A Causal Microwave Circuit Theory and Its Implications

Dylan F. Williams and Bradley K. Alpert

National Institute of Standards and Technology, 325 Broadway, Boulder, CO 80303 Ph: [+1] (303)497-3138 Fax: [+1] (303)497-3122 E-mail: dylan@boulder.nist.gov

Abstract- We will describe a new causal powernormalized waveguide equivalent-circuit theory and explore its implications. The new theory marries a power normalization with additional constraints that enforce simultaneity of the theory's voltages and currents and the actual fields in the circuit.

The causal waveguide circuit theory of [1] requires that $Z_0(\omega)$, the characteristic impedance of the guide, be minimum phase. That is, the theory requires that $\hat{Z}_0(t) = 0$ and $\hat{Y}_0(t) = 0$ for t < 0, where $\hat{Z}_0(t)$ and $\hat{Y}_0(t)$ are the inverse Fourier transforms of $Z_0(\omega)$ and $Y_0(\omega) \equiv 1/Z_0(\omega)$. This condition is required to ensure that the waveguide responds to inputs after, not before, it is excited.

The voltage v and current i in [1] are defined by

$$\boldsymbol{E}_{t}(\boldsymbol{r},z) = \frac{\boldsymbol{v}(z)}{\boldsymbol{v}_{0}} \boldsymbol{e}_{t}(\boldsymbol{r}); \ \boldsymbol{H}_{t}(\boldsymbol{r},z) = \frac{\boldsymbol{i}(z)}{\boldsymbol{i}_{0}} \boldsymbol{h}_{t}(\boldsymbol{r}), \qquad (1)$$

where $\mathbf{r} = (x,y)$ is the transverse coordinate, \mathbf{E}_t and \mathbf{H}_t are the total electric and magnetic fields in the guide, \mathbf{e}_t and \mathbf{h}_t are the modal electric and magnetic fields of the single propagating mode, and v_0 and i_0 are normalization factors.

The power normalization is achieved by imposing the constraint [2]

$$v_0 i_0^* = p_0 \equiv \int_S \boldsymbol{e}_t \times \boldsymbol{h}_t^* \cdot \boldsymbol{z} \, \mathrm{d}S, \qquad (2)$$

which ensures that the time-average power is $p = \frac{1}{2}vi^*$. The characteristic impedance Z_0 of the waveguide is defined by

$$Z_0 = \frac{v}{i}\Big|_{c_{-}=0} = \frac{v_0}{i_0} = \frac{|v_0|^2}{p_0^*} = \frac{p_0}{|i_0|^2}, \quad (3)$$

which shows that the power normalization sets the

phase of Z_0 equal to the phase of p_0 , a fixed property of the guide.

However, the minimum phase constraint imposed by causality is a strong one [3], [4]. It requires that the Hilbert transform of $\ln|\lambda Z_0|$, where λ is a constant, be equal to $\arg(Z_0) = \arg(p_0)$, a fixed property of the guide. As a result, the characteristic impedance of the guide is determined within a constant.

The implications of the new causal circuit theory of [1] are significant. The power flow p_0 is real in a lossless coaxial transmission line, so the phase of Z_0 is 0, and in the causal circuit theory $|Z_0|$ must be constant. We also show that the characteristic impedance of a rectangular waveguide must be proportional to the wave impedance of the guide: the choice $|Z_0| = 1$, allowed in conventional waveguide circuit theories, is not admissible in the causal theory.

REFERENCES

1. D.F. Williams and B.K. Alpert, "Causality and waveguide circuit theory," submitted to *IEEE Trans. Microwave Theory Tech.* Advance copies posted on http://www.boulder.nist.gov/div813/dylan/ and http://math.nist.gov/mcsd/Staff/BAlpert/.

2. R. B. Marks and D. F. Williams, "A general waveguide circuit theory," *J. Res. Natl. Inst. Stand. Technol.*, vol. 97, no. 5, pp. 533-562, Sept.-Oct., 1992.

3. E.A. Guillemin, *Synthesis of Passive Networks*. John Wiley and Sons: New York, 1957.

4. A.V. Oppenheimer and R.W. Schafer, *Digital Signal Processing*. Prentice-Hall International: London, 1975.

Publication of the National Institute of Standards and Technology, not subject to copyright.