## CORRELATIONS

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# Correlation for the Vapor Pressure of Mercury<sup>†</sup>

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We present a new correlation for the vapor pressure of mercury that is valid from the triple point to the critical point. The equation is a Wagner-type form, where the terms of the equation are selected using a simulated annealing optimization algorithm. To improve the reliability of the equation at low temperatures, heat-capacity data were used in addition to vapor-pressure data. We present comparisons with available experimental data and existing correlations. The estimated uncertainty at a coverage factor of 2 varies from 3% near the triple point to 1% for temperatures from 273 to 400 K; 0.15% for the intermediate temperature region from 400 K to the normal boiling point at 629.77 K; for temperatures above the normal boiling point but below  $\sim$ 900 K, it is 0.5%; and for temperatures between 900 K and the critical point, we estimate that the uncertainty is 5%.

#### Introduction

Concerns about mercury as an industrial pollutant have led to increased interest in the detection and regulation of mercury in the environment.1 The recent Clean Air Mercury Rule2 will permanently cap and reduce mercury emissions from coal-fired power plants. The development of standardized equations for the thermophysical properties of mercury can aid in the implementation of this task. A critical evaluation of density, thermal expansion coefficients, and compressibilities, as a function of temperature and pressure, was conducted by Holman and ten Seldam.<sup>3</sup> Bettin and Fehlauer<sup>4</sup> recently reviewed the density of mercury for metrological applications. Vukalovich and Fokin's book<sup>5</sup> and the *Gmelin Handbook*<sup>6</sup> are both thorough treatises on the thermophysical properties of mercury. Thermal properties such as thermal conductivity and heat capacity were reviewed by Sakonidou et al.,7 whereas Hensel and Warren<sup>8</sup> have covered other properties, including optical and magnetic characteristics. To aid in the development of standards for the concentration of mercury in air, it is important to have an accurate representation of the vapor pressure of mercury. Numerous compilations and correlations of the vapor pressure of mercury have been published;<sup>9-26</sup> however, there is no consensus on which is the best one to use for a given purpose. To address this issue, we review the existing experimental data and correlations and provide a new representation of the vapor pressure of mercury that is valid from the triple point to the critical point. We also present comparisons with both experimental data and correlations, and we estimate the uncertainty of the correlation. This manuscript summarizes the work; a more-complete description, including tabulations of available experimental data, and a moredetailed discussion of the results for the temperature range of 273-333 K, is presented in a NIST Internal Report.<sup>27</sup>

#### **Experimental Vapor-Pressure Data**

Experimental measurements of the vapor pressure of mercury have a long history, dating all the way back to the 1800s. Table 1 gives a detailed compilation of sources of vapor-pressure data from 1862 to the present, along with the temperature range of the measurements, the experimental method used, and an estimate of the uncertainty of these measurements. Generally, determinations of the purity of the mercury were not available; however, methods for the purification of mercury have been known for a long time, and high-purity samples were prepared before it was possible to quantify the purity.<sup>19</sup> The estimates of uncertainty were obtained by considering the experimental method and conditions, the original author's estimates (when available), and the agreement with preliminary correlations. These correspond to our estimate of a combined expanded uncertainty with a coverage factor of 2.

As indicated in Table 1, many measurements have been made on the vapor pressure of mercury. However, only a limited number of these are comprehensive and have uncertainty levels of 1% or less. These sets have been identified as primary data sets in our work and are indicated by boldface type in Table 1. Generally, the most-accurate measurements were those made with ebulliometric methods. Ambrose and Sprake<sup>19</sup> used an ebulliometric technique for their measurements over a temperature range of 380-771 K. These data have an uncertainty of  $\sim 0.03\%$  or lower, with the largest uncertainty at the lowest temperatures. Beattie et al.<sup>28</sup> very accurately determined the boiling point of mercury over a temperature range of 623-636 K. Spedding and Dye81 used an isoteniscope to measure the vapor pressure over a temperature range of 534-630 K, with uncertainties on the order of 0.03%, except at the lowest temperatures, where they are larger. Menzies<sup>62,88</sup> used an isoteniscope at temperatures of 395-708 K; however, these data show more scatter and have larger uncertainties than the sets previously mentioned; however, the uncertainties are still <0.5%. Shpil'rain and Nikanorov<sup>80</sup> used an ebulliometric method, extending from 554 K to 883 K. Their data are more consistent with the measurements

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Table 1.	Summary	of Available	Data for the	Vapor	Pressure of Mercury <sup>a</sup>

reference(s)	year	method	number of points	T range (K)	estimated uncertainty (%)
Ambrose and Sprake <sup>19</sup>	1972	ebulliometer	113	417-771	less than 0.03,
Deattin at al 28	1027	hailing tuba	42	(22 (26	greatest at lowest T
Beattle et al. <sup>20</sup>	1937	2 static mathods	42	<b>623-630</b>	0.03
Bessel-Hagen <sup>30</sup>	1925	Töpler vacuum numn	21	273-293	>20
Burlingame <sup>31</sup>	1068	transpiration	38	344-409	4
Busey and Giauque <sup>32</sup>	1908	derived from caloric properties	24	234-750	$\frac{1}{2}$
Dusey and Glauque	1755	derived from calorie properties	24	254 750	3.5 at lowest T
Cailletet et al.33	1900	Bourdon manometer	11	673-1154	varies from 1 to 7
Callendarand Griffiths <sup>34</sup>	1891	Meyer tube	2	630	0.2
Cammenga <sup>35</sup>	1969	effusion	graphical results	273-325	
Carlson et al.36	1963	effusion	9	299-549	varies from 3 to $>20$
Dauphinee <sup>37,38</sup>	1950, 1951	transpiration	18	305-455	5
Douglas et al. <sup>39</sup>	1951	derived from caloric properties	30	234-773	varies from 0.03 (at normal boiling point)
Durrans <sup>40</sup>	1920	gives table attributed to Smith and Menzies <sup>41</sup>	46	273-723	to 1.5 at lowest T
Egerton <sup>42</sup>	1017	affusion	27	280-200	5
Egenon Frnsherger and Pitman <sup>43</sup>	1917	niston manometer	18	289 309	1
Galchenko and Pelevin <sup>44</sup>	1978	static method	graphical results	523-723	3
Galchenko et al. <sup>45</sup>	1978	atomic absorption	correlating	723-873	3
Gebbardt <sup>46</sup>	1005	boiling tube		403-483	8
Haber and Kerschbaum <sup>47</sup>	1905	vibrating quartz filament	1	203	2
Hagen <sup>48</sup>	1882	differential pressure	5	293	>20
Hensel and Franck <sup>49</sup>	1966	electrical resistance	graphical results	1073-critical	not available
Hertz <sup>50</sup>	1882	static absolute manometer	9	363-480	5
Hevcock and Lamplough <sup>51</sup>	1913	not available	1	630	0.2
Hildenbrand et al <sup>52</sup>	1964	torsion-effusion	6	295-332	5
Hill <sup>53</sup>	1922	radiometer principle	19	272-308	30
Hubbard and Ross <sup>54</sup>	1982	static	graphical results	742-1271	not available
Jenkins <sup>55</sup>	1926	isoteniscope	21	479-671	0.1  to  > 20
Kahlbaum <sup>56</sup>	1894	ebulliometer	43	393-493	>10
Knudsen <sup>57</sup>	1909	effusion	10	273-324	varies from 5 to 10
Knudsen <sup>58</sup>	1910	radiometer principle	7	263-298	varies from 5 to 10
Kordes and Raaz <sup>59</sup>	1929	temperature scanning evaporation method	2	630-632	4
Mayer <sup>60</sup>	1930	effusion	82	261-298	5, except greater at T < 270 K
McLeod <sup>61</sup>	1883	transpiration	1	293	>20
Smith and Menzies, <sup>41</sup> Menzies <sup>62</sup>	1910, 1927	isoteniscope	46	395-708	0.5
Millar <sup>63</sup>	1927	isoteniscope	6	468-614	2
Morley <sup>64</sup>	1904	transpiration	6	289-343	varies from 8 to $>20$
Murgulescu and Topor <sup>03</sup>	1966	quasi-static	9	301-549	3
Neumann and Volker <sup>60</sup>	1932	torsion balance	19	290-344	6
Pedder and Barratt <sup>o</sup>	1933	transpiration	3	229-273	2
Plaululer <sup>50</sup>	1025	gas saturation	5 17*	200-572	12 5 20 grantast at
Pointexter <sup>35</sup>	1925		17*	255-295	5-20, greatest at lowest T
Raabe and Sadus <sup>70</sup>	2005	computer simulation	20	408-1575	varies from 0.5 to $\geq 20$
Ramsay and Young <sup>**</sup>	1860	isoteniscope	13	495-721	varies from 0.5 to 10 at highest T
Regilault	1025	avasi statia	29	297-785	higher for lower $T$
Roeder and Morawietz <sup>74</sup>	1925	quasi-static	7	413-614	2
Ruff and Bergdahl <sup>75</sup>	1919	temperature scanning	12	478-630	$^{2} > 20$
Schmahl et al. <sup>76</sup>	1965	evaporation method static method	43	412-640	1.5
Schneider and Schupp <sup>77</sup>	1944	gas saturation	23	484-575	10
Schönherr and Hensel <sup>78</sup>	1981	electrical conductivity	13	1052-1735	3
Scott <sup>79</sup>	1924	vibrating quartz filament	1	293	2
Shpil'rain and Nikanorov <sup>80</sup>	1971	ebulliometer	50	554-883	0.6-0.8
Spedding and Dye <sup>81</sup>	1955	isoteniscope	13	534-630	0.03
Stock and Zimmermann <sup>82</sup>	1929	transpiration	$3^b$	253-283	20
Sugawara et al. <sup>10</sup>	1962	static method	14	602-930	2
van der Plaats <sup>83</sup>	1886	transpiration	26	273-358	
Villiers <sup>84</sup>	1913	ebulliometer	12	333-373	6
Volmer and Kirchhoff <sup>85</sup>	1925	effusion	10	303-313	3
von Halban <sup>86</sup>	1935	resonance light absorption	1 <sup>b</sup>	255	7
Young <sup>87</sup>	1891	static	11	457-718	2

<sup>a</sup> References in boldface indicate primary data sets (see text). <sup>b</sup> Excludes points below the triple point.

of Ambrose and Sprake<sup>19</sup> in their region of overlap than are other high-temperature sets, such as those by Sugawara et al.,<sup>10</sup> Bernhardt,<sup>29</sup> or Cailletet et al.,<sup>33</sup> and thus were selected as the primary data for the high-temperature region from  $\sim$ 700 K to 900 K. In addition, although the uncertainty is >1%, we have selected the data of Schönherr and Hensel<sup>78</sup> for the highest-

Table 2. Critical Temperature and Pressure of Mercury<sup>a</sup>

reference	year	$T_{\rm c}({\rm K})$	p <sub>c</sub> (MPa)
Koenigsberger92	1912	~1543	
Menzies <sup>88</sup>	1913	>1548	
Bender <sup>93</sup>	1915	1923	
Meyer <sup>94</sup>	1921	1747	
Bernhardt <sup>29</sup>	1925	1923	294.2-343.2
Birch <sup>95</sup>	1932	$1733 \pm 20$	$161 \pm 5$
Hensel and Franck,49	1966	$1763.15 \pm 15$	$151 \pm 3$
Franck and Hensel96			
Kikoin and Senchenkov97	1967	$1753 \pm 10$	$152 \pm 1$
Neale and Cusack98	1979	$1768 \pm 8$	$167.5\pm2.5$
Hubbard and Ross <sup>99</sup>	1983	1750	172
Götzlaff <sup>14</sup>	1988	$1751 \pm 1$	$167.3\pm0.2$
Kozhevnikov et al.91	1996	$1764 \pm 1$	$167 \pm 3$

<sup>*a*</sup> Uncertainties are expressed in units of K and MPa for the temperature and pressure, respectively.

temperature region, 1052–1735 K. This data set was obtained by observing changes in the electrical conductivity. At fixed pressures, the temperature was increased, and when a discontinuity was observed, this was considered to be an indication of phase change.

All of the sets mentioned thus far are given for temperatures of >380 K. At lower temperatures, the measurements are much more uncertain and display significant scatter. In the low-temperature range, we considered the measurements of Ernsberger and Pitman<sup>43</sup> to be the most accurate. These measurements were made with an absolute manometer method, with uncertainties on the order of 1%, and they cover the temperature range of 285–327 K. This data set has been adopted in the metrology community for use in precision manometry, and it has been described as reliable and confirmed by heat-capacity measurements.<sup>89</sup>

The triple point of mercury has been designated as a fixed point of the ITS-90 temperature scale,<sup>90</sup> with a value of 234.3156 K. The critical point has been measured by several investigators; these values are listed in Table 2, along with uncertainty estimates provided by the authors. In this work, we adopted the critical point of Kozhevnikov et al.<sup>91</sup>

#### **Correlation Development**

Numerous expressions have been used to represent the vapor pressure of a pure fluid; many are reviewed in Růžička and Majer.<sup>100</sup> Equations of the general form

$$\ln\left(\frac{p}{p_{\rm c}}\right) = \left(\frac{T_{\rm c}}{T}\right) \sum_{i} a_i \tau^{i/2} \tag{1}$$

where  $\tau = 1 - (T/T_c)$ , are attributed to Wagner and coworkers<sup>101-104</sup> and have been used successfully to represent the vapor pressures of a wide variety of fluids. Lemmon and Goodwin<sup>105</sup> used the Wagner form with exponents that had values of 1, 1.5, 2.5, and 5 to represent the vapor pressures of normal alkanes up to C<sub>36</sub>. This form, which we will call Wagner 2.5-5, is one of the most widely used forms, along with the equation with exponents that had values of 1, 1.5, 3, and 6,<sup>101,102</sup> which we call Wagner 3-6. The Wagner 2.5-5 form has emerged as the generally preferred form.<sup>106</sup> When the data set is extensive and of high quality, other forms with alternative sets of exponents with additional terms have been used. For example, a Wagner equation with exponents of 1, 1.5, 2, 2.5, and 5.5 was used to represent the vapor pressure of acetonitrile,107 and another variant of the Wagner equation, with exponents of 1, 1.89, 2, 3, and 3.6 was used to represent the vapor pressure of heavy water<sup>108</sup> from the triple point to the critical point, to within the experimental scatter of the measurements. The International Association for the Properties of Water and Steam (IAPWS) formulation for the vapor pressure of water<sup>109,110</sup> uses a six-term Wagner equation with exponents of 1, 1.5, 3, 3.5, 4, and 7.5.

Because there is a lack of high-quality experimental vaporpressure data in the low-temperature region ( $T \le 285$  K), liquid heat-capacity measurements at low temperatures can be used to supplement the vapor-pressure data.<sup>100,106,111</sup> This permits the simultaneous regression of heat-capacity and vapor-pressure data to determine the coefficients of a vapor-pressure equation that is valid down to the triple point. An alternative method is to use an expression that involves the enthalpies of vaporization, in addition to vapor-pressure data.<sup>112</sup> Both of these approaches can be used to ensure that the vapor pressure is thermodynamically consistent with other thermodynamic data.

King and Al-Najjar<sup>111</sup> related heat capacity and vapor pressure, using the relation

$$\frac{\mathrm{d}}{\mathrm{d}T} \left( T^2 \frac{\mathrm{d}\ln p_{\mathrm{sat}}}{\mathrm{d}T} \right) = \frac{C_p^0 - C_p^\mathrm{L} - G}{R} \tag{2}$$

where  $C_p^0$  and  $C_p^L$  are the heat capacities, at constant pressure, of the ideal gas and the saturated liquid, respectively; *R* is the molar gas constant<sup>113</sup> (*R* = 8.314472 J/(mol K)), *p*<sub>sat</sub> is the vapor pressure, and *G* approximates vapor-phase nonidealities and is given as

$$G = T \left[ p_{\text{sat}} \frac{\mathrm{d}^2 B}{\mathrm{d}T^2} + 2 \frac{\mathrm{d}p_{\text{sat}}}{\mathrm{d}T} \left( \frac{\mathrm{d}B}{\mathrm{d}T} - \frac{\mathrm{d}V_{\text{L}}}{\mathrm{d}T} \right) + \frac{\mathrm{d}^2 p_{\text{sat}}}{\mathrm{d}T^2} \left( B - V_{\text{L}} \right) \right]$$
(3)

In this expression, B is the second virial coefficient and  $V_{\rm L}$  is the molar volume of the liquid. We restrict the use of this equation to temperatures of <270 K, where vapor pressures are on the order of  $10^{-5}$  kPa. In this region, we treat the gas phase as ideal, so that the G term may be neglected. (For example, we applied equations in Douglas et al.<sup>39</sup> for the virial coefficients, liquid volumes, heat capacities, vapor pressures, and their derivatives and estimated that the magnitude of the G term at 270 K, relative to the heat-capacity difference in eq 2, is on the order of 0.0001%.) Assuming that mercury can be considered as an ideal monatomic gas for these low pressures, the idealgas heat capacity for mercury is  $C_p^0 = 5R/2$ .<sup>114</sup> With these assumptions, after the derivatives of the vapor pressure in eq 2 are taken analytically, incorporating the specific form of the vapor-pressure correlation function of eq 1, one obtains the simple expression  $(5R/2 - C_p^L)/R = (T/T_c)\sum a_i(i/2)[(i/2) - C_p^L]/R$ 1)] $\tau^{(i/2)-1}$ .

Busey and Giauque<sup>32</sup> measured the heat capacity ( $C_p$ ) at atmospheric pressure of solid and liquid mercury from 15 K to 330 K, with estimated uncertainties of 0.1%. Amitin et al.<sup>115</sup> also measured the heat capacity of mercury at temperatures of 5–300 K, with an estimated uncertainty of 1%. The smoothed data over the temperature range of 234–270 K from these two sources were identified as primary data for use in the regression, in addition to the primary vapor-pressure data that have been previously discussed.

For our analysis of both  $p_{sat}$  and  $C_p$  experimental data, all temperatures were first converted to the ITS-90 scale. Data taken prior to 1927 were converted to ITS-90, assuming that the older data were on the International Temperature Scale of 1927, although we realize this introduces additional uncertainties.

Table 3. (a) Fitted Values of the Parameters in Eq 4 and Their Standard Deviations, and (b) Fixed Parameters in Eq 4

	(a) Fitted Va Parameters U	lues of the sed in Eq 4	(b) Fixed Used	l Parameters l in Eq 4
i	$a_i$	standard deviation	$T_{\rm c}$ (K)	$p_{\rm c}$ (MPa)
1	-4.57618368	0.0472		
2	-1.40726277	0.8448		
3	2.36263541	0.8204		
4	-31.0889985	1.3439		
5	58.0183959	2.4999		
6	-27.6304546	1.1798		
			1764	167

Except for the data of Menzies,<sup>62</sup> all primary data were measured after 1927. The temperatures of the data of Menzies were first converted to the 1948 temperature scale using the procedure given by Douglas et al.<sup>39</sup> and then were converted to ITS-90.

We regressed the primary data set to three different Wagnertype expressions: the 3-6 form, the 2.5-5 form, and an expression that used variable exponents, where the exponents were selected from a bank of terms, using a simulated annealing procedure.<sup>116,117</sup> Simulated annealing is an optimization technique that can be used in complex problems where there may be multiple local minima. It is a combinatorial method that does not require derivatives and is not dependent on "traveling downhill"; it also is relatively easy to implement. In this work, the search space contained a bank of terms where the bank contained exponents with powers of  $\tau$  in increments of 0.5, with terms up to  $\tau^{12}$ . We followed the recommendation of Harvey and Lemmon<sup>108</sup> and required the equation to contain terms of orders 1, 1.89, and 2, based on theoretical considerations on the behavior near the critical point. The simulated annealing algorithm was used to determine the optimal terms from the bank of terms. We implemented a Lundy and Mees annealing schedule,<sup>118</sup> similar to that of earlier work.<sup>119</sup> During the regression, one can treat the critical pressure as a variable to be determined in the regression, or it can be fixed. Because of concerns about the quality and amount of experimental data in the temperature range of 930-1764 K, we adopted the critical point of Kozhevnikov et al.,91 rather than determining it by fitting experimental data. The minimization was done with orthogonal distance regression, using the NIST statistical package ODRPACK.<sup>120</sup> For the regression, the data were weighted according to their estimated uncertainty (u) with weights of  $1/u^2$ . In addition, the vapor-pressure data were given a relative weight factor of 1, and the heat-capacity data were given a relative weight factor of 0.02. Points that deviated by more than three standard deviations from preliminary fits were considered outliers and were not included in the statistics or the final regression.

The 2.5-5 form of the Wagner equation provided a better fit of the primary data set than the 3.0-6 form; further improvement resulted from the use of the simulated annealing algorithm. Upon closer inspection, we noted that, although one could reasonably reproduce the numerical value of the heat capacity, it was not possible to reproduce well the slope of the saturated liquid heat capacity near the triple point without degrading the fit in other regions. We note that the liquid heat capacity at mercury saturation, as a function of temperature, displays an interesting behavior: a distinct minimum in the curve is observed below the normal boiling point. Douglas et al.<sup>39</sup> noted that other liquid metals such as sodium and potassium also exhibit this behavior. To fit the vapor-pressure and liquid heat-capacity data simultaneously, and to have the correct behavior of the slope of the heat capacity, as a function of

Table 4. Vapor Pressure of Mercury Calculated Using Eq 4 for 273-333 K

			ideal gas de	ensity <sup>a</sup>
$T(\mathbf{K})$	<i>t</i> (°C)	p (MPa)	(mol/L)	(ng/mL)
273.15	0	$2.698829 \times 10^{-8}$	$1.188337 \times 10^{-8}$	2.383684
274.15	1	$2.979392 \times 10^{-8}$	$1.307088 \times 10^{-8}$	2.621887
275.15	2	$3.286720 \times 10^{-8}$	$1.436675 \times 10^{-8}$	2.881826
276.15	3	$3.623129 \times 10^{-8}$	$1.577990 \times 10^{-8}$	3.165289
277.15	4	$3.991118  imes 10^{-8}$	$1.731989 \times 10^{-8}$	3.474196
278.15	5	$4.393376 \times 10^{-8}$	$1.899698 \times 10^{-8}$	3.810605
279.15	6	$4.832795 \times 10^{-8}$	$2.082217 \times 10^{-8}$	4.176720
280.15	7	$5.312487 \times 10^{-8}$	$2.280723 \times 10^{-8}$	4.574903
281.15	8	$5.835798 \times 10^{-8}$	$2.496477 \times 10^{-8}$	5.007682
282.15	9	$6.406319 \times 10^{-8}$	$2.730825 \times 10^{-8}$	5.477762
283.15	10	$7.027907 \times 10^{-8}$	$2.985209 \times 10^{-8}$	5.988031
284.15	11	$7.704698 \times 10^{-8}$	$3.261169 \times 10^{-8}$	6.541579
285.15	12	$8.441128 \times 10^{-8}$	$3.560348 \times 10^{-8}$	7.141702
286.15	13	$9.241950 \times 10^{-8}$	$3.884501 \times 10^{-8}$	7.791920
287.15	14	$1.011225 \times 10^{-7}$	$4.235498 \times 10^{-8}$	8.495986
288.15	15	$1.105749 \times 10^{-7}$ 1.208248 × 10 <sup>-7</sup>	$4.015554 \times 10^{-8}$	9.257899
289.15	10	$1.208348 \times 10^{-7}$	$5.020135 \times 10^{-8}$	10.08192
290.15	17	$1.519040 \times 10^{-7}$ $1.440208 \times 10^{-7}$	$5.470101 \times 10^{-8}$	11.02475
291.15	10	$1.440308 \times 10^{-7}$ 1.571046 × 10 <sup>-7</sup>	$5.949822 \times 10^{-8}$ 6/67678 × 10 <sup>-8</sup>	12 97352
293.15	20	$1.371040 \times 10^{-7}$ 1.712619 × 10 <sup>-7</sup>	$7.026452 \times 10^{-8}$	14 09436
294.15	20	$1.712017 \times 10^{-7}$ 1.865835 × 10 <sup>-7</sup>	$7.020432 \times 10^{-8}$ 7.629036 × 10 <sup>-8</sup>	15 30308
295.15	22	$2.031558 \times 10^{-7}$	$8.278502 \times 10^{-8}$	16 60585
296.15	23	$2.210708 \times 10^{-7}$	$8.978112 \times 10^{-8}$	18.00919
297.15	23	$2.404265 \times 10^{-7}$	$9.731323 \times 10^{-8}$	19.52006
298.15	25	$2.613271 \times 10^{-7}$	$1.054180 \times 10^{-7}$	21.14581
299.15	26	$2.838837 \times 10^{-7}$	$1.141344 \times 10^{-7}$	22.89423
300.15	27	$3.082141 \times 10^{-7}$	$1.235036 \times 10^{-7}$	24.77358
301.15	28	$3.344440 \times 10^{-7}$	$1.335691 \times 10^{-7}$	26.79262
302.15	29	$3.627066 \times 10^{-7}$	$1.443770 \times 10^{-7}$	28.96059
303.15	30	$3.931433 \times 10^{-7}$	$1.559763 \times 10^{-7}$	31.28729
304.15	31	$4.259045 \times 10^{-7}$	$1.684185 \times 10^{-7}$	33.78306
305.15	32	$4.611495 \times 10^{-7}$	$1.817581 \times 10^{-7}$	36.45885
306.15	33	$4.990473 \times 10^{-7}$	$1.960527 \times 10^{-7}$	39.32620
307.15	34	$5.397770 \times 10^{-7}$	$2.113631 \times 10^{-7}$	42.39732
308.15	35	$5.835283 \times 10^{-7}$	$2.277535 \times 10^{-7}$	45.68508
309.15	36	$6.305024 \times 10^{-7}$	$2.452917 \times 10^{-7}$	49.20305
310.15	37	$6.809117 \times 10^{-7}$	$2.640489 \times 10^{-7}$	52.96556
311.15	38	$7.349813 \times 10^{-7}$	$2.841004 \times 10^{-7}$	56.98770
312.15	39	$7.929493 \times 10^{-7}$	$3.055255 \times 10^{-7}$	61.28535
214 15	40	$8.550071 \times 10^{-7}$	$3.284075 \times 10^{-7}$	05.8/52/
315.15	41	$9.210003 \times 10^{-7}$ $9.928302 \times 10^{-7}$	$3.528344 \times 10^{-7}$ 3.788986 $\times 10^{-7}$	76.00327
316.15	42	$1.060052 \times 10^{-6}$	$4.066972 \times 10^{-7}$	81 57939
317.15	43	$1.000002 \times 10^{-6}$ 1.150580 $\times 10^{-6}$	$4.363324 \times 10^{-7}$	87 52391
318 15	45	$1.130300 \times 10^{-6}$ $1.237743 \times 10^{-6}$	$4.505524 \times 10^{-7}$ 4 679116 × 10 <sup>-7</sup>	93 85838
319.15	46	$1.237743 \times 10^{-6}$ 1 330888 × 10 <sup>-6</sup>	$5.015475 \times 10^{-7}$	100 6054
320.15	47	$1.430383 \times 10^{-6}$	$5.373585 \times 10^{-7}$	107.7888
321.15	48	$1.536613 \times 10^{-6}$	$5.754690 \times 10^{-7}$	115.4333
322.15	49	$1.649985 \times 10^{-6}$	$6.160093 \times 10^{-7}$	123.5653
323.15	50	$1.770928 \times 10^{-6}$	$6.591162 \times 10^{-7}$	132.2121
324.15	51	$1.899890 \times 10^{-6}$	$7.049329 \times 10^{-7}$	141.4025
325.15	52	$2.037347 \times 10^{-6}$	$7.536097 \times 10^{-7}$	151.1666
326.15	53	$2.183795  imes 10^{-6}$	$8.053040 \times 10^{-7}$	161.5359
327.15	54	$2.339760 \times 10^{-6}$	$8.601806 \times 10^{-7}$	172.5436
328.15	55	$2.505789 \times 10^{-6}$	$9.184118 \times 10^{-7}$	184.2242
329.15	56	$2.682462 \times 10^{-6}$	$9.801783 \times 10^{-7}$	196.6140
330.15	57	$2.870385 \times 10^{-6}$	$1.045669 \times 10^{-6}$	209.7507
331.15	58	$3.070193 \times 10^{-6}$	$1.115081 \times 10^{-6}$	223.6740
332.15	59	$3.282555 \times 10^{-6}$	$1.188620 \times 10^{-6}$	238.4253
1111	60	$10^{-0}$ × 10 × 10 <sup>-0</sup>	$1.700004 \times 10^{-0}$	754 U/4 / X

<sup>a</sup> Assuming that the ideal gas law applies.

temperature along the saturation boundary, we increased the number of terms in the regression from five to six and used the simulated annealing algorithm to obtain our final equation,

$$\ln\left(\frac{p}{p_{\rm c}}\right) = \left(\frac{T_{\rm c}}{T}\right)(a_1\tau + a_2\tau^{1.89} + a_3\tau^2 + a_4\tau^8 + a_5\tau^{8.5} + a_6\tau^9)$$
(4)

The regressed coefficients and their standard deviations are given in Table 3a, and fixed parameters for eq 4 are given in



Figure 1. Deviations between the correlation given in eq 4 and the primary data set.



Figure 2. Deviations between the correlation given in eq 4 and selected secondary data.

Table 3b. Table 4 gives sample values of the vapor pressure calculated from eq 4 over the temperature range of 273.15–333.15 K. To validate the computer code, more digits are given than are statistically meaningful. For the calibration community, in Table 4, we also have included the density of saturated mercury vapor in moles per liter and in nanograms per milliliter obtained, assuming that the ideal gas law applies ( $\rho = p/(RT)$ ). We use the currently accepted values of the molar gas constant<sup>113</sup> (R = 8.314 472 J/(mol K)) and the atomic mass of mercury<sup>121</sup> (200.59 g/mol).

#### **Comparison with Experimental Data**

For the 294 vapor pressure points in the primary data set, the average absolute deviation (AAD) is 0.14%, the bias is -0.028%, and the root-mean-square (RMS) deviation is 0.35% where we use the definitions AAD =  $(100/n)\Sigma abs(p_i^{calc}/p_i^{expt} - 1)$ , BIAS =  $(100/n)\Sigma(p_i^{calc}/p_i^{expt} - 1)$ , and RMS<sup>2</sup> =  $(100/n) \times \Sigma(p_i^{calc}/p_i^{expt} - 1)^2 - ((100/n)\Sigma(p_i^{calc}/p_i^{expt} - 1))^2$ , where *n* is the number of points. The AAD and RMS values for the primary data are given in Table 5. The normal boiling point calculated by this equation is 629.7705 K.

Figure 1 compares the primary data set with our correlation (eq 4). The data of Ernsberger and Pitman<sup>43</sup> display substantial scatter, but the results are within their estimated experimental uncertainty of 1%. The data of Shpil'rain and Nikanorov<sup>80</sup> also display a fairly high scatter, but, again, it is within their

uncertainty estimate (0.6% - 0.8%). The very accurate measurements of Beattie et al.<sup>28</sup> are in the vicinity of the normal boiling point, and the correlation (eq 4) indicates an uncertainty of 0.02%, at a coverage factor of 2. The measurements of Spedding and Dye<sup>81</sup> and those of Ambrose and Sprake<sup>19</sup> also are represented well by our correlation, although the lowest temperature points display larger scatter than at higher temperatures. The measurements of Smith and Menzies<sup>41</sup> and Menzies<sup>62</sup> are also represented to within their estimated uncertainty. The highest-temperature data of Schönherr and Hensel<sup>78</sup> are represented with an AAD of 1% and a standard deviation of 1.4%; several points are outside of the range of the plot and are not shown. The correlation is valid to the critical point at 1764 K but does not account for a metal-nonmetal transition<sup>54</sup> in mercury at  $\sim$ 1360 K, which results in a change of slope in the vapor-pressure curve.

Figure 2 compares selected data not used in the regression (secondary data) with the correlation (eq 4), and Table 6 summarizes comparisons with all secondary data. It is interesting to note that the behavior of the correlation at low temperatures falls between the values of Douglas et al.<sup>39</sup> and those of Busey and Giauque.32 Both of these sets were not obtained from direct vapor-pressure measurements, but rather were calculated based on caloric measurements combined with vapor-pressure data at higher temperatures. The data of Schmahl et al.<sup>76</sup> cover a range of temperatures, from 412 K to 640 K, and are in good agreement with the correlation. The measurements of Burlingame<sup>31</sup> and of Dauphinee<sup>37</sup> were made using a transpiration technique with uncertainties on the order of 4%-5%, and the correlation represents them within this range of deviations. Figure 2 also displays considerably more scatter at both the highand low-temperature ends of the plot.

#### Comparisons with Correlations from the Literature

Figures 3a and 3b compare correlations and tables for the vapor pressure of mercury in different temperature regions obtained in the literature. In these figures, we define the percent deviation as  $100 \times (p_{eq4} - p_{corr})/p_{eq4}$ , where  $p_{corr}$  is the vapor pressure from correlations in the literature and  $p_{eq4}$  is that obtained from eq 4. We also show the estimated uncertainty band of the new correlation, eq 4, by a heavy black line. The existing correlations in the literature agree well with each other and with the new correlation in the intermediate temperature region from  $\sim$ 400 K to the normal boiling point. In this region, there is a fair number of high-quality experimental data. At low temperatures, the existing correlations differ from each other and some differ from the new correlation. As mentioned previously, there is a paucity of high-quality direct vapor-pressure measurements in this region, and we feel that simultaneously using low-temperature heat-capacity data allows our new correlation to display the proper behavior in the low-temperature region. We also had access to newer data that some of the earlier correlations did not include. For example, the Lange's Handbook correlation<sup>122,123</sup> is based on the International Critical Tables of 1928,<sup>124</sup> whereas the most recent CRC Handbook<sup>125</sup> values are based on the work of Vargaftik et al.,9 which itself is based upon the 1972 book of Vukalovich and Fokin.<sup>5</sup> Some earlier editions of the CRC Handbook (for example, the 57th Edition, 1976-1977, page D-182) used the values from the International Critical Tables of 1928.<sup>124</sup> Few correlations are applicable for higher temperatures. The maximum temperature limit of the Korea Thermophysical Properties Databank (KDB) correlation<sup>126</sup> is given as 654.15 K. The maximum of the Physikalisch-Technische Bundesanstalt (PTB) equation<sup>23</sup> is 930 K; these corre-

Table 5.	Summary of	of Com	oarisons	of the	Correlation	with th	ie Primarv	Data f	for the	Vapor	Pressure	of M	ercury
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				Deviat	ion (%)
reference(s)	number of points	T range (K)	estimated uncertainty (%)	AAD <sup>a</sup>	$\mathrm{RMS}^b$
Ambrose and Sprake <sup>19</sup>	113 <sup>c</sup>	417-771	<0.03, greatest at lowest <i>T</i>	0.02	0.06
Beattie et al. <sup>28</sup>	42	623-636	0.03	0.01	0.01
Ernsberger and Pitman <sup>43</sup>	18	285-327	1	0.33	0.35
Smith and Menzies,41 Menzies62	$46^{d}$	395-708	0.5	0.14	0.20
Schönherr and Hensel <sup>78</sup>	13	1052-1735	3	1.06	1.42
Shpil'rain and Nikanorov <sup>80</sup>	50	554-883	0.6-0.8	0.25	0.29
Spedding and Dye <sup>81</sup>	13	534-630	0.03	0.05	0.06

<sup>a</sup> Average absolute deviation. <sup>b</sup> Root-mean-square deviation. <sup>c</sup> Two outliers, at 380 and 400 K, were not included in the statistics. <sup>d</sup> One outlier, at 395 K, was not included in the statistics.

Table 0, Summary of Comparisons of the Correlation Orgen in Eq. 7 with Secondary Data for the yapor ressure of Mercury	Table 6. St	ummary of Co	mparisons of the	<b>Correlation Give</b>	en in Eq 4	with Secondary	Data for the V	Vapor Pressure of Mercu	rv
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		•	· ·	Deviati	ion (%)
	number of	tomporatura			
reference(s)	points	range (K)	estimated uncertainty (%)	$AAD^{a}$	$RMS^b$
Bernhardt <sup>29</sup>	27	694-1706	varies from 2 to $>15$	14.13	17.26
Bessel-Hagen <sup>30</sup>	2	273-293	>20	96.12	2 50
Burlingame <sup>31</sup>	28	344-400	1 20	1.44	1.02
Busey and Ciouque <sup>32</sup>	24	224 750	4 $T_{\rm varias}$ from 0.2 to 2.5 at lawset T	1.44	1.92
Coilletet et el 33	24	234-730	varies from 1 to 7	0.90	1.05
	11	6/5-1154	varies from 1 to/	5.97	2.20
Callendar and Griffiths <sup>34</sup>	2	630	0.2	0.17	0.14
Cammenga <sup>33</sup>	graphical results	2/3-325			
Carlson et al. <sup>36</sup>	9	299-549	varies from 3 to $\geq 20$	19.74	16.83
Dauphinee <sup>37,38</sup>	18	305 - 455	5	2.14	2.94
Douglas et al. <sup>39</sup>	30	234-773	varies from 0.03 (at normal boiling point) to 1.5 at lowest <i>T</i>	0.45	0.54
Durrans <sup>40</sup>	19	290-344		4.63	3.06
Egerton <sup>42</sup>	27 <sup>c</sup>	289-309	5	6.99	2.34
Galchenko et al.44	graphical results	523-723	3	na <sup>d</sup>	$na^d$
Gebhardt <sup>46</sup>	9	403-483	8	3.34	4.03
Haber and Kerschbaum <sup>47</sup>	1	293	2	1.84	nad
Hagen <sup>48</sup>	5	273-473	>20	51.02	57 44
Hensel and Franck <sup>49</sup>	graphical results	1073-critical	nad	nad	nad
Hortz <sup>50</sup>		363 - 480	5	4.50	1.04
Hevcock and Lamplough <sup>51</sup>	1	630	0.2	4.50	1.94 nod
Heycock and Lampiough <sup>2</sup>	1	205 222	5	0.21	11a <sup></sup>
Hildenbrand et al. <sup>32</sup>	0	295-552	3	2.70	5.10
Hill <sup>55</sup>	19	2/2-308	30	29.40	4.38
Hubbard and Ross <sup>34</sup>	graphical results	/42-12/1	na	na <sup>a</sup>	na"
Jenkins <sup>33</sup>	21	4/9-6/1	varies from 0.1 to $\geq 20$	5.08	5.67
Kahlbaum <sup>36</sup>	43	393-493	>10	8.89	9.47
Knudsen <sup>57</sup>	10	273-324	varies from 5 to 10	7.36	1.67
Knudsen <sup>58</sup>	7	263 - 298	varies from 5 to 10	7.12	7.64
Kordes and Raaz <sup>59</sup>	2	630-632	4	2.59	1.84
Mayer <sup>60</sup>	82	261-298	5, except greater at $T \le 270$ K	6.72	8.86
McLeod <sup>61</sup>	1	293	>20	77.65	$na^d$
Millar <sup>63</sup>	6	468-614	2	1.27	1.84
Morley <sup>64</sup>	6	289-343	varies from 8 to $>20$	17.58	11.82
Murgulescu and Topor <sup>65</sup>	9	301-549	3	1.41	1.56
Neumann and Völker <sup>66</sup>	19	290 - 344	6	4.63	3.06
Pedder and Barratt <sup>67</sup>	3	559-573	2	1.14	0.94
Pfaundler <sup>68</sup>	3	288-372	12	8.06	5.76
Poindexter <sup>69</sup>	17	235-293	>5-20: greatest at lowest T	28.23	29.19
Pamsay and Voung <sup>71</sup>	17	495-721	$x_{1} = 5 - 20$ , greatest at lowest T varies from 0.3 to 10 at highest T	3 23	3.02
Perpault <sup>72</sup>	20	207-785	$\sim 6$ for $T \ge 400$ K much higher for lower T	24.74	34.03
Regiaun Redebush and Divon <sup>73</sup>	29	291-105	$^{1}$ $^{1}$ $^{1}$ $^{2}$ $^{2}$ $^{1}$	24.74	0.54
Rodebush and Dixon <sup>14</sup>	7	444-470	1	0.33	0.34
Roeder and Morawietz	/	413-014	2	1.00	1.11
Ruff and Bergdani <sup>75</sup>	12	4/8-630	>20	22.49	25.78
Schmahl et al. <sup>76</sup>	43	412-640	1.5	0.70	0.71
Schneider and Schupp <sup>77</sup>	23	484-575	10	4.04	5.02
Scott <sup>79</sup>	1	293	2	1.11	na <sup>a</sup>
Stock and Zimmermann <sup>82</sup>	3	253-283	20	15.05	16.80
Sugawara et al. <sup>10</sup>	14	602-930	2	1.15	0.95
van der Plaats <sup>83</sup>	26	273-358	>20	86.65	23.03
Villiers <sup>84</sup>	12	333-373	6	4.76	3.24
Volmer and Kirchhoff <sup>85</sup>	10	303-313	3	1.57	1.13
von Halban <sup>86</sup>	2	220-255	7	8.15	2.21
Young <sup>87</sup>	11	457-718	2	1.40	1.30

<sup>a</sup> Average absolute deviation. <sup>b</sup> Root-mean-square deviation. <sup>c</sup> One outlier, at 288.6 K, was not included in the statistics. <sup>d</sup> Not applicable.

lations should not be extrapolated outside of their given ranges. At the highest temperatures, there are considerable differences

among the various correlations; however, there is also a lack of experimental measurements in this region. The de Kruif corre-



Figure 3. Comparison of the new correlation, eq 4, with previous compilations and correlations in (a) the low-temperature region, up to 600 K, and (b) the high-temperature region, from 600 K to the critical temperature. In each panel, the uncertainty band for eq 4 is indicated by a heavy black solid line.

lation<sup>21,22</sup> does not specifically state the temperature limits of the correlation; however, the very thorough literature survey in the thesis<sup>21</sup> indicates that the only high-temperature data used in their work were those of Bernhardt <sup>29</sup> and Cailletet et al.,<sup>33</sup> and they did not have access to the more-recent measurements of Shpil'rain and Nikanorov,<sup>80</sup> Sugawara et al.,<sup>10</sup> or Schönherr and Hensel.<sup>78</sup> Lange's Handbook<sup>122</sup> includes a note in their table identifying 900 °C as the critical point; this model deviates substantially from the other correlations at high temperatures. The DIPPR<sup>127</sup> and Yaws<sup>128</sup> correlations seem to be indistinguishable on the plot, and both have adopted a critical point of 1735 K and 160.8 MPa. Our correlation agrees very well with these correlations, up to  ${\sim}1500$  K, where the differences are probably due to the critical point adopted in the correlations. Also, the correlation of Schmutzler (as presented in Götzlaff<sup>14</sup>) adopts a different critical point from the selection here; it uses  $T_{\rm c} = 1751$  K and  $p_{\rm c} = 167.3$  MPa. We note that the tabulated

values in the book by Hensel and Warren<sup>8</sup> seem to have been generated from the Schmutzler correlation.<sup>14</sup>

# Detailed Comparisons for the Temperature Range of $0{-}60\ ^\circ C$

The temperature range of 0-60 °C is of particular interest. Unfortunately, in this region, there are very few vapor-pressure data of high accuracy. Our approach, as detailed previously, was to identify the data sets of highest quality and supplement the vapor-pressure data with low-temperature heat-capacity data, to improve the behavior of the correlation at low temperatures and to ensure thermodynamic consistency. The data of Ernsberger and Pitman<sup>43</sup> are the only direct vapor-pressure measurements of low uncertainty (1%) available in this region and were the only low-temperature vapor-pressure data used in the regression. Figure 4 shows the deviations of all data with



**Figure 4.** Comparison of the new correlation, eq 4, in the temperature range of 273–333 K with experimental data, with estimated uncertainties of 3% or less.



**Figure 5.** Comparison of the new correlation, eq 4, in the temperature range of 273–333 K with correlations from the literature.

estimated uncertainties of 3% or less in this temperature range. The data of both Busey and Giauque<sup>32</sup> and Douglas et al.<sup>39</sup> were not direct measurements but rather were values obtained from their analysis of heat-capacity data. Our correlation does not agree with these sets to within their estimated uncertainties, nor do the sets agree with each other (to within these uncertainties). The single data point of Scott<sup>79</sup> at 293 K, determined with a quartz fiber manometer with an estimated uncertainty of 2%, is represented by our correlation within this margin. The measurements of Volmer and Kirchoff<sup>85</sup> have a slightly higher (3%) estimated uncertainty and are represented well by the correlation.

Figure 5 compares correlations in the literature with eq 4 for the temperature range of 273-333 K (0-60 °C). There are four correlations that agree with eq 4 to within our estimated uncertainty of 1%: those by de Kruif,<sup>21,22</sup> DIPPR,<sup>127</sup> Yaws,<sup>128</sup> and Mukhachev et al.<sup>17</sup> Yaws<sup>128</sup> does not state the uncertainty of his equation; however, the DIPPR<sup>127</sup> equation reports an estimated uncertainty of <3%, and the two correlations are almost indistinguishable from each other and are shown here as a single curve. The DIPPR correlation was developed by fitting vapor-pressure data, with a primary data set that consisted of 54 experimental points from Ambrose and Sprake<sup>19</sup> for temperatures of 426-771 K, nine smoothed points from the correlation of Stull<sup>12</sup> for 399-596 K, and 81 points from the tables in Vargaftik<sup>129</sup> for temperatures of 273-1073 K.<sup>130</sup> The correlation of de Kruif<sup>21,22</sup> was developed using the method of Clark and Glew<sup>131</sup> that, in addition to vapor-pressure data, used

supplementary data such as heat capacities, Gibbs free energies of vaporization, and enthalpies of vaporization to develop the correlation. The curve from the CRC Handbook (85th Edition) is based on that of Vargaftik et al.,<sup>9</sup> which itself is based on the work of Vukalovich and Fokin.5 The Vukalovich and Fokin5 source lists the data used in the development of the equation, and apparently they were unaware of the data of Ernsberger and Pitman.<sup>43</sup> As mentioned previously, Ernsberger and Pitman<sup>43</sup> gave an estimated uncertainty of 1% for their measurements, and they seem to be the most-reliable vapor-pressure measurements in the 0-60 °C range. The Mukhachev et al.<sup>17</sup> correlation was developed from caloric data such as the heat of vaporization and heat capacities, along with the normal boiling point of mercury. The KDB correlation<sup>126</sup> is presented only as a set of coefficients with a range of applicability, and we do not know the data used in its development; it is consistently lower than our correlation. The PTB curve,<sup>23</sup> with a reported maximum uncertainty of 4%, is very different in shape from all of the others that have been investigated. This analysis did not incorporate caloric data, and the experimental data in the 0-60°C range that were used in the regression were those of Poindexter<sup>69</sup> and Neumann and Völker.<sup>66</sup> The equation recommended in ASTM Standard D6350132 is presented as a concentration, in terms of nanograms per milliliter. We converted the expression to a vapor pressure by applying the ideal gas law and using an atomic mass<sup>121</sup> of 200.59 and a gas constant<sup>113</sup> value of R = 8.314472 J/(mol K). It agrees well with the values from Lange's Handbook<sup>122,123</sup> and deviates the most from our correlation, approaching 10% at 273 K, and gives vapor pressures that are lower than all the other correlations. The curve in Lange's Handbook<sup>122</sup> is based on the 1928 International Critical Tables (ICT)<sup>124</sup> and was developed with only the limited data and computational methods available at that time.

#### Conclusions

We have developed a new correlation for the vapor pressure of mercury that is valid from the triple point<sup>90</sup> (234.3156 K) to the critical point<sup>91</sup> (1764 K), using a Wagner-type equation. We have determined the uncertainties to be associated with the equation through our comparisons with the primary experimental data and consideration of the uncertainties of these data, as discussed previously. The estimated uncertainty at a coverage factor of 2 varies from 3% near the triple point to 1% for temperatures of 273–400 K, 0.15% for the intermediate temperature region from 400 K to the normal boiling point at 629.77 K, 0.5% for temperatures above the normal boiling point but below ~900 K, and ~5% for temperatures between 900 K and the critical point. The new correlation gives a normal boiling point (at 101.325 kPa) of 629.77 K.

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