_w$  determinations of SRM 1482, SRM 1483, and SRM 1484. Since the uncertainty is in the calibration it appears as a percentage of the final result. In that paper, they concluded the maximum relative expanded uncertainty of assuming the scattering of the rod is unchanged from 23 °C to 130 °C is 0.4% of the  $M_w$ . Here, we accept their estimate as the expanded uncertainty. This leads to an expanded uncertainty of  $M_w$  for this polymer of  $0.03 \times 10^{+3} \text{ g/mol}$ .

#### 5.10.5.4 Estimating ratio of Glass Rod Scattering to TCB Scattering at 130 °C

We have 42 repeat measurements of the ratio of the scattering of the glass rod to the scattering from the TCB working standard, described in Section 5.5. We take the uncertainty in the repeatability of this experiment as the overall uncertainty in this measurement. Fourteen measurements of the ratio of the glass rod scattering to that of TCB, the working standard, were made for each of three different scattering cells containing TCB. The relative standard deviation of the mean is 0.2 %. We take 2 times this uncertainty as the expanded uncertainty from the ratio of the benzene scattering to the glass rod scattering. This yields 0.4 % as the relative expanded uncertainty, or  $0.03 \times 10^{+3}$  g/mol.

#### 5.10.6. Uncertainties in the Polarization of Light

There are two uncertainties associated with the laser light. First, the "vertically polarized" laser beam actually contains "horizontally polarized" components for two reasons: the polarizer inside the laser head lets through a small fraction  $\epsilon$  of the "wrong" polarization and the principal axis of polarization of the light from the laser may not be exactly perpendicular to the optic plane defined by the incident and scattered beams. Both uncertainties will cause light, assumed to be vertically polarized, to contain a small admixture of horizontally polarized light. The effect upon scattering signals from SRM 2885 will be slight, but the effect upon the benzene calibration signals is to change the effective Rayleigh ratio that should have been used toward the  $R_{H,V+H}$  value. The resulting uncertainty in  $M_w$  is  $\epsilon/(1-\epsilon)$  for the first effect and  $\tan^2\alpha$ , where  $\alpha$  is the angular mis-setting, for the second. We take  $\epsilon = 1/500$  and  $\alpha = 5^\circ$ . Then the relative expanded uncertainty from  $\epsilon$  is less than 0.2 % with at least a 95 % level of confidence considering the liberal boundaries assigned to the constituent uncertainties. The uncertainty from  $\alpha$  is less than 0.8 % with at least a 95 % level of confidence considering the liberal boundaries assigned to the constituent uncertainties. Following NIST guidelines we take the root-sum-of-squares from these contributions to yield the standard uncertainty of 0.85 % and the relative expanded uncertainty from this contribution of 1.7 %, or  $0.11 \times 10^{+3}$  g/mol.

#### 5.10.7 Ratio of Working Standard Scattering to Sample Scattering

Since photon-counting techniques were employed, there should be no systematic uncertainties from this source. Random uncertainties are reflected in the overall random uncertainty of the  $M_w$ .

#### 5.10.8 Solvent Density

For the density of 1-chloronaphalene at 130 °C, we used the value 1.098 g/mL as given in references [11,25]. Following Han, Wagner and Verdier [28], we estimate that this value has a relative expanded uncertainty of < 0.1 %. The resulting relative expanded uncertainty on  $M_w$  is



just 0.2 %, or  $0.01 \times 10^{+3}$  g/mol.

#### 5.10.9. Solute and Solvent Masses

For the measurements actually used in the final determination of  $M_w$  for SRM 2885, solvent masses were chosen so that the solute masses were always about 0.05 g. Using the uncertainty limit of 0.05 mg we usually assign to the balance used to weigh the PE samples, we have relative expanded uncertainties of 0.1 % in the solute masses. The balance used for solute measurements was regularly checked with a 50 mg mass standard calibrated by the NIST Mass Division and was found to vary by less than 0.01 mg from the standard. The uncertainty in  $M_w$  is then the relative uncertainty in solute masses, or about 0.1 % with at least a 95 % level of confidence. This 95 % confidence interval estimate provides a relative expanded uncertainty of 0.2 %, or  $0.01 \times 10^{+3}$  g/mol.

Solvent masses of at least 30 g were used in solution preparation. The solvent balance was checked against a 100 g mass standard and found to be off by less than 0.01 g. The solvent masses were measured to 0.01 g. Thus, there are negligible uncertainties in solvent masses.

#### 5.10.10 Reflection Correction

The refractive index of 1-chloronaphalene at 130 °C is given as  $n_D = 1.5772$  by an estimate described in Section 5.3. The refractive index of the sample cell is given by the vendor as  $n_D = 1.500$ . Although the wavelength of the reported refractive index of 1-chloronaphthalene and of the cell are different from that uses in our experiments, these values should be adequate to estimate what will turn out to be an extremely small uncertainty. Han, Wagner and Verdier [28] assumed that the refractive index difference between the sample cell and 1-chloronaphalene was about 0.1, an extreme overestimation for our case. With that assumption, they found for a scattering system like ours, a reflection correction of 0.1 yields a reflectance factor  $f = 2 \times 10^{-3}$ . Comparison calculations of  $M_w$  for SRM 1484 with and without this correction show the resulting relative standard uncertainty to be less than 0.01%. The equivalent calculation for SRM 2885 would yield a standard uncertainty of less than 0.01%. We take the uncertainty to the molecular mass from this contribution to be zero.

#### 5.10.11 Instrumental Misalignment

The effects of instrument misalignment are difficult to estimate. For the geometry of the current high temperature light scattering instrument, it is expected that any deviation from constancy of  $I \sin(\Theta)$  is indicative of instrument misalignment. We look at this effect in two different ways.

First,  $I \sin(\Theta)$  values calculated from solvent scattering indicated alignment problems. Whereas these values divided by the intensity at 90° should be independent of  $\Theta$  they showed a fractional

variation of 0.6 % to 1.0 % . If we assume that the data scales with this uncertainty, we would estimate a relative expanded uncertainty of 0.6 % to 1.0 % in  $M_w$ .

Second, from our experience with the alignment, we would also estimate the maximum misalignment to be  $0.2^\circ$ . We have examined two sets of data by purposefully recomputing the  $M_w$  putting in a misalignment of  $0.2^\circ$ . They consistently both show for a systematic angle variation of  $+0.2^\circ$  the  $M_w$  varies by about a fraction of 1.0 % and for an angle of  $-0.2^\circ$  the  $M_w$  varies by -1.0 %.

Since both estimates of uncertainty yield a maximum expanded uncertainty of about 1 % from misalignment, we estimate a total relative expanded uncertainty arising from instrument misalignment of 1.0 %, or  $0.06 \times 10^{+3}$  g/mol for SRM 2885.

#### 5.10.12. Anisotropy of Solute

Following Han, Wagner, and Verdier [28], we find that equations for  $M_w$  and  $K'$  in Section 5.8 are derived on the assumption that the light scattering from the polyethylene is not depolarized. When the solute is optically anisotropy,  $M_w$  should be replaced with  $M_w(1+\epsilon)$  where the correction term is given by:

$$\epsilon = (1/45)(1/M_w) (\langle \gamma^2 \rangle / M_w) [4\pi n_s N_a / (dn/dc)]^2$$

where  $\langle \gamma^2 \rangle$  is given approximately by  $267 \times 10^{-50} \text{ cm}^6$  per  $\text{CH}_2$  group [31, 32]. Thus  $\langle \gamma^2 \rangle / M$  is  $1.91 \times 10^{-49} \text{ mL}^2 / \text{g}$ . We estimate  $\epsilon$  for SRM 2885 as less than 0.0003. We take this to be a relative expanded uncertainty of 0.03 % on  $M_w$ . We consider this correction and uncertainty on this measurement negligible.

#### 5.10.13 Cutoff of Virial Expansion for SRM 2885

We refit the data on all 5 sample sets with and without including a third virial term. The average computed  $M_w$  changed from  $6.28 \times 10^{+3}$  with the third virial to  $6.28 \times 10^{+3}$  with the second virial term in the series only. As a result we found a change in the  $M_w$  using a fit including only the second virial coefficient and that with a third virial of +1.5%, +1.5 %, + 4.5%, +4.0 % and - 4.5%. We take the average of the above percentages to be the standard uncertainty, 1.5%, and twice that to be the expanded uncertainty. Thus, we take the expanded uncertainty from the virial fit to be  $0.19 \times 10^{+3}$  g/mol.

#### 5.10.14 Scattering Changing during the Measurement: Degradation and other Sources

By their nature light scattering experiments are of short duration. A number of solutions can be prepared and examined by light scattering in a single day. To avoid instability problems solutions

used in the certification of  $M_w$  were prepared and measured on the same day. To test stability we conducted a second set of measurements on the same solutions a few days later. Of the two runs of SRM 2885 where stability was investigated,  $M_w$  was seen to increase by 2.2 %, or  $0.14 \times 10^{+3}$  g/mol, and 4.4 %, or  $0.28 \times 10^{+3}$  g/mol, when the solutions were stored at 130 °C as long as 2 d after preparation. Studies of time effects on another polyethylene fraction being certified, SRM 2887, revealed both increases and decreases in the measured molecular mass as a function of time. We estimate that the light scattering data used in certification of SRM 2885 were acquired within 12 h after the solutions were first heated. We take the contribution to the uncertainty due to changes during the first 12 h of heating to be at most 2 %, or  $0.13 \times 10^{+3}$  g/mol. We take this to be our expanded uncertainty from this part of the measurement.

#### 5.10.15 Summary

The combined expanded uncertainties,  $U_c$ , of SRM 2885 are computed as root-sum-of-squares of the component expanded uncertainties,  $u_i$ , following the formal NIST policy for evaluating and expressing uncertainty in measurements [15]. In Table 2, we find that the combined expanded uncertainty,  $U_c$ , of SRM 2885 is  $0.56 \times 10^{+3}$  g/mol.

## 6.0 Conclusions

The  $M_w$  of SRM 2885 by light scattering was determined to be  $6.28 \times 10^{+3}$  g/mol with a sample standard deviation of  $0.39 \times 10^{+3}$  g/mol. A combined expanded uncertainty for this light scattering  $M_w$  determination including all type A and type B uncertainties was  $0.56 \times 10^{+3}$  g/mol. The intrinsic viscosity of SRM 2885 by solution viscosity in 1,2,4-trichlorobenzene was determined to be 22.3 mL/g with a sample standard deviation of 0.17 mL/g. The standard deviation on the mean value was 0.17 mL/g. A combined expanded uncertainty for this intrinsic viscosity determination including all type A and type B uncertainties was 0.20 mL/g. The bottle-to-bottle variation of the SRM was checked by size exclusion chromatography and found to be negligible.

### Acknowledgements

The authors would like to thank Charles Han for the use of his high temperature light scattering instrument and his help and discussions concerning this project. Sachin Bhatt assisted with the intrinsic viscosity measurements.

Table 1

Contributions to Expanded Uncertainty in Measured Intrinsic Viscosity of SRM 2885

<b>Source of Uncertainty</b>	<b>Uncertainty (mL/g)</b>
Shear rate dependence	0.0
Solvent density, $\rho(0)$	0.05
Polymer specific volume, $V_{ave}$	0.04
Buoyancy corrections	0.0
Solute masses	0.0
Solvent masses	0.0
Timer	0.01
Flow time correction factor	0.07
Measurement temperature	0.07
Sample uncertainty in fit of data	0.17
Combined Expanded Uncertainties	0.20

Table 2

Contributions to Combined Expanded Uncertainty  
Of the  $M_w$  of SRM 2885

Source of Uncertainty	Contribution ( $10^{+3}$ g/mol)
Expanded Uncertainty from standard deviation of the mean	0.39
Solvent index of refraction	0.01
Calibration of differential refractometer	0.13
Differential refractive index	0.09
Wavelength of light	<0.01
Rayleigh ratio of scattering standard, benzene	0.25
Ratio Scattering Benzene to glass rod	0.05
Temperature Dependence Glass Rod	0.03
Ratio Scattering glass rod to TCB scattering standard	0.03
Polarization of light	0.11
Ratio of standard scattering to sample scattering	<0.01
Solvent density	0.01
Solute and solvent masses	0.01
Light reflection	0.0
Instrumental misalignment	0.06
Anisotropy of polymer in solution	<0.01
Truncation of virial expansion	0.19
Scattering change during the scattering measurement	0.13
Combined expanded uncertainty *, $U_c$	0.56

\* by root-sum-of-squares [15]

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# National Institute of Standards & Technology

## Certificate of Analysis

### Standard Reference Material<sup>®</sup> 2885

#### Polyethylene

( $M_w$ , 6 280 g/mol)

This Standard Reference Material (SRM) is intended primarily for use in calibration and performance evaluation of instruments used to determine the molar mass\* and molar mass distribution by size exclusion chromatography. A unit of SRM 2885 consists of approximately 0.3 g of polyethylene powder. The certified values and uncertainties for mass-average molar mass and intrinsic viscosity are presented in Table 1.

Table 1. Certified Properties

Property	Certified Value
Mass-Average Molar Mass* ( $M_w$ )	$6.28 \times 10^3 \text{ g/mol} \pm 0.56 \times 10^3 \text{ g/mol}$
Intrinsic Viscosity [ $\eta$ ] in 1,2,4-trichlorobenzene at 130 °C	$22.3 \text{ mL/g} \pm 0.20 \text{ mL/g}$

\* Previously expressed as molecular weight [1].

**Certified Values and Uncertainties:** The certified value for  $M_w$  was measured using static light scattering with 1-chloronaphthalene as the solvent at 130 °C [2]. The certified value for the intrinsic viscosity was determined in 1,2,4-trichlorobenzene at 130 °C.

The certified measurement uncertainty is expressed as a combined expanded uncertainty with a coverage factor,  $k = 2$ , calculated in accordance with NIST procedure [3]. Type A and Type B contributions to the expanded uncertainty of the measured mass-average molar mass include the uncertainties in the Rayleigh ratio of the scattering standard, optical alignment, and calibration of the differential refractometer.

**Expiration of Certification:** The certification of SRM 2885 is valid until **01 January 2008**, within the measurement uncertainties specified, provided that the SRM is handled in accordance with the storage instructions given in this certificate. This certification is nullified if the SRM is modified or contaminated.

**Maintenance of SRM Certification:** NIST will monitor this SRM over the period of its certification. If substantive technical changes occur that affect the certification before expiration of this certificate, NIST will notify the purchaser. Return of the attached registration card will facilitate notification.

The technical coordination leading to certification of this SRM was provided by B.M. Fanconi of the NIST Polymers Division. Technical measurements and data interpretation were provided by C.M. Guttman, W.R. Blair, J.R. Maurey, and C.R. Schultheisz of the NIST Polymers Division.

The support aspects involved in the preparation, certification, and issuance of this SRM were coordinated through the NIST Standard Reference Materials Program by J.W.L. Thomas.

Eric J. Amis, Chief  
Polymers Division

Gaithersburg, MD 20899  
Certificate Issue Date: 06 April 2001

Nancy M. Trahey, Chief  
Standard Reference Materials Program

**Storage:** The SRM should be stored in the original bottle with the lid tightly closed and under normal laboratory

conditions.

**Homogeneity and Characterization:** The homogeneity of SRM 2885 was tested by size exclusion chromatography analysis of solutions in 1,2,4-trichlorobenzene at 130 °C. The characterization of this polymer is described in Reference 3. SRM 2885 is the result of a clean-up, blending, and rebottling of the fractionation of SRM 1475. It was produced in the same fractionation as SRM 1482, SRM 1483, and SRM 1484 [4].

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*Users of this SRM should ensure that the certificate in their possession is current. This can be accomplished by contacting the SRM Program at: telephone (301) 975-6776; fax (301) 926-4751; e-mail [srminfo@nist.gov](mailto:srminfo@nist.gov); or via the Internet <http://www.nist.gov/srm>.*